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# 216 PATERSON PLANK ROAD SITE CARLSTADT, NEW JERSEY

# OFF-PROPERTY INVESTIGATION INTERIM DATA REPORT

# Prepared for:

The 216 Paterson Plank Road Cooperating PRP Group

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#### 1. INTRODUCTION

On behalf of the 216 Paterson Plank Road Cooperating PRP Group (Group), Golder Associates Inc. (Golder Associates) has prepared this Interim Data Report (Report) for the Off-Property Investigation (Investigation) at the 216 Paterson Plank Road Site (Site) in Carlstadt, New Jersey. The Investigation was conducted pursuant to the Final Work Plan Amendment (Work Plan; Golder Associates, 1995) dated December 21, 1995 and approved on February 14, 1996, by the United States Environmental Protection Agency (USEPA). This Report is submitted in partial fulfillment of the reporting requirements set forth in the Work Plan. Administratively, the work is being conducted pursuant to the additional work provisions of an Administrative Order on Consent (Index No. CERCLA II-50114) dated September 30, 1985 (RI/FS Order).

The primary objective of the Investigation is to provide additional information regarding the nature and extent of groundwater contamination within the till and bedrock units. This Report presents the data collected during the Investigation conducted between June and September 1996; and provides recommendations for additional investigations at the Site.

This Report includes the following key elements:

- Section 2 describes the Site, including previous studies, the 1990 Record of Decision, interim remedial measures, and the regional geologic and hydrogeologic settings;
- Section 3 describes the Investigation procedures including installation of 10 monitoring wells; borehole geophysical testing; hydrogeologic testing; groundwater sampling and analysis; and, long-term water level monitoring;
- Section 4 describes the Site geology and hydrogeology based on previous Site data and the new data obtained during the investigation program, and presents results of chemical analyses of groundwater samples collected during the Investigation; and
- Section 5 presents the conclusions and provides recommendations for future investigations at the Site.

These sections are supported by tables and figures which summarize the analytical data and illustrate geologic and hydrogeologic interpretations. Additional supporting information generated from field activities is included in appendices.

# 2. SITE BACKGROUND

The 6-acre Site is a former chemical recycling and waste processing facility which ceased operation in 1980 and is located in a light industrial/commercial area of Carlstadt, New Jersey (Figure 1). The property is bordered to the southwest by Paterson Plank Road, to the northwest by Gotham Parkway, to the southeast by a trucking company, and to the northeast by Peach Island Creek. The Site was placed on USEPA's National Priorities List (NPL) in 1983.

The following sections provide a brief overview of the major remedial activities conducted at the Site to date.

#### 2.1 Previous Studies

A Remedial Investigation (Dames and Moore, 1990) was initiated in 1987 which evaluated soil and groundwater contamination beneath the Site. Borings were advanced at 30 locations during the remedial investigation and chemical analyses were performed on soil samples from 17 of these borings. In broad terms, the investigation revealed ground conditions comprising fill overlying a clay layer which was in turn underlain by glacial till and bedrock. Fourteen shallow piezometers (P-1 to P-14), and 7 shallow monitoring wells (MW-1S to MW-7S), were installed in the fill zone along with 3 deeper monitoring wells (MW-2D, MW-5D, and MW-7D) as shown on Figure 2.

An initial Feasibility Study was conducted in 1989 by Environmental Resources Management, Inc. (ERM, 1989). The Feasibility Study evaluated remedial alternatives for First Operable Unit (FOU) comprising groundwater and soils/sludge above the clay layer.

A total of nine monitoring wells were installed off-property by Dames and Moore in 1989 pursuant to Project Operations Plan (POP) No. 8 (Dames and Moore, 1988). Five shallow monitoring wells were screened within the fill (MW-8S to MW-12S) and four deeper monitoring wells were installed (MW-8D, MW-11D, MW-12D, and MW-13D). At the specific request of one of the off-Property owners, and with the approval of USEPA, monitoring well RMW-13D was subsequently installed in October 1995 as a replacement for MW-13D. The well installation and boring log was submitted to USEPA on November 20, 1995. Following two rounds of comparative groundwater sampling in RMW-13D and MW-13D, monitoring well MW-13D was decommissioned as part of the Investigation with the approval of USEPA. The well decommissioning form is included in Appendix A.

A deep bedrock monitoring well (MW-2R) was installed on the property by Dames and Moore in 1989 pursuant to POP No. 9 (Dames and Moore, 1988). Dames and Moore also excavated 23 test pits in July, 1989 to evaluate the nature of the fill material. The results are summarized in a report titled Final Report - Excavation of Test Pits (Dames and Moore, 1989).

A Baseline Risk Assessment (BRA) for the Site was conducted by Clement Associates (Clement, 1990) for the USEPA. The BRA followed USEPA guidance for conducting risk assessments current at the time and utilized the information primarily collected during the initial phase of the RI.

#### 2.2 1990 Record of Decision

On September 14, 1990, USEPA issued a Record of Decision (ROD) selecting an interim remedy for the FOU at the Site based on the Remedial Investigation, Feasibility Study, and the BRA. The ROD defined the FOU as "contaminated soils and groundwater above the clay layer" and the selected remedy comprised the following major elements:

- Installation of a slurry wall around the entire Site;
- Installation of an infiltration barrier over the Site;
- Installation of a groundwater collection system, and extraction of groundwater from the FOU zone; and
- Off-Site treatment and disposal of extracted groundwater.

USEPA determined that the selected Interim Remedy would "reduce the migration of hazardous substances, pollutants and contaminants out of the first operable unit zone" and be "consistent with an overall remedy which will attain the statutory requirement for protectiveness."

# 2.3 Interim Remedial Measures

The Interim Remedy was designed and implemented by the Group pursuant to an Administrative Order (Index No. II CERCLA - 00116) dated September 28, 1990. The Interim Remedy is illustrated in Figure 2 and consists of the following:

- 1. A lateral containment wall comprising a soil-bentonite slurry wall with an integral high density polyethylene (HDPE) vertical membrane which circumscribes the property;
- 2. A horizontal "infiltration barrier" consisting of high density polyethylene (HDPE) covering the property;

- 3. A sheet pile retaining wall along Peach Island Creek;
- 4. A groundwater extraction system for shallow groundwater consisting of 5 extraction wells screened in the fill which discharge to an above grade 10,000 gallon holding tank via an above grade header system; and
- 5. A chain link fence which circumscribes the Site.

The design of the Interim Remedy is presented in the Interim Remedy Remedial Design Report (Canonie, 1991) and construction was undertaken between August, 1991 and June, 1992. As part of the Interim Remedy design, 18 soil borings were conducted to evaluate subsurface conditions in the vicinity of the proposed slurry wall. The Interim Remedy construction is documented in the Final Report - Interim Remedy for First Operable Unit (Canonie, 1992).

The Interim Remedy has been in operation since June 1992 and extracted groundwater is regularly shipped, via tanker trucks, to the DuPont Environmental Treatment (DET) facility, located in Deepwater, New Jersey, for treatment and disposal. Between March 1993 and March 1994, the extraction system was not operational because of pump fouling by free phase product (Canonie, 1993).

Maintenance and monitoring of the Interim Remedy is conducted pursuant to the USEPA approved Operations and Maintenance Plan (Canonie, 1991). Quarterly Operations and Maintenance reports are submitted to USEPA which contain the following:

- 1. Summary of groundwater extraction from the FOU;
- 2. Summary of Site inspections and maintenance activities;
- 3. Groundwater levels; and
- 4. Groundwater and surface water quality results from the quarterly sampling program.

The monitoring program currently consists of thirteen groundwater monitoring wells (MW-2D, MW-2R, MW-5D, MW-7D, MW-8S, MW-8D, MW-9S, MW-10S, MW-11S, MW-11D, MW-12S, MW-12D, and RMW-13D) as shown on Figure 2 and four surface water sampling points in Peach Island Creek. In accordance with correspondence from USEPA dated June 30, 1995, samples are analyzed for Target Compound List (TCL) volatile organic compounds (VOCs) quarterly, and the Target Analyte List (TAL) and TCL compounds annually.

# 2.4 Regional Geology

The Site is located in the Piedmont Lowland physiographic province of Bergen County and is underlain by interbedded sedimentary and igneous rocks of the Triassic-Jurassic age Newark basin. The Site is situated in a lowland called the Hackensack Meadowlands, a large tidally influenced marsh drained by the Hackensack River and its tributaries which flow south to Newark Bay. The lowland is characterized by flat topography and underlain by the sedimentary rocks. More resistant igneous rocks form prominent northeast-trending strike ridges on either side of the lowland. Much of the original topography of the Hackensack Meadowlands was originally under several feet of tidal estuarine waters. Large portions of the estuary are now several feet above mean sea level as a result of extensive industrialization, landfilling and reclamation, and construction of major roadways including the New Jersey Turnpike. The regional geology is illustrated in Figure 3.

#### **Physiography**

The topography and surficial geology in the vicinity of the Site is largely a reflection of man-made fill and unconsolidated deposits related to the Wisconsinan stage glaciation which reached its maximum extent approximately 20,000 years ago during the Pleistocene Epoch (Stanford et al. 1993). Modern day, tidally influenced stream valleys have cut meandering channel networks within the lowlands and a vast array of narrow mosquito-abatement drainage trenches and ditches were cut into the surficial meadow mat during the early historical development of the Meadowlands (USEPA, 1993, Dames and Moore, 1989).

Bedrock outcrops are quite rare in the lowland because of an extensive mantle of unconsolidated glacial deposits and the present topography. The terminal Wisconsinan moraine which was located about 20 miles south of the site in Essex, Hudson and Monmouth counties, has influenced the development of the geologic conditions underlying the site. As the glaciers advanced south, existing drainage courses were modified by glacial erosion and deposition, and locally blocked by ice forming glacial lakes. Deep scoured preexisting bedrock valleys were infilled by the glacial deposits to the west of the Site. The north-south running Kenilworth bedrock valley was scoured down into bedrock to a depth of 250 feet below Mean Sea Level (MSL) and the Overpeck bedrock valley, trending almost parallel with the New Jersey Turnpike and the present day Hackensack River, is as much as 200 feet deep. The bedrock surface rises from the valley axes to a gently undulating, glacially smoothed interfluve surface which underlies most of the New Jersey Sports Complex and adjacent areas. The bedrock surface may locally rise to within 10 feet of the present

grade, or break through the lowland as isolated "islands", such as Laurel Hill. In the area of the Site, the bedrock occurs at an elevation of 30 feet to 50 feet below MSL. An almost continuous mantle of glacial till overlying the bedrock shows that the buried bedrock valleys, and the broad intervening interfluves were present prior to glaciation.

During the final, northward retreat of the glacial ice sheet, proglacial lakes dammed behind the terminal moraine inundated the lowlands. Glacial Lakes Hackensack and Bayonne formed about 15,000 years ago, at which time locally up to 200 feet of varved clays accumulated as seasonal (or varved) lacustrine sediments (Parillo, 1959, Stanford et al. 1995). Along the margins of these lakes, coarser grained silts, sands, gravels and occasional boulders were shed into the varved sediments from the surrounding ridges and dropped by floating icebergs. Glacial Lake Hackensack drained into the Atlantic Ocean about 10,000 years ago when the terminal moraine was breached, leaving behind a vast featureless lowland (Averill. et al. 1980).

About 4000 years ago, rising sea level and resultant marine incursions into northern New Jersey converted the lowlands into a vast salt marsh and tidal-flat, drained by the present day Passaic, Hackensack and Rahway Rivers

# **Stratigraphy**

In general terms, the stratigraphic sequence (Stanford et al., 1994; Averill et. al., 1980) in the Piedmont Lowland Physiographic Province from the youngest to the oldest geologic units can be subdivided as follows:

#### **Unconsolidated Deposits**

- Man-Made Fill: Consisting of a mixture of soil, sand and gravel, and significant quantities of varying sizes of debris.
- Marine and Marsh Sediments: Inter-tidal and Recent fluvial deposits: consisting of fluvial and estuarine sands, silts, clays and gravels overlain by the intertidal silts, clays, salt marsh and meadow-mat deposits;
- Glacial Deposits: consisting of stratified glaciolacustrine silts, silty clays and clays, often varved (including the older Glacial Lake Bayonne and younger, Glacial Lake Hackensack deposits), and outwash sands, silts and gravels; the stratified deposits generally overlie unstratified deposits which include glacial till (Rahway Till) and proglacial fan-delta deposits;
- Pre-glacial Deposits: consisting of sands, gravels and silts infilling buried bedrock valleys carved by the pre-glacial, ancestral Passaic and Hackensack rivers;

## Consolidated Deposits

 Bedrock: consisting of Triassic and Jurassic age, bedded, gently west-dipping, sandstones, siltstones, and conglomersates, interbedded with basalt lava flows and sills of the Newark Basin.

## 2.5 Regional Hydrogeology

Groundwater in this part of New Jersey is obtained from bedrock and the overlying unconsolidated deposits. The unconsolidated deposits consist of both Recent and Holocene age fluvial deposits, and the underlying glacial deposits. Bedrock aquifers are generally confined by the overlying mantle of unconsolidated deposits. The fluvial deposits, and the glacial deposits form unconfined, semi-confined, and locally confined aquifers. The extent and thickness of discrete water-producing beds within the bedrock aquifer is generally controlled by secondary porosity such as joints, bedding planes and an assortment of other fractures. The hydraulic properties of the bedrock aquifers have been described in detail by Herpers and Barksdale (1951).

The glacial deposits are divided into stratified and unstratified deposits and can form productive aquifers. The glacial deposits consist of boulders, gravel, sand, silt, and clay largely derived from the local bedrock. Glacial tills, when present, generally serve as confining beds to the underlying bedrock. In deeper portions of the glacially scoured bedrock valley, glacial aquifers are developed in the pre-glacial valley fill deposits which consist of moderately- to well-sorted silts, sands and gravels, having been transported by glacial meltwater streams.

Overlying these older glacial deposits are the stratified glaciolacustrine sediments consisting of laminated (varved) clays, silts, very fine-grained sands and occasional gravel. The lacustrine sediments may be described as regional confining beds. Sand and gravel deposited as deltas and fans in the glacial lakes may also locally overlie lake-bottom sediment, resulting in surficial, unconfined glacial aquifers. Recent age overbank flood plain silts and clays, and laterally discontinuous silts and clays of short-lived proglacial lakes may also locally act as confining beds.

## 3. OFF-PROPERTY INVESTIGATION FIELD WORK

The Investigation was initiated pursuant to the Agency approval of the Final Work Plan Amendment dated December 1995 and entailed the installation of ten monitoring wells; the completion of one deep bedrock pilot boring; borehole geophysical testing; hydrogeologic testing; groundwater quality sampling; and, long-term water level monitoring. All field activities were overseen by the USEPA oversight contractor ICF Kaiser.

Site investigations commenced with the deep bedrock pilot boring (MW-8R) on June 24, 1996. Monitoring well installation and development was completed on August 28, 1996. Borehole geophysical testing commenced on July 9, 1996 in the deep bedrock pilot boring and was subsequently completed on September 26, 1996 with the natural gamma and acoustic (cement-bonding) logging. Hydrogeologic testing commenced with the packer testing of the deep bedrock pilot borehole on July 11, 1996 and was completed on August 29, 1996 with the slug testing of the newly installed till monitoring wells. Groundwater sampling commenced on September 17, 1996 concurrent with the scheduled quarterly Operation & Maintenance (O&M) sampling program and was completed on September 24, 1996. Long-term water level monitoring commenced on October 3, 1996 and was completed on November 25, 1996.

The Site investigation used the following field instruments: Microtip-2000 Photo-ionization detector (PID) and Mini-Rae PID PGM-75 were used for VOC monitoring during the drilling program; Hydac 910 portable water quality meter (pH, temperature, and specific conductivity) and HF Scientific Model DRT-15 Portable Turbidity Meter for monitoring well development; and, Horiba U-10 portable water quality meter (pH, specific conductivity, turbidity, dissolved oxygen, and temperature), Hanna meter (eH), and YSI Dissolved Oxygen Meter for groundwater sampling. All instruments were calibrated, at a minimum, to the operations manual specifications prior to use each day.

Drilling and well installation services were provided by Aquifer Drilling & Testing - MidAtlantic, Inc. of Trenton, New Jersey. Laboratory services were provided by CompuChem Laboratories, Inc. of Chapel Hill, North Carolina and Accutest of Dayton, New Jersey. Borehole geophysical services for the natural gamma and acoustic logging were provided by COLOG, Inc. of Golden, Colorado. Surveying services were provided by GEOD Corporation of Newfoundland, New Jersey.

# 3.1 Monitoring Well Installation

A total of six till monitoring wells (MW-10D, MW-14D, MW-15D, MW-16D, MW-17D, and MW-18D) and four bedrock monitoring wells (MW-8R, MW-10R, MW-11R and MW-14R) were installed per sections 5.4.2 and 5.4.3 of the Work Plan.

Figure 2 illustrates the location of the monitoring wells and Table 1 summarizes the well construction. Appendix B includes boring and well installation logs and the New Jersey Department of Environmental Protection (NJDEP) Well Certifications-Form A (As-Built Certification) and Form B (Location Certification).

The following sections summarize the procedures used to drill, install and develop the monitoring wells.

## 3.1.1 Drilling Program

The drill rig, augers and drill stem, rig tools, and well materials were thoroughly steam cleaned upon arrival on-Site, between each borehole and prior to leaving the Site with potable water obtained from a water main located on-Site. A temporary decontamination pad was used to contain water generated from the steam cleaning operations. The water generated from the steam cleaning was disposed of in the on-Site 10,000 gallon leachate holding tank for subsequent off-Site disposal. Drill cuttings/mud generated from the steam cleaning was placed into DOT approved 55-gallon drums and staged on-Site for subsequent disposal.

#### Bedrock Pilot Borehole - MW-8R

The borehole for MW-8R was completed in several stages. First, a 14-inch diameter borehole was advanced 2 feet into the clay confining unit using hollow stem auger (HSA) drilling techniques. A 10-inch diameter steel casing was then driven 1-foot below the drilled borehole. The annulus between the borehole and the casing was grouted using cement-bentonite grout placed using the tremie method. After a minimum period of twelve hours, fluid within the casing was flushed out and a 9-5/8-inch borehole was advanced to the top of bedrock using HSA and wash rotary drilling techniques. The natural mud from the formations was used as the drilling fluid.

Soil samples were taken during drilling by driving a 2-inch outside diameter (OD) split-spoon sampler a distance of 2 feet at continuous intervals to refusal. Blow counts required to drive the

split-spoon each 6-inch increment were recorded. The total recovery of each sample was measured and the soil classified using the Unified Soils Classification System (USCS) based on visual description only. Soil samples were monitored for the potential presence of VOCs using a PID and readings were recorded on the boring log. A representative portion of each sample was placed in a glass jar and labeled for archive.

Refusal was encountered at 59 feet below ground surface (bgs) from which point further samples were obtained by coring with HQ diamond-bit core barrel with wireline setup. The core barrel seized up and lost circulation at 64 feet bgs. The borehole was augered to 65 feet bgs and drilled to 69 feet bgs using wash rotary. Rock coring resumed at 69 feet bgs and continued until 10 feet of competent bedrock (69 to 79 feet bgs) was cored. It should be noted that although coring began at 59 feet bgs bedrock was not actually encountered until 69 feet bgs. The corehole was then reamed using air rotary techniques (9-5/8-inch diameter borehole). A 6-inch steel casing was subsequently set within the reamed corehole and grouted with a cement-bentonite grout using the tremie method. After a minimum period of twelve hours, fluid within the casing was flushed out and the next 50 feet of bedrock was cored. Ten foot core runs were completed to a depth of 129 feet bgs. Borehole geophysics and packer testing were completed as described in Sections 3.2 and 3.3.

To complete the installation of monitoring well MW-8R, the cored borehole was grouted to a depth of 97 feet bgs with a cement-bentonite grout using the tremie method. After a minimum of 12 hours, the portion of the borehole between the bottom of the 6-inch steel casing and the top of grout was reamed to 5-5/8-inches in diameter using air rotary drilling techniques and an in-line filter. A 3 foot thick layer of filter sand (fine grained sand pack) was placed on top of the grout prior to the installation of the well screen and riser. Monitor well construction details are provided in Section 3.1.2.

#### **Bedrock Monitoring Wells**

The boreholes for bedrock monitoring wells MW-10R, MW-11R and MW-14R were also advanced in several stages using generally the same procedures as described above. Several deviations from the Work Plan were necessary based on the field conditions encountered which were approved in the field by ICF Kaiser. These modifications include:

• Monitoring well MW-10R was completed with 2-inch diameter stainless steel well screen and riser due to the poor rock quality; and

• Monitoring well MW-11R was triple cased consisting of 12-inch, 8-inch, and 4-inch steel casing to prevent possible cross-contamination. Contamination was encountered (based on visual and PID readings) at the following depths: 16 to 20 feet bgs and 27.5 feet bgs.

Drilling methods consisted of the following: hollow stem auger for the installation of the outer casings into the clay confining unit for all three monitoring wells; wash rotary to the top of bedrock with the exception of MW-10R in which air rotary was utilized for the installation of the inner casing; and coring followed by reaming using air rotary to complete the boreholes into bedrock for all three wells. The natural mud from the formations was used as the drilling fluid during wash rotary drilling. It should be noted that in all cases the outer casing was installed a minimum of 2 feet into the confining layer and to a depth at which no PID readings were measured on the soils.

# **Till Monitoring Wells**

The boreholes for monitoring wells MW-10D and MW-14D through MW-18D were advanced in several stages using the same general procedures as previously described. No significant modifications to the Work Plan drilling procedures were necessary.

Drilling methods consisted of the following: hollow stem auger for the installation of the outer casings into the clay confining unit for all six monitoring wells; HSA to top of bedrock at locations MW-15D and MW-16D; wash rotary to the top of bedrock at locations MW-10D, MW-17D, and MW-18D; and, air rotary to top of bedrock at location MW-14D. The natural mud from the formations was used as the drilling fluid during wash rotary drilling, except for MW-14D in which bentonite was added to keep the borehole open for well installation. The top 5 feet of bedrock was cored at locations MW-15D and MW-16D to confirm the top of bedrock (at all other locations an adjacent bedrock corehole existed to confirm bedrock elevation).

Drill cuttings and fluids were placed into DOT approved 55-gallon drums and labeled and staged on-Site for subsequent disposal.

# 3.1.2 Well Installation

Monitoring wells MW-10D and MW-14D through MW-18D were constructed with 4-inch internal diameter well screens and risers and monitoring wells MW-8R and MW-10R were constructed with 2-inch internal diameter well screen and riser. All screens and risers were flush threaded, Schedule 5, Type 304 stainless steel. Well screens were continuous wrap No. 10 slot (0.010-inch). Bedrock monitoring wells MW-11R and MW-14R were completed as open coreholes.

Monitoring wells MW-10D and MW-14D through MW-18D were constructed to provide data from groundwater within the till unit. It should be noted that the original intention of monitoring well MW-18D was to provide data from groundwater within the weathered bedrock zone. However, the pilot bedrock boring (and the other bedrock wells) did not encounter a weathered rock zone. Therefore, monitoring well MW-18D was completed within the lower portion of the till unit.

As per the Work Plan, each till well was to be screened within the most contaminated zone based on PID readings and visual observations during drilling. If no elevated readings and/or visual contamination was observed, the most permeable zone (based on visual assessment of split spoon samples) was to be screened with a maximum screen length of 10 feet. No elevated PID readings and/or visual contamination was observed within the till unit during the drilling of each borehole. The following provides a summary of the resulting till well construction details:

- A 2-foot well screen was used in the construction of monitoring well MW-15D due to the presence of only 6.5 feet thickness of the till unit;
- A 5-foot well screen was used in construction of monitoring wells MW-10D and MW-16D based on a till thickness of 10 and 14 feet, respectively. Although a 10-foot well screen might have been used for monitoring well MW-16D, it was decided to use only a 5-foot well screen in order to ensure there was isolation from the underlying bedrock and the overlying varved clay unit. As such, the well screen was placed across the more permeable portion of the till unit which had a thickness of only 6.5 feet.
- A 10-foot well screen was used in construction of monitoring wells MW-14D and MW-17D. Monitoring well MW-14D was screened from 40 to 30 feet bgs in order to monitor a medium to coarse sand lense encountered from 33.5 to 35 feet bgs. Monitoring well MW-17D was screened from 45 to 55 feet bgs within a portion of the till unit visually identified as being more permeable. Additionally, as no weathered bedrock was encountered, monitoring well MW-18D was installed at depth of 62 to 67 feet bgs to provide additional coverage of the till unit which had a thickness of 31 feet at this location.

Bedrock monitoring wells MW-8R and MW-14R were constructed in accordance with the Work Plan. The construction of MW-10R and MW-11R was modified as described in Section 3.1.1.

All wells, except MW-11R, were completed with 12-inch diameter steel protective flushmount casing. Monitoring well MW-11R was completed with a 24-inch flushmount square vault.

The construction details of each well (total depth, length of well screen, screen interval, and thickness of sand pack) were discussed and approved in the field by ICF Kaiser prior to well installation.

# 3.1.3 Well Development

Following installation, each well was developed using a combination of a Grundfos Redi-Flo 2 or 3 inch JetSub submersible pump and a surge block. A sand bucket and bailer was initially used to assist with the development of monitoring well MW-15D due to excessive siltation which precluded the initial use of a submersible pump.

Well development forms are presented in Appendix C. The well development procedure and completion of development at each well was approved in the field by ICF Kaiser. The procedure generally involved initially pumping one well volume and then hand surging for approximately five minutes. This procedure was repeated until no further significant improvement was observed through the monitoring of field parameters (turbidity, pH, and conductivity). In addition, approximately two times the volume of water lost in the borehole during coring was removed from bedrock wells MW-10R and MW-11R.

Development water was contained and allowed to settle prior to discharge into the on-Site 10,000 gallon holding tank for subsequent off-Site disposal.

#### 3.1.4 Well Decommissioning

Although not originally part of this Investigation, monitoring well MW-13D, which was replaced with monitoring well RMW-13D in October 1995, was decommissioned on August 11, 1996 in accordance with N.J.A.C. 7:9-9.1 et. seq. and USEPA's letter dated April 5, 1996. The abandonment procedure was approved in the field by ICF Kaiser. The procedure included removing the flush mount casing and driving a split-spoon sampler through the bottom of the well screen in order to remove the well screen and riser. After unsuccessfully attempting to remove the well screen and riser, the well was sealed in place with a cement/bentonite grout using a pressure grout hose placed at the bottom of the well. After the well was sufficiently sealed, the area in which the flushmount casing had been removed was patched with an asphalt material. The well decommissioning form is presented in Appendix A.

# 3.2 Hydrogeologic Testing

Estimates of horizontal hydraulic conductivity, hydraulic head and potential groundwater flow zones were obtained by conducting packer tests in cored borehole MW-8R. Estimates of horizontal hydraulic conductivity were also obtained by conducting packer tests in cored boreholes MW-11R

and MW-14R. Originally, a packer test was to be completed in cored borehole MW-10R. However, due to the poor quality of the bedrock (low rock quality designation (RQD)), the installation of a stainless steel well screen and riser was necessary in order to keep the borehole open for subsequent groundwater sampling events. Therefore, a rising head slug test was performed at this location. Packer testing commenced on July 11, 1996 at location MW-8R and was completed on August 28, 1996 at locations MW-11R and MW-14R. Details of the packer testing procedures and results are presented in Appendix D and results are discussed in Section 4.0.

Rising head tests were performed in monitoring wells MW-10D, MW-10R, and MW-14D through MW-18D on August 28 and 29, 1996. Details of the testing procedures and results are presented in Appendix D and results are discussed in Section 4.0.

Decontamination of the packer tools, pressure transducers, and submersible pump was performed upon arrival on-Site, between each monitoring well and prior to leaving the Site, following the procedure outlined in the Work Plan.

## 3.3 Geophysical Testing

Geophysical testing was completed in two phases. The first phase included downhole velocity survey, caliper log, and temperature log in the pilot borehole; and, downhole velocity and downhole camera survey in MW-2D, MW-2R, MW-5D, MW-7D, and MW-11D. This phase of the work commenced on July 9 and was completed on July 11, 1996. As discussed in a letter to the USEPA dated September 17, 1996, a downhole velocity survey was not performed in monitoring well MW-11D due to the presence of NAPL. The first phase of geophysical testing was performed by Golder Associates.

The second phase of the geophysical testing was completed by COLOG, Inc. Acoustic (cement bonding) and natural gamma logging was performed on existing monitoring wells MW-2D, MW-2R, MW-5D, MW-7D, and MW-11D and newly installed monitoring wells MW-14D and MW-18D. This work was performed on September 25 and 26, 1996. Details of the procedures and results are presented in Appendix E and are discussed in Section 4.0.

Decontamination of the geophysical instruments was performed upon arrival on-Site, between each monitoring well and prior to leaving the Site, following the procedure outlined in the Work Plan.

# 3.4 Groundwater Sampling

The groundwater sampling program included one round of sampling from the newly installed groundwater monitoring wells using the low flow purge technique. Sampling locations are shown in Figure 2, a sampling and analyses summary is provided in Table 2, summary tables of the purging data are presented in Appendix F and the Chain-of-Custody forms are included in Appendix G. The analytical results are presented in Section 4.0. All water generated during purging was collected and discharged into the on-Site 10,000 gallon holding tank for subsequent off-Site disposal.

Groundwater sampling was performed between September 17, 1996 and September 24, 1996 and was conducted concurrent with the scheduled quarterly O&M sampling. Groundwater sampling as part of the Investigation included till wells MW-10D and MW-14D through MW-18D, and the bedrock wells MW-8R, MW-10R, MW-11R, and MW-14R. In addition, a sample of the water source used during the drilling investigation was collected directly from the garden hose used to fill the water tanks for drilling and steam cleaning. It should be noted that the Work Plan allowed for the possibility of collecting a second groundwater sample in monitoring wells MW-5D, MW-7D, and MW-11D from a zone other than the middle of the well screen if discrete flow zones were determined based on the downhole velocity meter survey. The second samples were not collected based on the geophysical results as conveyed to the USEPA in a letter from Golder Associates dated September 17, 1996 and subsequently approved.

Groundwater samples and the potable water sample (PW-01) were analyzed for target compound list (TCL) and target analyte list (TAL) constituents plus cyanide in accordance with the Work Plan. As described in a letter from Golder Associates dated September 17, 1996 to USEPA, additional indicator parameters were also analyzed comprising alkalinity, sulfate, sulfide, methane, ethane, ethene, total organic carbon, chloride, dissolved iron, nitrogen, nitrate, nitrite, and phosphorus.

Well purging and sampling procedures for the low flow purge and sampling technique for the monitoring wells were conducted in general conformance with the Work Plan and with the concurrence with the USEPA oversight contractor ICF Kaiser. Water was purged from each well prior to sampling using a stainless steel Grundfos Redi-Flo 2 submersible pump. Prior to purging and sampling each well, the submersible pump was decontaminated following procedure #2 as set out in Appendix B, Section 6.0 of the Work Plan. Dedicated decontaminated teflon lined

polyethylene tubing was installed in each of the monitoring wells with the exception of monitoring well MW-11D (due to the presence of NAPL in this well). A length of tubing was connected to the submersible pump and the pump was carefully lowered down each well until the bottom rested at the approximate mid-point of the screened interval. Attempts were made to keep the submersible pump from resting on the bottom of the well to minimize the disturbance of any sediment which may have accumulated. The tubing was connected to a flow-through cell into which the portable water quality meter probes were placed for monitoring indicator parameters. The purge and sample depth of each well is summarized in Table 2.

The submersible pump was used to purge and sample water from the well at very low flow rates (approximately 85-1200 ml/min. depending on the well yield). Temperature, pH, eH, specific conductance, turbidity, and dissolved oxygen were monitored continuously as indicator parameters. In addition, water levels were continuously monitored. Once the indicator parameters stabilized to within  $\pm 10\%$ , over a minimum of two consecutive readings, the water level had stabilized, and a minimum of one volume of the tubing had been removed, the well was considered adequately purged and ready to be sampled. The tubing was then disconnected from the flow-through cell and the pumping rate reduced to approximately 100 ml/min (or lowest achievable pumping rate) prior to sampling. Samples were collected directly from the tubing using the submersible pump.

Quality assurance/quality control (QA/QC) samples were collected to monitor the quality and integrity of the field and laboratory techniques. Six trip blanks (one per day of sampling for volatile organic compounds), two field duplicates at locations MW-14R (MW-14RD) and MW-18D (MW-18DD); six field rinsate blanks (RBGW-01 through RBGW-06); and an MS/MSD (triple volume) at locations MW-2R and MW-11R were collected. The field rinsate blanks included one sample collected per equipment type used for the decontamination event, including one sample per day for the submersible pump. Additionally, ICF Kaiser collected a split sample at location MW-18D and one rinsate blank.

# 3.5 Analytical Testing and Validation

Groundwater samples were analyzed for TCL and TAL parameters by CompuChem Laboratories and for additional indicator parameters by Accutest. Specific conductance, temperature, pH, eH, dissolved oxygen, and turbidity were measured in the field by Golder Associates personnel. The analytical methods for TCL/TAL and indicator parameters are outlined in Table 2.

Strict quality assurance and quality control (QA/QC) measures were taken to ensure sample integrity and to maintain confidence in the resultant data as described below:

- 1. **Sampling Techniques:** Dedicated teflon lined polyethylene tubing for all monitoring wells and rigorous decontamination of the submersible pump in accordance with procedure #2 as specified in Appendix B, Section 6.0 of the Work Plan.
- 2. **Sampling Containers:** The container type and size were used as specified in the Work Plan for compatibility with the sample media and analyte. Aqueous samples were preserved in accordance with the Work Plan.
- 3. Samples: Numerous quality assurance and control samples were taken during sampling consisting of trip blanks, field rinsate blanks, field blind duplicates, and MS/MSDs. In addition, sample splits were collected by the USEPA oversight contractor. Trip blanks were prepared each day when taking an aqueous sample for volatile organic analysis. Field rinsate blanks were prepared each day for each type of sampling equipment used. Field duplicates were taken at a frequency of one per 20 samples. MS/MSD samples were prepared in triple volume at a frequency of one per 20 samples. A summary of the QA/QC samples is given in Table 2.
- 4. **Documentation:** Documentation of the sampling event consisted of chain of custody forms and field sampling logs or Sample Information Collection forms.
- 5. **Laboratory:** The QA/QC procedures for CompuChem were followed as presented in the Work Plan.

All data was validated in accordance with the appropriate USEPA Region II Standard Operating Procedure as outlined in the Work Plan. Narratives discussing the results of the data validation for the newly installed monitoring wells are included in Appendix H.

## 3.6 Water Level Monitoring

Synoptic and continuous groundwater and surface water level measurements were collected during the Investigation to assess variation in groundwater and surface water levels and to evaluate tidal and other influences at the Site.

Synoptic groundwater level measurements were collected from all monitoring wells using a electronic water level meter on September 17, 1996. The water level meter was field decontaminated prior to each use by rinsing the probe with distilled water. Measurements to the depth of water were made in each monitoring well to the nearest 0.01 foot relative to a survey mark at the top of the inner casing. This measurement was converted to a water level elevation based upon the surveyed elevation of the inner casing.

Continuous long-term water level measurements were collected from a total of 12 monitoring wells for a duration of approximately seven weeks between October 3, 1996 and November 25, 1996 using In-Situ TROLL® SP2000 pressure transducers and data loggers. The pressure transducers and data loggers were field decontaminated and installed below the water table in monitoring wells MW-2D, MW-2R, MW-5D, MW-7D, MW-8R, MW-10D, MW-10R, MW-11R, MW-14D, MW-14R, MW-16D, and MW-17D. Additionally, one pressure transducer and data logger was placed in a stilling well (PIC) in Peach Island Creek immediately adjacent to the Site to monitor creek level fluctuations. The depth to water was manually confirmed at each location with an electronic water level meter before installing and removing the logging equipment. Water level information was collected automatically at 1 hour intervals over approximately seven weeks. It should be noted that slight modifications to the water level monitoring program were implemented to enhance the program based upon information obtained during the drilling program. The modifications were discussed in a letter from Golder Associates to the USEPA dated September 17, 1996 which was subsequently approved.

The results from the continuous water level measurements are presented in Appendix I and are discussed in Section 4.0.

## 4. OFF-PROPERTY INVESTIGATION RESULTS

## 4.1 Site Geology

The subsurface interpretation presented here is based on previously completed investigations at the Site and off-Property (Dames and Moore, 1989; Canonie, 1990; Golder, 1995) and data obtained during the present Investigation. The stratigraphy at the Site consists of the following units, from youngest to oldest:

- 1. Man-Made Fill;
- 2. Marine and Marsh Sediments;
- 3. Glaciolacustrine Varved Deposits;
- 4. Glacial Till; and
- 5. Bedrock.

All subsurface units directly over bedrock, including man-made fill, are considered in this Report as overburden. These overburden units are unconsolidated, and generally flat lying. A brief description of each geologic unit is provided below, a conceptual block diagram of the Site geology is presented as Figure 4, and geological/hydrogeologic cross-sections are presented on Figure 5.

#### 4.1.1 Man-Made Fill Unit

The unit directly underlying the site area consists of miscellaneous man-made fill material. The fill is about 3 feet thick near Peach Island Creek and increases to about 11 feet near Paterson Plank Road. At the Site, the miscellaneous fill consists of a mixture of soil, sand and gravel, and substantial quantities of varying sizes of construction and demolition debris, asphalt, steel girders, wire, concrete blocks, bricks, timber, etc. The variable composition results in a highly erratic response to split spoon penetration as shown by the variation in the Standard Penetration Test (SPT) blow counts.

#### 4.1.2 Marine and Marsh Unit

A "meadow mat" or peat, organic silt and clay intermixed with sand is the youngest natural material underlying the Site. The peat is of variable thickness ranging from 0 (e.g., MW-12D and RMW-13D) to as much as 7 feet near Peach Island Creek. The varying thickness of the peat layer may be due to uneven loading or placement of the fill, localized scouring by modern-day streams, or previous site operations. SPT blow counts are highly variable, ranging from no penetration resistance to as much as 15 where sand stringers are present with the unit.

The base of the peat unit presents a sharp, well defined contact with an organic gray fine-sand, and silt layer that is correlatable with similar deposits across the Hackensack and adjacent lowlands. SPT blow counts range from 5 to as much as 23 in sandier portions or where it grades downward into gravel-bearing interbeds. It is distinguished from the overlying peat unit by color and texture, and highly mottled character.

#### 4.1.3 Glaciolacustrine Varved Unit

The youngest glacial deposits intercepted are of glaciolacustrine origin, herein referred to as the glaciolacustrine varved unit. The glaciolacustrine varved unit can be correlated with the varved silts, and silty clays of Glacial Lake Hackensack, although the lower portions may belong to the Glacial Lake Bayonne stage (see Stanford and Harper, 1991). Based on the present Investigation, this unit has been broadly subdivided into the following horizons:

- a. An upper, stiff to medium stiff, bedded, varved horizon which is significantly sandier than the lower horizon. This horizon also displays distinct banding by stringers and intercalation of silty sand and silt.
- b. A lower, very soft to soft, highly plastic clayey horizon. This horizon consists of a clayey silt to massive clay, wherein the varved nature is more difficult to recognize because of the higher clay content.

The boundary between these two horizons is sharp, recognizable by a marked drop in the SPT blow counts when the lower horizon is encountered. Additionally, the upper horizon is generally lighter reddish brown in color with local variagated tones that may be grayish, brownish gray or gray with distinct alternating seams and stringers of fine sand and silt. The lower horizon is characteristically brown, brick red to purple in color and is characterized by silty clay and clay. At several locations, such as at MW-11D and MW-12D, a basal sand and gravel intercalation has been reported, and at MW-2D a local zone of silty-sand with trace gravel was encountered in the middle portion of the varved unit.

Based on a review of the published literature, the elevation across the site, and the lithologic character, the two horizons may be considered to be different facies (Stanford, 1994) of glaciolacustrine deposition, and/or the result of weathering and desiccation of the upper zone glaciolacustrine deposits in the Hackensack lowlands (Averill et al. 1980, Argon, 1980, Harris, 1972).

The glaciolacustrine unit ranges in thickness from 0 feet (south corner of the Site) to about 28 feet (near Peach Island Creek). The geotechnical properties, particularly the SPT blow counts are distinctly different between the two horizons. The SPT blow counts are generally lower than 2 in the lower horizon. The uniform lithology and plastic nature of the fat clay precludes recognition of varves in some portions of the lower horizon. The upper horizon is generally stiffer with blow counts as high as 24, indicating a generally coarser texture with intercalated seams of silt and sand, and possibly desiccation (see Averill et al. 1980, Harris, 1972). No evidence of desiccation was noted during the present subsurface investigation, other than the variagated coloration mentioned above.

The top surface of the lower clay horizon surface, as shown on Figure 6, is gently undulating and rises to an elevation of about -6 feet MSL in the central area of the Site (-5.4 feet MSL at MW-2R). The lower horizon surface falls in elevation in each direction from this point. In the eastern part of the Site, a north-trending trough is evident along MW-8D, MW-7D (top of lower horizon at -10.9 feet MSL), and MW-14R (elevation -10.6 feet MSL). The top of the lower clay horizon also falls to the west to a low centered at MW-11D (elevation -13.6 feet MSL). Neither the upper horizon nor the lower horizon were intercepted at the location of B-6 and B-7 located in the south corner of the Site (Canonie, 1990). Based on a review of the data on the underlying Glacial Till unit (see section below), it appears that the Glaciolacustrine Varved sediments may not have been deposited in this area, as a result of a higher glacial till elevation than the level of glacial lake sedimentation. The pattern of thickness variation of the lower horizon corresponds to the undulation of the top of the underlying Glacial Till. In broad terms, the lower horizon is thinner (or absent) along a northwest trending zone parallel with B-6, B-7, MW-2R (7.3 feet thick), and MW-11R (8 feet thick). Its thickness increases both to the southwest (16 feet in thickness at MW-10D), east (11 feet thick at RMW-13D, 11.3 feet thick at MW-14D), and it is 18 feet thick at MW-7D and 21.7 feet thick at MW-8R northeast of the thin-zone mentioned above.

# 4.1.4 Glacial Till Unit

Informally correlated with the Rahway Till (Stanford et al, 1994), this unit consists of a heterogeneous mixture of red, yellow-brown, reddish-brown, and reddish-gray clay, silt, sand, and gravel. The glacial till is generally considered to be massive, however, the SPT blow counts recorded for the glacial till unit are highly variable. At several locations (see Figure 5) a softer glacial till has been recognized to overlie a much harder, overconsolidated glacial till. At other

locations (see cross section A-A' at MW-12D and MW-8D, and cross section B-B' at MW-15D) the softer till horizon has not been intercepted. The overconsolidated glacial till is a distinct horizon which is characteristic of a basal, lodgement till (see Lutenegger et al. 1983; Averill et al. 1980). SPT blow counts range from 60 up to 200. The softer till displays significantly lower blow counts, ranging from 20 to 30.

Based on the above observations the glacial tills beneath the Site can be subdivided as follows:

- a. The upper horizon of the Glacial Till unit is herein informally called the *Soft Till* and ranges in thickness from 0 to 11 feet; and
- b. The overconsolidated lower horizon is called the *Lodgement Till* and ranges in thickness from 2 to 30 feet.

The Lodgement Till displays a composition which is similar to the bedrock with clasts entirely composed of the underlying siltstone or sandstone, set in a clayey silt or silty clay matrix. In the Soft Till, however, the clasts may also include metamorphic rock fragments such as quartzite and gneiss and occasional well rounded to subrounded quartzite gravel.

#### 4.1.5 Bedrock Unit

The bedrock beneath the Site area has been assigned to the siltstone-mudstone-sandstone facies of the Passaic Formation (Parker, 1994). It consists of fining-upward sequences of intercalated massive siltstone and mudstone and laminated siltstone with occasional interbeds of micaceous, fine to medium grained sandstone. The bedrock is brick red, reddish brown or brown in color, and this coloration dominates all overlying glacial deposits. Distinctly cross-bedded and ripple laminated, fissile siltstone horizons occur dispersed throughout the unit. Nodules of carbonate (dolomite and calcite) are common throughout the mudstones and siltstones, and in the latter, bedding plane partings and hairline fractures are commonly coated with carbonate deposits. Discrete beds bearing the carbonate material have been selectively dissolutioned, resulting in poor rock quality (reflected in RQD indices less than 15%). These horizons with vugs and open cavities where the carbonate material has been dissolved serve as water-bearing zones in the bedrock.

Very few vertical fractures have been intercepted in the off-Property boreholes. Bedding plane partings are open if the carbonate material has been dissolved. Occasionally fractures at angles

with the bedding plane have also been intercepted. Bedding plane dip as determined in all the rock cores collected is essentially sub-horizontal.

## 4.2 Site Hydrogeology

#### 4.2.1 Continuous Water level Measurements

Continuous water level measurements were recorded in till monitoring wells MW-2D, MW-5D, MW-7D, MW-10D, MW-14D, MW-16D, and MW-17D, bedrock monitoring wells MW-2R, MW-8R, MW-10R, MW-11R, and MW-14R, and Peach Island Creek at location PIC. Water levels were monitored hourly for a period of seven weeks. Appendix I presents charts showing groundwater elevation versus time.

A seven-day cycle of fluctuations was generally recorded for all till wells and bedrock monitoring wells. In general, it appears that the high water levels were recorded on Mondays, while the lowest levels were generally recorded on Friday/Saturdays. This observation indicates that the water levels may be influenced by an extraction well(s) operating during the week and idling on the weekends. Additionally, an approximate 12-hour fluctuation was also recorded in till monitoring wells MW-2D, MW-5D, MW-14D, and MW-16D and all bedrock monitoring wells which coincides with fluctuations observed from the data collected from the stilling well (PIC) located in Peach Island Creek. The remaining till monitoring wells, MW-7D, MW-10D, and MW-17D do not clearly exhibit this fluctuation.

#### 4.2.2 Groundwater Flow Direction

Interpreted groundwater contour maps were constructed using only the monitoring wells that were part of the long term monitoring program in order to use truly synoptic water levels avoiding the effect of the seven-day and 12-hour fluctuations observed. Based on a number of groundwater contour maps developed using data from different time intervals (e.g. during high and low tide and various plots from Monday through Saturday) it is apparent that the 12-hour tidal fluctuation does not significantly affect groundwater flow direction. However, the weekly variations do impact flow directions. Groundwater maps for both units using water levels recorded on specific Mondays and Fridays are presented on Figures 7 and 8. Additionally, because only a select number of till wells were equipped with continuous water level recorders, manual water levels were collected from additional till wells to provide additional coverage on Friday November 22, 1996. The manual

water levels were collected over as short a time as possible corresponding to the measurement time of the automatic recorders.

## Till Unit

The potentiometric surface on Mondays indicates that the groundwater flow direction is towards the west/northwest and on Fridays trends towards the north.

# **Bedrock Unit**

The potentiometric surface on Monday, October 14, 1996 indicates that the groundwater flow direction is towards the northwest. The potentiometric surface on the other dates shown indicates an overall general trend towards the north.

## 4.2.3 Hydraulic Gradients

Based on the groundwater contour maps, horizontal hydraulic gradients, average approximately  $1 \times 10^{-3}$  ft./ft. for the till unit and  $6 \times 10^{-4}$  ft./ft. for the bedrock unit.

The vertical hydraulic gradients between the clustered monitoring wells are illustrated in Appendix I. As indicated by the charts, vertical gradients between the till and bedrock units at well clusters MW-10D/MW-10R and MW-2D/MW-2R are variable and indicate slightly upward and slightly downward gradients at differing times. The data for well cluster MW-17D/MW-8R indicates slightly downward gradients until the last week of monitoring during which the potentiometric surfaces for the two units are essentially equal. Slightly downward gradients are observed at well cluster MW-14D/MW-14R during most of the monitoring.

## 4.2.4 Hydraulic Conductivity

Hydrogeologic testing (packer and slug testing) to estimate horizontal hydraulic conductivity was completed in all wells installed as part of the Investigation. The analysis sheets and tables of data collected during the field program are presented in Appendix D. A summary of the results of the hydraulic conductivity testing is presented in Table 3. The till hydraulic conductivities range from 3.2x10<sup>-6</sup> cm/s (0.009 ft./day) at location MW-10D to 7.1x10<sup>-4</sup> cm/s (2.01 ft./day) at location MW-16D with a geometric mean value of 7.0x10<sup>-5</sup> cm/s (0.2 ft./day). The bedrock hydraulic conductivities range from 3.1x10<sup>-5</sup> cm/s (0.087 ft./day) at location MW-8R to 1.2x10<sup>-2</sup> cm/s (33.17 ft./day) at location MW-11R with a geometric mean value of 4.3x10<sup>-4</sup> cm/s (1.23 ft./day).

## 4.2.5 Groundwater Flow Velocity

An estimate of average linear groundwater flow velocity (v) was made using the following equation:

$$\overline{v} = \frac{ki}{n}$$

where:

k = 0.20 ft./day, the estimated geometric mean of hydraulic conductivity in till unit and 1.23 ft./day for the bedrock unit;
 i = 0.001 ft/ft, average horizontal hydraulic gradient for the till unit and 0.0006 ft/ft for the bedrock unit; and,
 n = 10% estimated porosity for a glacial till (Fetter, 1980) and 5% for fractured bedrock (Freeze and Cherry, 1979).

The resulting estimation of the average linear groundwater flow velocity for the till unit is 0.002 ft./day (0.73 ft./year) and 0.015 ft./day (5.4 ft./year) for the bedrock unit. It should be noted that the linear velocity predicted in this way is based on a uniform porous medium approximation and may not accurately predict fracture controlled velocities within the bedrock units.

# 4.3 Borehole Geophysical Results

As stated previously, the geophysical investigation was completed in two phases. The first phase was completed by Golder Associates personnel from July 9 through July 11, 1996 and consisted of downhole video, caliper (borehole diameter), and heat pulse flowmeter measurements. The second phase of the investigation was performed by Colog Inc. of Golden Colorado under the supervision of Golder personnel. Testing for the second phase included cement bonding and natural gamma tests to confirm well construction and determine the quality of the grout seals. This testing was performed on September 15 and September 16, 1996.

## Downhole Video, Caliper, and Heat Pulse Flowmeter

The downhole video survey was performed to inspect the well screens and casings in the screened wells, to inspect the open interval of well MW-2R, and to confirm the well construction of the wells. The downhole video survey of wells MW-2D, MW-2R, MW-5D, and MW-7D indicated that the well construction diagrams for these well were consistent with the actual conditions. The video camera survey of MW-11D confirmed the presence of NAPL in the well and suggested that the top of the well screen was at an elevation approximately 1 foot higher than the well construction

diagram indicates. The downhole video of the open borehole portion of well MW-2R indicated bedrock visually similar to that of MW-8R.

The results of the caliper testing of wells MW-2D, MW-5D, and MW-7D indicated that the well construction diagrams for these well were consistent with the actual conditions. The caliper test on well MW-2R borehole indicated that there were no substantial cave-ins within the open interval.

The purpose of the heat pulse flowmeter testing was to identify any zones of preferential flow of groundwater within the screened intervals of wells MW-5D, MW-7D, MW-11D, and borehole MW-8R. As discussed previously in a letter from Golder Associates to the USEPA dated September 17, 1996, a downhole velocity survey was not performed in monitoring well MW-11D due to the presence of NAPL. The results of the tests in the other wells indicated that there were no significant flow contrasts within the screened intervals of these wells. Heat pulse flow meter testing was also performed in MW-8R prior to packer testing. The results of the survey indicated a few zones of vertical gradients and these potential flow zones were individually tested by isolating them with the straddle packer tool. The results are presented in Appendix E.

# **Cement Bonding and Natural Gamma**

The cement bonding and natural gamma tests were run on previously installed wells MW-2D, MW-2R, MW-5D, MW-7D, and MW-11D and newly installed monitoring wells MW-14D and MW-18D. These tests were conducted to assess the integrity of the grout in all of the wells and the extent of the bentonite seals in the previously installed wells.

Cement bond integrity is determined using a full waveform sonic logging probe. The downhole probe emits sonic waveforms and a downhole receiver records the sounds reflected from the casing. Unbonded casing tends to ring with a smooth, high amplitude acoustic wave response while bonded casing gives a more muffled response. The grout integrity can be determined by evaluating the amplitude and travel time of the response.

The results of the cement bonding and natural gamma testing are presented in Appendix E. The results indicate that the grout integrity is highly variable with depth. Greater than 60% of the grout of wells MW-5D, MW-7D, MW-11D, MW-14D, and MW-18D is classified as having "Good" integrity. At least 60% of the grout of well MW-2D was classified as either "Fair-Poor" or "Poor". Only 6% of the grout of well MW-2R was classified as having "Good" integrity and this interval

was near the ground surface. 74% of the grout of MW-2R, including the bottom 30 feet, was classified as having "Poor" integrity. Poor grout integrity, especially at the till/bedrock interface could provide a pathway for vertical migration of contaminants.

The natural gamma testing indicated that bentonite seals are present in wells MW-2D, MW-5D, MW-7D, and MW-11D and their locations are generally similar to those indicated in the well construction diagrams.

# 4.4 Summary of Groundwater Analytical Results

The groundwater chemistry data is presented in Appendix J. A summary of TCL/TAL and cyanide detections is presented on Table 4. The groundwater data was compared to the New Jersey Groundwater Quality Standards (GWQS) adopted January 7, 1993 pursuant to N.J.A.C 7:9-6. Exceedances for those constituents for which a criteria is given are shown on Figures 9 (till unit) and 10 (bedrock unit). As discussed previously, the monitoring wells installed as part of the present Investigation were sampled concurrent with the existing monitoring wells that are sampled as part of the O&M program. Therefore, a summary of the O&M data collected from till and bedrock monitoring wells as presented in the Quarterly Operations and Maintenance Report (Golder Associates, 1996) is also included below and on Table 4 and Figures 9 and 10 for completeness.

## Off-Property Investigation Monitoring Wells

The off-Property investigation wells consist of six till monitoring wells (MW-10D, MW-14D and MW-15D through MW-18D) and four bedrock monitoring wells (MW-8R, MW-10R, MW-11R, and MW-14R).

## Till Monitoring Wells

VOCs were detected below the GWQS in four of the six till wells. There were no detections of VOCs in monitoring wells MW-15D and MW-17D and only one constituent was detected in wells MW-10D and MW-18D; in both cases at concentrations below the GWQS. There were no detections in the duplicate sample for MW-18D. Chloroform was detected at 3 ug/l at location MW-10D and methylene chloride at 1 ug/l at location MW-18D. For the remaining two monitoring wells, MW-14D and MW-16D, total VOCs were detected at a concentration of 65 ug/l and 151 ug/l, respectively. Tetratchloroethene and trichloroethene were detected at concentrations above the GWQS at location MW-14D and 1,1-dichloroethene, 1,2-dichloroethane, tetrachloroethene, and trichloroethene were detected at concentrations above the GWQS at location MW-16D. Total

VOCs in the potable water sample (PW-01) were detected at a concentration of 34 ug/l with chloroform and bromodichloromethane exceeding the GWQS.

Semi-volatile organic compounds (SVOCs) and pesticide/PCBs were not detected in five of the six till wells. Bis(2-ethylhexyl)phthalate was the only SVOC constituent detected at a concentration of 1 ug/l at location MW-16D. 4,4-DDE, endosulfan II, and endrine aldehyde were detected at concentrations of 0.1 ug/l, 0.1 ug.l, and 0.013 ug/l at location MW-15D, respectively. No SVOCs or pesticide/PCBs were detected in the potable water sample PW-01.

The total metals analyses indicated very few metals exceeded the GWQS with the exception of aluminum (five wells and the potable water sample) and sodium (six wells). Chromium was detected in samples MW-10D and MW-14D above the GWQS at concentrations of 373 and 434 ug/l, respectively. Manganese was detected in samples MW-17D and MW-18D above the GWQS at concentrations of 1,360 and 318 ug/l, respectively. Iron was detected at a concentration of 945 ug/l at location MW-17D. Cyanide was detected in only one sample, MW-14D, at a concentration of 10.9 ug/l which is well below the GWQS of 200 ug/l.

# Bedrock Monitoring Wells

Total VOC concentrations ranged from 1 ug/l (MW-14R) to 155 ug/l (MW-11R) with exceedances of the GWQS in samples MW-10R and MW-11R. Chloroform was detected at a concentration of 7 ug/l at location MW-10R which is slightly above the GWQS, although it should be noted that chloroform was also detected in the potable water sample PW-01. Chloroform, 1,1-dichloroethene, 1,2-dichloroethane, tetrachloroethene, and trichloroethene were detected at concentrations above the GWQS in sample MW-11R.

SVOCs were not detected in MW-8R and MW-10R. Phenol was detected at a concentration of 19 ug/l in sample MW-11R and pyrene at a concentration of 1 ug/l in sample MW-14R, both of which are each below the GWQS. Pyrene was not detected in the duplicate sample for MW-14R. Pesticides/PCBs were not detected in any of the wells.

The total metals analyses indicated very few metals exceeded the GWQS with the exception of iron (three wells) ranging from 354 ug/l (MW-10R) to 1,320 ug/l (MW-14R) and aluminum (two wells) at concentrations of 348 ug/l (MW-10R) and 361 ug/l (MW-11R). Chromium and sodium were

detected in sample MW-8R at concentrations of 163 ug/l and 144,000 ug/l, respectively, which exceed the GWQS. Cyanide was not detected in any bedrock well.

## **Operation & Maintenance Monitoring Wells**

The O&M monitoring wells consist of six till wells (MW-2D, MW-5D, MW-7D, MW-8D, MW-11D, MW-12D, and RMW-13D), and one bedrock monitoring well (MW-2R). The analytical data and results of the data review and validation was presented in the Quarterly O&M Report dated December 1996. A summary of the analytical results is presented below and exceedances of the GWQS are shown on Figures 9 and 10.

# Till Monitoring Wells

Total VOCs concentrations ranged from 3 ppb in MW-7D to 63,772 ppb in MW-11D and were generally consistent with previous results. The commonly detected VOCs in the till wells were total 1,2-dichloroethene, 1,1-dichloroethene, 1,1-dichloroethene, trichloroethene, tetrachloroethene, and vinyl chloride.

SVOCs were not detected in MW-2D, MW-5D, MW-7D, MW-8D, MW-12D, and RMW-13D. SVOCs were detected in MW-11D at a total concentration of 91 ppb. In MW-11D, low levels of pesticides were detected and PCBs were detected at a concentration of 14 ppb, but these compounds were not detected in any other wells except MW-7D where there was one low level pesticide detect. Inorganics were detected in unfiltered samples in each of the till monitoring wells and the results are generally consistent, with respect to constituents, to those detected historically at individual sampling points.

# Bedrock Monitoring Wells

The bedrock zone is monitored by MW-2R. The analytical results indicate a total VOC concentration of 767 ppb including similar compounds to those found in the adjacent till well, MW-2D. There were no detections of SVOCs, pesticides nor PCBs. Inorganics were detected in unfiltered samples at low levels consistent with previous monitoring.

#### **Additional Indicator Parameters**

As discussed in a letter to the USEPA dated September 17, 1996, additional indicator parameters were collected from all till and bedrock wells. The analytical results are presented in Appendix J. The purpose for collecting this data was to obtain additional information about the groundwater

geochemistry which may be of value to the assessment of groundwater remedial options, if necessary.

# 4.5 Well Survey Results

Potable water supply to Carlstadt is primarily provided by the United Water New Jersey Company (formerly the Hackensack Water Company) and is obtained from the impounded northern waters of the Hackensack River. There is no known use of groundwater for potable supply purposes within Carlstadt (USEPA & Army Corps of Engineers, 1995).

A search of water withdrawal points (100,000 gpd) located within a 1/2 mile radius of the Site was performed by the Bureau of Water Allocation of the NJDEP at the request of the Group. The results of this survey indicate no wells are located within 1/2 mile of the Site.

An additional search for all wells (excluding monitoring wells) within a 1/2 mile radius of the Site was also performed by the Bureau of Water Allocation. Figure 11 illustrates approximate well locations within a 1/2 mile radius of the Site and summarizes the well records available from the NJDEP. A total of seven wells were identified, each installed in the bedrock aquifer. Five wells are used for industrial and cooling, one well for lawn irrigation and one well for irrigation. The current status of these wells is unknown as all of the wells were installed over 15 years ago.

In addition, during the Investigation, a representative of the NJDEP from the Bureau of Water Allocation visited the Site on August 27, 1996 and stated that the NJDEP has a Well Record for one well on-Site (location unknown) and one well located adjacent to the monitoring well MW-11 cluster. Both of these wells were believed to have been installed around 1969 and to be bedrock wells, although the precise construction details are unknown. The well located by cluster MW-11 was field located and is not operating based on a visual inspection of the well and a conversation with a representative of the property owner. The location of the former well on-Site is unknown and was likely obscured either prior to or during the construction of the Interim Remedial measures.

## 5. CONCLUSIONS AND RECOMMENDATIONS

#### 5.1 Conclusions

The RI data indicated that the on-Site fill materials are impacted by a variety of contaminants including volatile organic compounds (VOCs), polychlorinated biphenyls (PCBs) and metals. VOCs are also present in the shallow groundwater within the fill on-Site, in some cases at concentrations exceeding 10% of solubility for compounds such as tetrachloroethene (PCE) and trichloroethene (TCE). These concentrations are consistent with the presence of free phase product in the fill on the Site as physically observed in the field. Groundwater within the fill is laterally contained by the slurry wall and the aqueous phase is being extracted and treated as part of the Interim Remedy. Based on quarterly water level data, inward gradients within the fill are generally indicated across the slurry wall, except for along Peach Island Creek, where the gradient is towards the Creek.

Previous analytical results have indicated that groundwater in the till and possibly the bedrock is also impacted and is considered to be a potential off-Property pathway for Site related contaminants. VOCs have been historically detected in the deep monitoring wells both on- and off-Property based on the quarterly monitoring results. Semi-volatile organic compounds (SVOCs) have generally not been detected in any of the monitoring wells with the exception of well MW-11D in which relatively low concentrations has been detected. PCBs (Aroclor-1242) have also been consistently detected in well MW-11D. Aroclor 1232 was detected only once in MW-5D in December 1987. Pesticides have not been detected in any of the wells. A wide variety of inorganics have been consistently detected in each well, including naturally occurring compounds.

As discussed in detail in Section 4.4, the groundwater chemistry data for the newly installed off-Property monitoring wells indicates that very few semi-volatile organic and pesticide/PCB compounds are present in either the till and bedrock units with no exceedances of the New Jersey GWQS. Metals were detected consistently in all wells with exceedances of New Jersey GWQS consisting primarily of naturally occurring metals such as aluminum, iron, manganese, and sodium. Therefore, given the results of the off-Property Investigation and historical data, VOCs are the primary focus of this Report.

Significantly lower concentrations of VOCs were detected in the new off-Property monitoring wells as compared to the previously existing monitoring wells. VOCs were detected below the New

Jersey GWQS in four out of the six till wells (MW-10D, MW-15D, MW-17D, and MW-18D) and two of the four bedrock wells (MW-8R and MW-14R). For the remaining till monitoring wells, MW-14D and MW-16D, total VOCs were detected at concentrations of 65 ug/l and 151 ug/l, respectively. Tetrachloroethene, trichloroethene, 1,1-dichloroethene, and 1,2-dichloroethane were the primary contaminants detected in these two wells. For the remaining bedrock wells, MW-10R and MW-11R, total VOCs were detected at concentrations of 8 ug/l and 155 ug/l, respectively. The only constituent detected in well MW-10R at slightly above the New Jersey GWQS was chloroform, although it should be noted that chloroform was also detected in potable water sample PW-01. Tetrachloroethene and trichloroethene were the primary contaminants detected in MW-11R at concentrations of 50 ug/l and 56 ug/l, respectively.

The analytical results from the Investigation indicate that the till unit has not been further impacted to the south, east and west of the Site as indicated by the results of samples MW-18D, MW-10D, and MW-15D, respectively. VOCs, at much lower concentrations, were detected north/northwest (MW-16D) and east/northeast (MW-14D) of the Site. The concentrations detected in these wells were much less (over an order of magnitude) than detected in the RI monitoring wells (e.g. MW-11D, MW-12D, and RMW-13D).

The analytical results for the bedrock unit show very little impact further to the south, north, and east of the Site as indicated by the results of samples MW-8R, MW-10R, and MW-14R. Analytical results for sample MW-11R indicate some impact with total VOCs detected at a concentration of 155 ug/l. However, given the high concentrations of VOCs detected at MW-11D (indicative of the presence of NAPL), adjacent to MW-11R, and the close proximity of a former bedrock water supply well recently identified by a NJDEP Bureau of Water Allocation Representative, the bedrock impact may be the result of local cross contamination.

Continuous water levels collected during the Investigation indicate that downward hydraulic gradients are not prevalent throughout the Site. The vertical hydraulic gradients between the till and bedrock units vary across the investigation area with very slight upward or downward gradients.

The glaciolacustrine varved unit separating the fill from the till and bedrock varies in thickness ranging from 0 to 28 feet. The only area of the Site in which the glaciolacustrine varved confining unit was not intercepted was at slurry wall construction borehole locations B-6 and B-7 (southern

corner of the Site). The glaciolacustrine unit is a predominantly clay soil, and has a hydraulic conductivity on the order of 10<sup>-7</sup> cm/sec based on RI data. Such a unit, where present, would be expected to act as an effective barrier to the migration of contaminants. However, where this unit is absent or thin, a pathway for the downward migration of contaminants to the underlying till and bedrock units could exist. The borehole logs for B-6 and B-7 did not indicate that contamination was encountered in this area of the Site based on visual observations and PID readings. Additionally, given the hydrologic characteristics of the till and bedrock units (e.g. very low average linear groundwater flow velocity for the till and bedrock units, 0.73 ft./year and 5.4 ft./year, and variable groundwater flow direction) the transport time for groundwater to migrate to impacted wells such as MW-11D/R from the area where the glaciolacustrine unit is absent far exceeds the history of Site operations. As such, there are probably other mechanism(s) that play a role in contaminant transport. As discussed in the Work Plan, and to the extent that the contamination in the deeper units originates from the Site, possible additional mechanism(s) that play a role in the transport of contaminants include:

1. Migration through the glaciolacustrine varved unit, in particular via fractures and sand/gravel stringers.

As discussed in Section 4.1 the glaciolacustrine varved unit can be broadly subdivided into two horizons with the upper horizon being sandier and including distinct banding of sand stringers and intercalation of silty sand and silt (bedded varved horizon) while the lower unit is a much softer and highly plastic massive clay and silty clay which would limit any migration. Consistent with this interpretation, significant contamination was noted in the upper bedded unit only. NAPL was observed within the upper unit at locations MW-11R and RMW-13D. Additionally, elevated PID readings were also observed in this unit at location MW-14D/R. PID readings and visual contamination significantly decrease within the lower varved unit indicating that physio-chemical degradation of the clay material/particles of the glaciolacustrine varved unit has probably not occurred.

2. Deterioration of the well seals, particularly in the presence of free-phase product.

Cement bonding (acoustic logging) tests were completed during the Investigation on RI wells MW-2D, MW-2R, MW-5D, MW-7D, and MW-11D and newly installed wells MW-14D and MW-18D. These tests were conducted to assess the integrity of the grout of the monitoring wells. In summary, only 6% of the grout for well MW-2R was classified as having "good" integrity and this interval was near the groundwater surface. 74% of the grout in this well, including the bottom 30 feet was classified as having "poor" integrity. At least 60% of the grout in well MW-2D was also classified as either "fair-poor" or "poor". The grout integrity for the interval from 19 to 21 feet below ground surface at location MW-11D was classified as "poor". This interval, based on data from MW-11R, intersects the bedded varved unit. Furthermore, the downhole video survey indicates that the top of the well screen was at an elevation approximately one foot higher than the well construction diagram indicates. This

information suggests that well seal deterioration may have contributed to contaminant transport.

3. Utility trenches which may have been excavated into the glaciolacustrine varved unit.

A number of utilities exist along Gotham Parkway including communications, water, gas, storm sewer and sanitary sewer (Carlstadt Sewer Authority and Bergen County Utilities Authority (BCUA)). The Carlstadt sewer line is a gravity fed line which slopes away from Paterson Plank Road and travels underneath Peach Island Creek. As-built data obtained from the Borough indicates that the invert elevation of the sewer line in the vicinity of the Site intercepts the upper bedded varved unit but does not intercept the lower varved unit. The BCUA sewer line is a force main line coming from the New Jersey Sports Authority property and runs along the east side of Gotham Parkway. This sewer line is not as deep but may intercept the upper portion of the upper bedded varved unit in the vicinity of the Site.

Because these utilities intercept only the upper horizon of the glaciolacustrine unit, it is unlikely that they serve as a pathway to the till and bedrock.

4. On-site well or other glaciolacustrine varved unit penetration related to past operational practices.

Based on depositional testimony from a former Site worker and records from the NJDEP, a water supply well existed on the Site, although its location has not been established. In addition, the NJDEP records also indicate a well located by well cluster MW-11. The location of this well was verified during the Investigation but it is not currently operating. Both wells were installed around 1969 and are bedrock wells with open boreholes estimated to be greater than 200 feet in length. These wells could have acted as pathways for contamination to the deeper water bearing units.

5. Groundwater extraction from the till and bedrock in the Site vicinity for industrial use.

The well survey completed as part of this Investigation located seven wells within a half-mile of the Site. The long term water level monitoring showed a seven-day fluctuation with water levels slowly declining during the week and recovering during the weekend. This trend suggests that off-Property pumping impacts the direction of groundwater flow. However, the hydraulic gradients are low so that the resulting average linear groundwater velocity in the till and bedrock units is very low and the impact on contaminant transport is probably limited.

The conclusions described above serve as the basis for the following recommendations for a final phase of off-Property work to complete this Investigation.

### 5.2 Recommendations

The following recommendations have been developed to: (1) obtain additional data to complete the off-Property groundwater investigation; (2) prevent further potential cross-contamination of the till

and bedrock units; and, (3) assess off-Property contamination within the upper glaciolacustrine bedded clay unit.

- 1. Installation and sampling of two additional till monitoring wells (MW-19D and MW-20D) north/northwest of Site. Precise locations to be determined following access discussions with appropriate Landowners. Each well will be sampled for TCL VOCs.
- 2. Installation and sampling of one additional till monitoring well (MW-21D) south of the Site (off-Property near boreholes B-6 and B-7) to provide additional geologic control and data on the groundwater quality within the till unit at the location where the glaciolacustrine confining unit is apparently absent. This monitoring well will be sampled once for TCL VOCs.
- 3. Decommissioning of off-Property monitoring well MW-11D to eliminate this potential route of cross contamination.
- 4. Additional long-term water level monitoring incorporating the proposed wells to enhance the understanding of the groundwater flow direction in the till unit.
- 5. Decommissioning on-Site monitoring wells MW-2D and MW-2R to eliminate this potential route of cross contamination.
- 6. Redevelop and assess the construction (e.g. depth of well screen interval) and grout integrity of monitoring well MW-8D. The depth to bottom of the well, as measured during the groundwater sampling, does not coincide with the as-built well construction log (difference of approximately 12 feet). The assessment will include downhole video camera and acoustic logging techniques. Decommission well if necessary based on the results of this assessment.
- 7. Assess monitoring well MW-12D construction (e.g. depth of well screen interval) and grout integrity using downhole video survey and acoustic logging techniques and decommission if necessary.
- 8. Further investigate off-Property pumping including: determining the location of each active well within a one-half mile radius of the Site concentrating to the north/northwest/northeast of the Site; and, obtain as-built construction details of each well located, the pumping rate and schedule, and use of the extracted groundwater.
- 9. Notify utilities and property owners of potential contamination within the upper glaciolacustrine bedded unit off-Site and of the need for appropriate precautions should this unit be disturbed.
- 10. Investigate potential off-Property contamination within the upper glaciolacustrine bedded unit. This investigation will include assessing the lateral extent through field screening techniques (e.g. visual and head space analysis using a PID) and confirmatory laboratory analyses for TCL VOCs, SVOCs, and pesticide/PCBs.
- 11. Decommissioning of the off-Property former production well located adjacent to well cluster MW-11 to eliminate this potential route of cross contamination.

12. Decommissioning of the on-Site former production well to eliminate this potential route of cross contamination, if the well can be located.

The details and schedule for these activities will be contingent upon gaining access approval from affected landowners.

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### ↑ABLE 1 MONITORING WELL CONSTRUCTION DATA 216 PATERSON PLANK ROAD SUPERFUND SITE CARLSTADT, NEW JERSEY

	DATE OF	GROUND	ELEVATION	WELL	WELL	SCREEN	ELEVATION	ELEVATION	TOP OF	TOP OF	TOP OF	TOP OF	TOP OF	TOP OF	SCREENED
WELL	INSTALLATION	SURFACE	TOP OF	DIAMETER &	DEPTH	LENGTH	TOP OF	BOTTOM OF	PEAT	GRAY SILT/	VARVED CLAY	SOFT TILL	LODGEMENT TILL	BEDROCK	INTERVAL
- - ID		<b>ELEVATION</b>	INNER CASING	MATERIAL			SCREENED INTERVAL	SCREENED INTERVAL		BEDDED GLAY (Upper Horizon)	(Lower Horizon)				FORMATION
		(FT-MSL)	(FT-MSL)		(FT BGS)	(FT)	(FT - MSL)	(FT-MSL)	(FT-MSL)	(FT-MSL)	(FT-MSL)	(FT-MSL)	(FT-MSL)	(FT-MSL)	
							REME	DIAL INVESTIGATION MO	NITORING WELL	S					
MW-2D	6/18/87	8.57	12.09	4-INCH SS	61	15	-37.4	-52.4	8.0	-0.8	-5.4	-12.4	-21.4	-51.4	TILL
MW-2R	2/8/89	8.86	11.30	6-INCH OPEN HOLE	88	25	-54.1	-79.1	0.8	-0.8	-5.4	-12.4	-21.4	-51.4	BEDROCK
MW-5D	6/26/87	7.32	10.23	4-INCH SS	62	15	-39.7	-54./	1.4	-1.6	-6.6	-16.9	-27.7	-52.7	TILL
MW-7D	7/6/87	9.09	11.18	4-INCH SS	60	15	-35.9	-50.9	NOT PRESENT	-0.3	-10.9	-28.9	-35.3	-50.0	TILL
MW-8S	1/5/89	5.50	5.08	4-INCH SS	7.5	5	3.0	-2.0	0.5	-2.0	NA <sup>-</sup>	NA	NA	NA	FILL
MW-8D	1/16/89	5.58	5.24	4-INCH SS	54	15	-33.4	-48.4	0.5	-2.0	-9.9	NOT PRESENT	-39.4	-48.2	TILL
MW-9S	1/4/89	5.95	5.55	4-INCH SS	88	5	3.0	-2.1	1.0	-2.8	NA NA	NA	NA	NA	FILL
MW-10S	1/3/89	7.82	7.54	4-INCH SS	9	5	3.8	-1.2	NOT PRESENT	-0.4	NA	NA NA	NA NA	NA	FILL
MW-11S	1/6/89	6.32	6.04	4-INCH SS	7	5	4.3	-0.7	-1.1	-2.1	NA	NA	NA	NA	FILL
MW-11D	1/23/89	5.76	5.51	4-INCH SS	38	15	-17.2	-32.2	1.7	-2.7	-9.9	-18.0	-29.2	-33.0	TILL
MW-12S	1/6/89	6.25	5.63	4-INCH SS	7.5	5	3.8	-1.3	NOT PRESENT	-1.6	NA	NA	NA	NA	FILL
MW-12D	1/18/89	6.37	5.85	4-INCH SS	34	15	-12.6	-27.6	NOT PRESENT	-1.4	-8.6	NOT PRESENT	-21.4	-28.0	TILL
RMW-13D	10/20/95	4.88	4.66	4-INCH SS	43.5	10	-28.6	-38.6	NOT PRESENT	0.9	-9.1	-20.1	-24.1	-38.6	TILL
								PERTY INVESTIGATION							
MW-8R	7/18/96	5.35	5.11	2-INCH SS	93	10	-77.7	-87.7	0.4	-1.5	11.7	-33.4	-39.7	-63.7	BEDROCK
MW-10D	8/21/96	7.49	7.09	4-INCH SS	42	5	-29.5	-34.5	0.7	-2.5	-10.5	-26.5	-34.5	-36.5	TILL
MW-10R	8/26/96	7.48	7.01	2-INCH SS	65.5	10	-48.0	-58.0	0.7	-2.5	-10.5	-26.5	-34.5	-36.5	BEDROCK
MW-11R	8/7/96	6.41	6.19	4-INCH OPEN HOLE	58	10	-41.6	-51.6	-1.6	-3.6	-13.6	-21.3	-25.6	-31.6	BEDROCK
MW-14D	7/26/96	2.45	2.19	4-INCH SS	40	10	-27.6	-37.6	2.6	-6.1	-10.6	-21.9	-30.6	-51.6	TILL
MW-14R	7/23/96	2.37	2.22	4-INCH OPEN HOLE	74	10	-61.6	-71.6	-2.6	-6.1	-10.6	-21.9	-30.6	-51.6	BEDROCK
MW-15D	8/16/96	9.68	9.47	4-INCH SS	52	2	-40.3	-42.3	0.3	-3.3		NOT PRESENT	-37.3	-43.8	TILL
MW-16D	7/29/96	7.25	6.59	4-INCH SS	36	5	-23.8	-28.8	NOT PRESENT	-4.8	-8.8	-16.6	-26.3	-32.8	TILL
MW-17D	7/11/96	5.05	4.75	4-INCH SS	55	10	-40.0	-50.0	0.4	-1.5	-11.7	-33.4	-39.7	-63.7	TILL
MW-18D	7/18/96	5.23	4.51	4-INCH SS	66	5	-55.8	-60.8	0.4	-1.5	-11.7	-33.4	-39.7	-63.7	TILL

### NOTES

- (1) Well depths and screen length for existing monitoring wells estimated from the Dames & Moore monitoring well details provided in the RI Report.
- (2) Elevation data for stratigraphy presented for the existing monitoring wells is estimated based on Golder Associates interpretation of the borehole logs prepared by Dames & Moore and provided in the RI Report.
- (3) Monitoring wells surveyed by GEOD Corporation in October 1996.
- (4) Elevation data for stratigraphy at cluster monitoring well locations (e.g. MW-14D and MW-14R) is based on information from the deeper monitoring well borehole log.

### TABLE 2 SAMPLING AND ANALYSES SUMMARY 216 PATERSON PLANK ROAD SITE CARLSTADT, NEW JERSEY

					WELL DA	ATA INFOR	RMATION
SAMPLE POINT	SAMPLING	ANALYTICAL	QA/QC	(2)	SCREEN	WELL	PUMP
ID	DATE	PARAMETER (1)	FIELD	MS/MSD	LENGTH	DEPTH	DEPTH
			DUPLICATE		(FT)	(FT)	(FT)
Groundwater - Off-Pro	perty Investigat	ion Monitoring Wells	-				
MW-8R	9/19/96	TCL/TAL, CYANIDE & INDICATOR PARAMETERS			10	93	88
MW-10D	9/20/96	TCL/TAL, CYANIDE & INDICATOR PARAMETERS			5	42	40
MW-10R	9/20/96	TCL/TAL, CYANIDE & INDICATOR PARAMETERS			10	65.5	60
MW-11R	9/24/96	TCL/TAL, CYANIDE & INDICATOR PARAMETERS		Х	10 .	57	53
MW-14D	9/23/96	TCL/TAL, CYANIDE & INDICATOR PARAMETERS			10	40	35
MW-14R	9/23/96	TCL/TAL, CYANIDE & INDICATOR PARAMETERS	MW-14RD		10	74	69
MW-15D	9/20/96	TCL/TAL, CYANIDE & INDICATOR PARAMETERS			2	52	51
MW-16D	9/23/96	TCL/TAL, CYANIDE & INDICATOR PARAMETERS			5	36	34
MW-17D	9/19/96	TCL/TAL, CYANIDE & INDICATOR PARAMETERS			10	55	50
MW-18D	9/19/96	TCL/TAL, CYANIDE & INDICATOR PARAMETERS	MW-18DD		5	67	64
Groundwater - Operate MW-2D	9/17/96	TCL/TAL, CYANIDE & INDICATOR PARAMETERS			15	61	54
MW-2R	9/18/96	TCL/TAL, CYANIDE & INDICATOR PARAMETERS		X	25	88	76
MW-5D	9/18/96	TCL/TAL, CYANIDE & INDICATOR PARAMETERS	<del> </del>	<del></del>	15	62	54
MW-7D	9/18/96	TCL/TAL, CYANIDE & INDICATOR PARAMETERS			15	60	53
MW-8D (3)	9/18/96	TCL/TAL, CYANIDE & INDICATOR PARAMETERS		·	2.4	41.4	40.4
MW-11D	9/24/96	TCL/TAL, CYANIDE & INDICATOR PARAMETERS			15	38	30
MW-12D	9/23/96	TCL/TAL, CYANIDE & INDICATOR PARAMETERS			15	34	26
RMW-13D	9/23/96	TCL/TAL, CYANIDE & INDICATOR PARAMETERS			10	43.5	39
Potable Water			1		I		
PW-1	9/23/96	TCL/TAL & CYANIDE		<u> </u>	Γ.	<del></del>	
Notes:							

### Notes

- (1) TCL VOCs, SVOCs, and Pest/PCBs Methodology CLP SOW 0LM03.1, TAL Metals & Cyanide Methodology CLP SOW ILM03.0. Indicator Parameters Methodology: Alkalinity (EPA 310.1), Chloride (EPA 325.3), Ethane, Ethene, Methane, Ethene, Nitrate-Nitrite (EPA 353.2), Total Phosphorus (EPA 365.2), Sulfate (SM18 4500SO4C), Sulfide (EPA 376.1), TKN (EPA 351.2), Total Organic Carbon (EPA 415.1), and Dissolved Iron (CLP SOW ILM03.0).
- (2) Trip Blanks were taken one per day of sampling for VOCs.
- (3) Depth of well was sounded at 41.4 feet below ground surface. As-built well construction log indicates this well should be 54 feet deep with a 15 foot well screen.

### TABLE 3 SUMMARY OF HYDROGEOLOGIC TESTING RESULTS 216 PATERSON PLANK ROAD SITE CARLSTADT, NEW JERSEY

	WELL	T	EST INTERVAL			ONDUCTIVITY IED USING
		TOP	BOTTOM	LENGTH	HVOF	RSLEV
ļ		FT. BGS	FT. BGS	FT.	cm/s	ft/day
	TILL WELLS:					
140	MW-10D	35.5	42.0	6.5	3.19E-06	0.009
")	MW-14D	27.0	41.0	14.0	6.80E-06	0.019
Y4/c	MW-15D	48.5	52.0	3.5	1.53E-04	0.433
1.11 2.11 2.11 2.11	MW-16D	27.0	36.0	9.0	7.09E-04	2.010
,	MW-17D	42.0	55.0	13.0	2.71E-04	0.768
ا يرا	MW-18D	60	66	6.0	1.90E-04	0.537
~ ^ -				C 4*11 11	= 00E 0E	0.400
0		(	Geometric mean	n for till wells: [	7.03E-05	0.199
	BEDROCK WEI	LLS:				
	BEDROCK WEI MW-8R	L <b>LS:</b>	98.8	9.6	3.78E-05	0.107
		L <b>LS:</b> 89.2 89.5	98.8 99.1	9.6 9.6	3.78E-05 5.35E-05	0.107 0.152
		89.2 89.5 99.3	98.8 99.1 109.3	9.6 9.6 10.0	3.78E-05 5.35E-05 4.11E-05	0.107 0.152 0.117
		89.2 89.5 99.3 104.0	98.8 99.1 109.3 113.6	9.6 9.6 10.0 9.6	3.78E-05 5.35E-05 4.11E-05 1.79E-05	0.107 0.152 0.117 0.051
		89.2 89.5 99.3 104.0 109.7	98.8 99.1 109.3 113.6 119.3	9.6 9.6 10.0 9.6 9.6	3.78E-05 5.35E-05 4.11E-05 1.79E-05 1.14E-05	0.107 0.152 0.117 0.051 0.032
		89.2 89.5 99.3 104.0	98.8 99.1 109.3 113.6 119.3 130.0	9.6 9.6 10.0 9.6 9.6 16.0	3.78E-05 5.35E-05 4.11E-05 1.79E-05 1.14E-05 5.03E-05	0.107 0.152 0.117 0.051 0.032 0.143
		89.2 89.5 99.3 104.0 109.7	98.8 99.1 109.3 113.6 119.3	9.6 9.6 10.0 9.6 9.6 16.0	3.78E-05 5.35E-05 4.11E-05 1.79E-05 1.14E-05	0.107 0.152 0.117 0.051 0.032
		89.2 89.5 99.3 104.0 109.7	98.8 99.1 109.3 113.6 119.3 130.0	9.6 9.6 10.0 9.6 9.6 16.0	3.78E-05 5.35E-05 4.11E-05 1.79E-05 1.14E-05 5.03E-05	0.107 0.152 0.117 0.051 0.032 0.143
	MW-8R	89.2 89.5 99.3 104.0 109.7 114.0	98.8 99.1 109.3 113.6 119.3 130.0 Geometric Mea	9.6 9.6 10.0 9.6 9.6 16.0 an for MW-8R:	3.78E-05 5.35E-05 4.11E-05 1.79E-05 1.14E-05 5.03E-05 3.08E-05	0.107 0.152 0.117 0.051 0.032 0.143 0.087
	MW-8R	89.2 89.5 99.3 104.0 109.7 114.0	98.8 99.1 109.3 113.6 119.3 130.0 Geometric Mea	9.6 9.6 10.0 9.6 9.6 16.0 an for MW-8R:	3.78E-05 5.35E-05 4.11E-05 1.79E-05 1.14E-05 5.03E-05 3.08E-05	0.107 0.152 0.117 0.051 0.032 0.143 0.087

### Notes:

<sup>\*</sup> This value is the average of two tests conducted on this well.

		MW-2D	MW-2R	MW-5D	MW-7D	MW-8D	MW-8R
	Į.	Sampled:9/17/96	Sampled:9/18/96	Sampled:9/18/96	Sampled:9/18/96	Sampled:9/18/96	Sampled:9/19/96
STANDARD (1)	PARAMETER	RESULT	RESULT	RESULT	RESULT	RESULT	RESULT
1	Bromodichloromethane	-	-	-	-	-	-
	Carbon Disulfide	-	-	-	-	<u>-</u>	-
4	Chlorobenzene	-	-	19	-	-	-
6	Chloroform	82	98	160	-	-	5
10	Dibromochloromethane	-	-	-	-	-	-
2	1,1-Dichloroethene	6	3	110	-	25	-
70	1,1-Dichloroethane	8	5	33	-	-	-
	Total 1,2-Dichloroethene	11	7	650	-	3100	-
2.	1,2-Dichloroethane	400	370	110	-	-	-
700	Ethylbenzene	-	-	-	-	88	-
2	Methylene Chloride	13	41	22	-	-	-
30	1,1,1-Trichloroethane	-	-	68	-	-	-
1	Tetrachloroethene	-	2	900	-	160	-
1000	Toluene	-	-	-	-	110	3
1	Trichloroethene	230	200	2500	3	1100	
5	Vinyl chloride	36	41	32	-	-	-
40	Total Xylenes	-	-	-	-	320	-

Notes:

Units are in ug/l.

<sup>(1) -</sup> The standard column is derived from the "New Jersey Register" N.J.A.C. 7:9-6 "Groundwater Quality Standards" (GWQS), April 5th, 1994 edition.

<sup>&</sup>quot;---" indicates that no standard is available.

<sup>&</sup>quot;-" indicates that the constituent was not detected as qualified with a "U" or "UJ".

		MW-10D	MW-10R	MW-11D	MW-11R	MW-12D	RMW-13D
	ļ	Sampled:9/20/96	Sampled:9/20/96	Sampled:9/24/96	Sampled:9/24/96	Sampled:9/23/96	Sampled:9/23/96
STANDARD (1)	PARAMETER	RESULT	RESULT	RESULT	RESULT	RESULT	RESULT
1	Bromodichloromethane	-	-	-	-	-	-
	Carbon Disulfide	-	-	-	-	-	-
4	Chlorobenzene	-	-	-	-	39	-
6	Chloroform	3	7	-	10	-	240
10	Dibromochloromethane	-	-	-	•	-	-
2	1,1-Dichloroethene	-	-	-	3	370	210
70	1,1-Dichloroethane	-	-	-	2	99	94
	Total 1,2-Dichloroethene	-	-	42	24	4500	2200
2	1,2-Dichloroethane	-	-	-	9	-	210
700	Ethylbenzene	-	-	730	-	84	_
2	Methylene Chloride	-	1	-	-	-	-
30	1,1,1-Trichloroethane	-	-	-	1	110	82
1	Tetrachloroethene	-	-	53000	50	470	410
1000	Toluene	-	-	2200	-	-	_
1	Trichloroethene	-	-	4500	56	2100	1500
5	Vinyl chloride	-	-	-	-	380	92
40	Total Xylenes	-	-	3300	_	48	-

### Notes:

. Units are in ug/l.

<sup>(1) -</sup> The standard column is derived from the "New Jersey Register" N.J.A.C. 7:9-6 "Groundwater Quality Standards" (GWQS), April 5th, 1994 edition.

<sup>&</sup>quot;---" indicates that no standard is available.

<sup>&</sup>quot;-" indicates that the constituent was not detected as qualified with a "U" or "UJ".

		MW-14D	MW-14R	MW-14R (Dup.) Sampled:9/23/96	MW-15D	MW-16D Sampled:9/23/96	MW-17D Sampled:9/19/96
OTANDADD (4)	DADAMETER	Sampled:9/23/96	Sampled:9/23/96		Sampled:9/24/96	RESULT	RESULT
STANDARD (1)	<del>'</del>	RESULT	RESULT	RESULT	RESULT	RESULI	KESULI
1	Bromodichloromethane	_	-	-		-	-
	Carbon Disulfide	-	-	-		-	-
4	Chlorobenzene			-	-	-	-
6	Chloroform	5	-	-		1	-
10	Dibromochloromethane	-	-	-	-	-	<u> </u>
2	1,1-Dichloroethene	-	-	-	-	6	-
70	1,1-Dichloroethane	-	•			3	-
	Total 1,2-Dichloroethene	-	-	-	-	30	
2	1,2-Dichloroethane	- "	_	-	-	11	-
700	Ethylbenzene	2	-	-	-	-	-
2	Methylene Chloride	-	-	-	-		-
30	1,1,1-Trichloroethane	1	-	-	-	3	
1	Tetrachioroethene	2	•	-	-	21	-
1000	Toluene	2	-	-	-	-	-
1	Trichloroethene	45	1	1	-	76	-
5	Vinyl chloride	-	-	-	-	-	-
40	Total Xylenes	8	-	-	-	-	-

### Notes:

Units are in ug/l.

<sup>(1) -</sup> The standard column is derived from the "New Jersey Register" N.J.A.C. 7:9-6 "Groundwater Quality Standards" (GWQS), April 5th, 1994 edition.

<sup>&</sup>quot;---" indicates that no standard is available.

<sup>&</sup>quot;-" indicates that the constituent was not detected as qualified with a "U" or "UJ".

STANDARD (1)	PARAMETER	MW-18D Sampled:9/19/96 RESULT	MW-18D (Dup.) Sampled:9/19/96 RESULT	PW-01 Sampled:9/19/96 RESULT	RESULT	RESULT	RESULT
1	Bromodichloromethane	•	-	11			
	Carbon Disulfide	-	-	-			
4	Chlorobenzene	-	-	-			
6	Chloroform	-	-	23			
10	Dibromochloromethane		-	4			
2	1,1-Dichloroethene	-	-	-			
70	1,1-Dichloroethane	-	-	-			
	Total 1,2-Dichloroethene		-	-			
2	1,2-Dichloroethane	-	-	-			
700	Ethylbenzene	-	-	- 1			
2	Methylene Chloride	1	-	-			
30	1,1,1-Trichloroethane		-	-			
1	Tetrachloroethene	-	-	-			
1000	Toluene	-	-	-			
1	Trichloroethene	-	-	-			
5	Vinyl chloride	-	-	-			
40	Total Xylenes	-	•	-			

### Notes:

Units are in ug/l.

<sup>(1) -</sup> The standard column is derived from the "New Jersey Register" N.J.A.C. 7:9-6 "Groundwater Quality Standards" (GWQS), April 5th, 1994 edition.

<sup>&</sup>quot;---" indicates that no standard is available.

<sup>&</sup>quot;-" indicates that the constituent was not detected as qualified with a "U" or "UJ".

CTANDADD (4)	DADAMETER	MW-2D Sampled:9/17/96	MW-2R Sampled:9/18/96	MW-5D Sampled:9/18/96	MW-7D Sampled:9/18/96	MW-8D Sampled:9/18/96	MW-8R Sampled:9/19/96
STANDARD (1)		RESULT	RESULT	RESULT	RESULT	RESULT	RESULT
400	Acenaphthene				<b>-</b>		
2000	Anthracene	-	-	-	-	-	-
30	Bis(2-ethylhexyl)phthalate	-	-		-	-	
	Dibenzofuran	-	-	-	-	-	-
900	Di-n-butylphthalate	-	-	-	-	-	-
600	1,2-Dichlorobenzene	-	-	-	-	-	-
100	2,4-Dimethylphenol	-	-	-	-	-	-
300	Fluoranthene	-	-	-	-	-	-
300	Fluorene	-	-	-	-	-	-
	2-Methylphenol	-	•	-	-	-	-
	4-Methylphenol	-	-	-	-	<u>-</u> '	-
	2-Methylnapthalene	-	-	-	-	-	-
	Napthalene	-	-	-	-	-	_
	Phenanthrene	-	-	-	-	-	-
4000	Phenol	-	-	-	-	-	-
200	Pyrene	-	_		_	_	_

Notes:

Units are in ug/l.

<sup>(1) -</sup> The standard column is derived from the "New Jersey Register" N.J.A.C. 7:9-6 "Groundwater Quality Standards" (GWQS), April 5th, 1994 edition.

<sup>&</sup>quot;---" indicates that no standard is available.

<sup>&</sup>quot;-" indicates that the constituent was not detected as qualified by a "U" or "UJ".

STANDARD (1)	PARAMETER	MW-10D Sampled:9/20/96 RESULT	MW-10R Sampled:9/20/96 RESULT	MW-11D Sampled:9/24/96 RESULT	MW-11R Sampled:9/24/96 RESULT	MW-12D Sampled:9/23/96 RESULT	RMW-13D Sampled:9/23/96 RESULT
	<del></del>	NESOE1	KLOOLI	- KLSOLI	KESULI	RESOLI	RESOLI
400	Acenaphthene			-		<u> </u>	
2000	Anthracene	-			-	-	
30	Bis(2-ethylhexyl)phthalate	-	-	16			
	Dibenzofuran	-	-	-	-	-	-
900	Di-n-butylphthalate	-	-	1	-	-	
600	1,2-Dichlorobenzene	-		7	-	-	-
100	2,4-Dimethylphenol	-	-	4	-	-	-
300	Fluoranthene	-	-	-	-	-	-
300	Fluorene	-	-	-	_	-	-
	2-Methylphenol	-	-	17	_	-	-
	4-Methylphenol	-	-	18	-	_	-
	2-Methylnapthalene	-	-	5	-	-	-
	Napthalene	-	-	8	-	-	-
	Phenanthrene	-	-	1	-	-	-
4000	Phenol	-	-	-	19	-	-
200	Pyrene						-

### Notes:

Units are in ug/l.

<sup>(1) -</sup> The standard column is derived from the "New Jersey Register" N.J.A.C. 7:9-6 "Groundwater Quality Standards" (GWQS), April 5th, 1994 edition.

<sup>&</sup>quot;---" indicates that no standard is available.

<sup>&</sup>quot;-" indicates that the constituent was not detected as qualified by a "U" or "UJ".

January 1997

# TABLE 4 SUMMARY OF CHEMICAL ANALYSIS DETECTIONS GROUNDWATER SAMPLES 216 PATERSON PLANK ROAD SITE ORGANIC DETECTIONS - SEMIVOLATILES

		MW-14D	MW-14R	MW-14R (Dup.)	MW-15D	MW-16D	MW-17D
	1	Sampled:9/23/96	Sampled:9/23/96	Sampled:9/23/96	Sampled:9/24/96	Sampled:9/23/96	Sampled:9/19/96
STANDARD (1)	PARAMETER	RESULT	RESULT	RESULT	RESULT	RESULT	RESULT
400	Acenaphthene	-	-	-	-		-
2000	Anthracene	-	-	-	-	-	-
30	Bis(2-ethylhexyl)phthalate	-	-	-	-	1	-
	Dibenzofuran	-		-	-	-	
900	Di-n-butylphthalate	-	-	-	-	-	-
600	1,2-Dichlorobenzene	-	-	-	-	-	-
100	2,4-Dimethylphenol	-	-	-	-	-	
300	Fluoranthene	-	-	-	-	-	-
300	Fluorene	-	-	-	-	-	
	2-Methylphenol	-	-	-	-	-	-
	4-Methylphenol	-	-	-	-	-	-
	2-Methylnapthalene	_	-	-	-	-	-
	Napthalene	-	-	-	-	-	-
	Phenanthrene	-	-	-	-	-	-
4000	Phenol	-	-	-	-	-	-
200	Pyrene	-	1	-	-	-	-

### Notes:

Units are in ug/l.

<sup>(1) -</sup> The standard column is derived from the "New Jersey Register" N.J.A.C. 7:9-6 "Groundwater Quality Standards" (GWQS), April 5th, 1994 edition.

<sup>&</sup>quot;---" indicates that no standard is available.

<sup>&</sup>quot;-" indicates that the constituent was not detected as qualified by a "U" or "UJ".

		MW-18D	MW-18D (Dup.)	PW-01			
	İ	Sampled:9/19/96	Sampled:9/19/96	Sampled:9/23/96			
STANDARD (1)	PARAMETER	RESULT	RESULT	RESULT	RESULT	RESULT	RESULT
400	Acenaphthene	-	-	-			
2000	Anthracene	-	-	-			
30	Bis(2-ethylhexyl)phthalate	-	-	-			
	Dibenzofuran	-	-	-			
900	Di-n-butylphthalate	-	-	-			
600	1,2-Dichlorobenzene	-	-	-			
100	2,4-Dimethylphenol	-	-	-			
300	Fluoranthene	-	-	-			
300	Fluorene	-	-	-			
	2-Methylphenol	-	-	-			
	4-Methylphenol	-	-	-			
	2-Methylnapthalene	-	-	-			
	Napthalene	-	-	-			
	Phenanthrene	-	-	-			
4000	Phenol	-	-	-			
200	Pyrene	-		-			

Notes:

Units are in ug/l.

<sup>(1) -</sup> The standard column is derived from the "New Jersey Register" N.J.A.C. 7:9-6 "Groundwater Quality Standards" (GWQS), April 5th, 1994 edition.

<sup>&</sup>quot;--" indicates that no standard is available.

Indicates exceedance of the New Jersey Groundwater Quality Standard for a Class IIa aquifer.

<sup>&</sup>quot;-" indicates that the constituent was not detected as qualified by a "U" or "UJ".

-							
		MW-2D	MW-2R	MW-5D	MW-7D	MW-8D	MW-8R
		Sampled:9/17/96	Sampled:9/18/96	Sampled:9/18/96	Sampled:9/18/96	Sampled:9/18/96	Sampled:9/19/96
STANDARD (1)	PARAMETER	RESULT	RESULT	RESULT	RESULT	RESULT	RESULT
0.04	Aldrin	-	-	-	-	-	-
0.2	beta-BHC	-	-	-	-	-	-
0.5	alpha-Chlordane	-	-	-	-	-	-
0.5	gamma-Chlordane	-	-	-	-	-	-
0.1	4,4-DDE	-	-	-	-	-	-
0.1	4,4-DDT	-	-	-	0.0064	-	-
0.03	Dieldrin	-	-	-	-	-	-
0.4	Endosulfan II	-	-	-	-	_	-
	Endrin Aldehyde	-	-	-	-	-	-
0.4	Heptachlor	-	-	_	-	-	_
0.5	Aroclor-1242	-	-	-	-	-	-

### Notes:

Units are in ug/l.

<sup>(1) -</sup> The standard column is derived from the "New Jersey Register" N.J.A.C. 7:9-6 "Groundwater Quality Standards" (GWQS), April 5th, 1994 edition.

<sup>&</sup>quot;---" indicates that no standard is available.

<sup>&</sup>quot;-" indicates that the constituent was not detected as qualified by a "U", "UJ", or "R".

		MW-10D	MW-10R	MW-11D	MW-11R	MW-12D	RMW-13D
		Sampled:9/20/96	. Sampled:9/20/96	Sampled:9/24/96	Sampled:9/24/96	Sampled:9/23/96	Sampled:9/23/96
STANDARD (1)	PARAMETER	RESULT	RESULT	RESULT	RESULT	RESULT	RESULT
0.04	Aldrin	-	-	-	-	-	-
0.2	beta-BHC	-	-			-	-
0.5	alpha-Chlordane	-	-	0.017	-	-	-
0.5	gamma-Chlordane	-	-	-		-	-
0.1	4,4-DDE	-	-	-	•	-	•
0.1	4,4-DDT	-	-	-	-	-	-
0.03	Dieldrin	-	-	0.021	-	-	-
0.4	Endosulfan II	-	-	-	-	-	-
	Endrin Aldehyde	-	-	-	-	-	
0.4	Heptachlor	-	-	-	-	-	-
0.5	Aroclor-1242	•	-	14	-	-	-

### Notes:

Units are in ug/l.

<sup>(1) -</sup> The standard column is derived from the "New Jersey Register" N.J.A.C. 7:9-6 "Groundwater Quality Standards" (GWQS), April 5th, 1994 edition.

<sup>&</sup>quot;---" indicates that no standard is available.

<sup>&</sup>quot;-" indicates that the constituent was not detected as qualified by a "U", "UJ", or "R".

		MW-14D	MW-14R	MW-14R (Dup.)	MW-15D	MW-16D	MW-17D
		Sampled:9/23/96	Sampled:9/23/96	Sampled:9/23/96	Sampled:9/24/96	Sampled:9/23/96	Sampled:9/19/96
STANDARD (1)	PARAMETER	RESULT	RESULT	RESULT	RESULT	RESULT	RESULT
0.04	Aldrin	-	-	-	-	-	-
0.2	beta-BHC	-	-	-	-	-	-
0.5	alpha-Chlordane	-	-	-	-	-	-
0.5	gamma-Chlordane	-	-	-	-	-	-
0.1	4,4-DDE	-	-	-	0.1	-	-
0.1	4,4-DDT	-	-	-	-	-	-
0.03	Dieldrin	-	-	-	-	-	-
0.4	Endosulfan II	-	-	-	0.1	-	-
	Endrin Aldehyde	-	-	_	0.013	- 1	-
0.4	Heptachior	-	-	-	•	-	-
0.5	Aroclor-1242	-	-	-	-	-	-

Notes:

Units are in ug/l.

<sup>(1) -</sup> The standard column is derived from the "New Jersey Register" N.J.A.C. 7:9-6 "Groundwater Quality Standards" (GWQS), April 5th, 1994 edition.

<sup>&</sup>quot;---" indicates that no standard is available.

<sup>&</sup>quot;-" indicates that the constituent was not detected as qualified by a "U", "UJ", or "R".

		MW-18D Sampled:9/19/96	MW-18D (Dup.) Sampled:9/19/96	<b>PW-01</b> Sampled:9/23/96			
STANDARD (1)	PARAMETER	RESULT	RESULT	RESULT	RESULT	RESULT	RESULT
0.04	Aldrin	-	-	-			
0.2	beta-BHC	-	-	-			
0.5	alpha-Chlordane	-	-	-			
0.5	gamma-Chlordane	-	-	-			
0.1	4,4-DDE	•	-	-			
0.1	4,4-DDT	-	-	-			
0.03	Dieldrin	-	-	-			
0.4	Endosulfan II	-	-	-			
	Endrin Aldehyde	-	-	-			
0.4	Heptachlor	-	-	-			
0.5	Aroclor-1242	-	-	-			

### Notes:

Units are in ug/l.

<sup>(1) -</sup> The standard column is derived from the "New Jersey Register" N.J.A.C. 7:9-6 "Groundwater Quality Standards" (GWQS), April 5th, 1994 edition.

<sup>&</sup>quot;---" indicates that no standard is available.

<sup>&</sup>quot;-" indicates that the constituent was not detected as qualified by a "U", "UJ", or "R".

							=
		MW-2D Sampled:9/17/96	MW-2R Sampled:9/18/96	MW-5D Sampled:9/18/96	MW-7D Sampled:9/18/96	MW-8D Sampled:9/18/96	MW-8R Sampled:9/19/96
STANDARD (1)	PARAMETER	RESULT	RESULT	RESULT	RESULT	RESULT	RESULT
200	Aluminum, Total	159	91.9	77	112	3540	174
20	Antimony, Total	-	2.3	-	-	-	-
8	Arsenic, Total	2.4	-	2.6	-	5	-
2000	Barium, Total	54.2	84.5	25.4	16.2	55.5	73.4
20	Beryllium, Total	-	-	-	-	0.17	-
4	Cadmium, Total		-	_	-	0.16	-
	Calcium, Total	383000	355000	262000	104000	218000	308000
100	Chromium, Total	-	-	33.2	7.9	14.6	163
	Cobalt, Total	-	0.79	-	1	2.1	0.57
1000	Copper, Total	3.5	3.7	3.9	3.9	8.9	10.7
300	Iron, Total	150	-	180	96.9	4280	114
10	Lead, Total	-	-	-	1.6	3.7	-
	Magnesium, Total	23400	4310	16800	12100	30600	14700
50	Manganese, Total	109	3	104	74.5	278	6.6
2	Mercury, Total	-	-	-	-	-	-
100	Nickel, Total	4	4.9	15.5	20.2	16.8	15.7
	Potassium, Total	14500	6650	1940	2290	5920	38800
50	Selenium, Total	-	-	-	-	-	-
	Silver, Total	-	-	-	-	-	-
50000	Sodium, Total	120000	80400	61700	52700	186000	144000
10	Thallium	_	-	-	-	-	-
	Vanadium, Total	4.5	4.7	3.6	8	6.5	4.2
5000	Zinc, Total	24	17.4	31.6	30.1	27.9	21.8
200	Cyanide	-		-	-	-	-

Notes:

Units are in ug/l.

<sup>(1) -</sup> The standard column is derived from the "New Jersey Register" N.J.A.C. 7:9-6 "Groundwater Quality Standards" (GWQS), April 5th, 1994 edition.

<sup>&</sup>quot;-" indicates that no standard is available.

<sup>&</sup>quot;-" indicates that the constituent was not detected qualified by a "U", "UJ", or "R".

		MW-10D Sampled:9/20/96	MW-10R Sampled:9/20/96	MW-11D Sampled:9/24/96	MW-11R Sampled:9/24/96	MW-12D Sampled:9/23/96	RMW-13D Sampled:9/23/96
STANDARD (1)	PARAMETER	RESULT	RESULT	RESULT	RESULT	RESULT	RESULT
200	Aluminum, Total	193	348	632	361	395	128
20	Antimony, Total	3.5	-	-	-	-	-
8	Arsenic, Total	2.6	-	-	_	-	3.2
2000	Barium, Total	40.9	25.7	31.4	34.3	78.2	45.4
20	Beryllium, Total	-	-	-	-	-	
4	Cadmium, Total	0.31	0.3	-	-	0.3	
	Calcium, Total	88300	91900	148000	120000	176000	179000
100	Chromium, Total	373	5.3	4.1	14	3.4	1.7
	Cobalt, Total	0.54	•	0.61	•	-	-
1000	Copper, Total	8.6	4.5	5.4	10.4	15.5	3.6
300	Iron, Total	162	354	650	362	609	53.5
10	Lead, Total	1.7	-	2.8	2.5	1.7	-
	Magnesium, Total	527	4170	5620	119	36900	12900
50	Manganese, Total	4.3	14.9	41.8	3.7	817	24.5
2	Mercury, Total	-	-	-	-	-	-
100	Nickel, Total	13	6	6	4.3	4.9	3.5
	Potassium, Total	41100	3840	2510	10100	2410	5130
50	Selenium, Total	-	-	-	-	-	-
	Silver, Total	-	-	-	_	-	-
50000	Sodium, Total	82100	36700	63600	46300	179000	86900
10	Thallium	-	-	-	-	-	-
	Vanadium, Total	48.1	28.3	6.4	62.8	0.9	1.6
5000	Zinc, Total	16.7	24.1	-	-	33.4	-
200	Cyanide	-	-	-	-	-	•

Notes:

Units are in ug/l.

<sup>(1) -</sup> The standard column is derived from the "New Jersey Register" N.J.A.C. 7:9-6 "Groundwater Quality Standards" (GWQS), April 5th, 1994 edition.

<sup>&</sup>quot;---" indicates that no standard is available.

<sup>&</sup>quot;-" indicates that the constituent was not detected qualified by a "U", "UJ", or "R".

			<del></del>		<del></del>		<del></del>
		MW-14D Sampled:9/23/96	MW-14R Sampled:9/23/96	MW-14R (Dup.) Sampled:9/23/96	MW-15D Sampled:9/24/96	MW-16D Sampled:9/23/96	MW-17D Sampled:9/19/96
STANDARD (1)	PARAMETER	RESULT	RESULT	RESULT	RESULT	RESULT	RESULT
200	Aluminum, Total	544	167	173	389	246	531
20	Antimony, Total	-	-	-	-		-
8	Arsenic, Total	8	3	2.6	-	-	
2000	Barium, Total	61.4	16	16.7	108	184	64.6
20	Beryllium, Total	-	-	-	-	-	-
4	Cadmium, Total	0.48	-	0.34	-	-	0.34
	Calcium, Total	103000	170000	168000	123000	224000	254000
100	Chromium, Total	434	4	3.9	42	2.1	6.1
	Cobalt, Total	0.58	-	-	-	-	1.7
1000	Copper, Total	22.1	3.3	4.3	8.9	5.8	4.7
300	Iron, Total	135	1320	1310	290	41.9	945
10	Lead, Total	-	+	1.9	3.2	1.9	-
	Magnesium, Total	150	9760	9300	1270	4570	57300
50	Manganese, Total	2.9	36.8	35.3	6.5	3.1	1360
2	Mercury, Total	-	-	-	-	-	-
100	Nickel, Total	9	3.6	5.9	18.9	4.4	41.5
	Potassium, Total	101000	2520	2500	14800	12100	7640
50	Selenium, Total	4.1	-	-	-	-	-
	Silver, Total	-	-	-	•	-	-
50000	Sodium, Total	120000	36000	35400	55900	93100	244000
10	Thallium	-	-	-	-	-	-
	Vanadium, Total	87.3	9.8	9.6	21.7	10	1.9
5000	Zinc, Total	-	-	73.9	-	-	13.7
200	Cyanide	10.9	-	-	-	-	-

Notes:

Units are in ug/l.

<sup>(1) -</sup> The standard column is derived from the "New Jersey Register" N.J.A.C. 7:9-6 "Groundwater Quality Standards" (GWQS), April 5th, 1994 edition.

<sup>&</sup>quot;---" indicates that no standard is available.

<sup>&</sup>quot;-" indicates that the constituent was not detected qualified by a "U", "UJ", or "R".

January 1997

### TABLE 4 SUMMARY OF CHEMISTRY ANALYSIS DETECTIONS GROUNDWATER SAMPLES 216 PATERSON PLANK ROAD SITE INORGANIC DETECTIONS - TOTAL METALS/CYANIDE

		r	<del></del>				
		MW-18D Sampled:9/19/96	MW-18D (Dup.) Sampled:9/19/96	PW-01 Sampled:9/23/96			
STANDARD (1)	PARAMETER	RESULT	RESULT	RESULT	RESULT	RESULT	RESULT
200	Aluminum, Total	203	219	238			
20	Antimony, Total	-	-	_			
8	Arsenic, Total	-	-				
2000	Barium, Total	35.4	35.1	68.2			
20	Beryllium, Total	-	-	-			
4	Cadmium, Total	-	-				
	Calcium, Total	297000	296000	35100			
100	Chromium, Total	3.2	2.5				
	Cobalt, Total	0.9	1.0				
1000	Copper, Total	6.3	6.1	21.6			
300	Iron, Total	138	128	27			
10	Lead, Total	-	1.9	1.9			
	Magnesium, Total	48500	48500	6770			
50	Manganese, Total	318	319	7.7			
2	Mercury, Total	-	-	-			
100	Nickel, Total	29.4	30.6	3			
	Potassium, Total	5690	5690	1970			
50	Selenium, Total	-	-	-			
<del></del>	Silver, Total	-	-	-			
50000	Sodium, Total	199000	199000	37000			
10	Thallium	-	-	- 1			
	Vanadium, Total	4.8	4.7	0.93			
5000	Zinc, Total	18.4	31.8	-			
200	Cyanide		-	-			

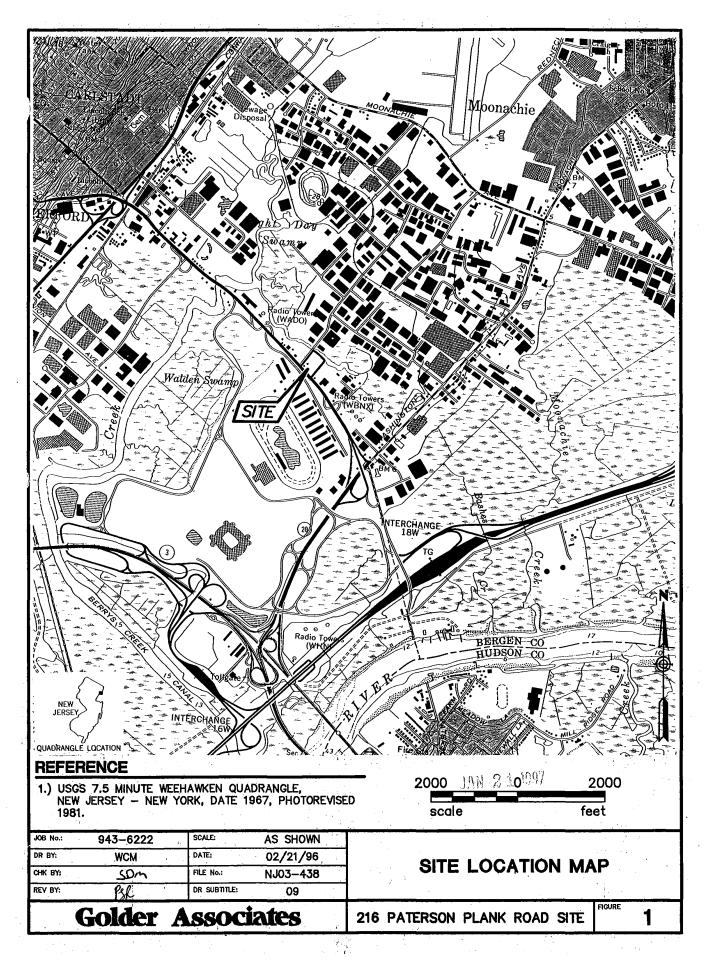
Notes:

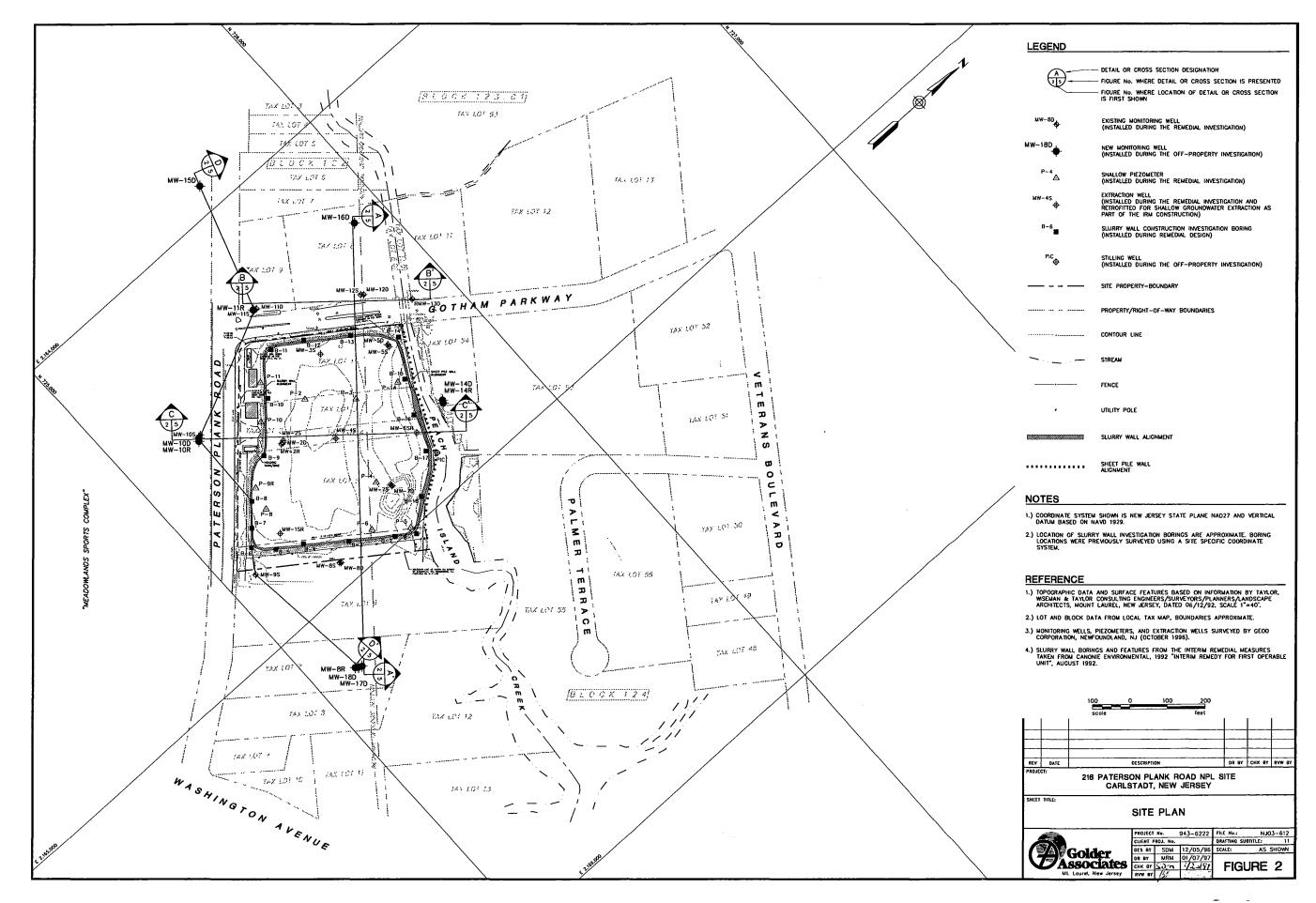
Units are in ug/l.

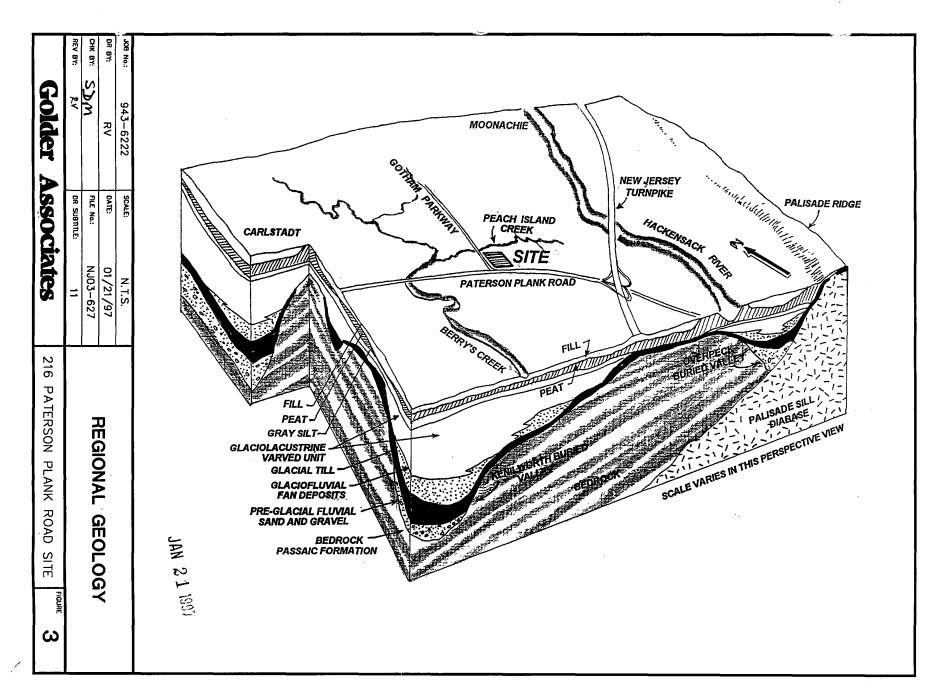
<sup>(1) -</sup> The standard column is derived from the "New Jersey Register" N.J.A.C. 7:9-6 "Groundwater Quality Standards" (GWQS), April 5th, 1994 edition.

<sup>&</sup>quot;---" indicates that no standard is available.

<sup>&</sup>quot;-" indicates that the constituent was not detected qualified by a "U", "UJ", or "R".







### STRATIGRAPHIC UNITS

FILL: variable thickness; including asphalt, silt, sand, gravel, \_ concrete, brick, timber etc.; highly variable SPT blow counts

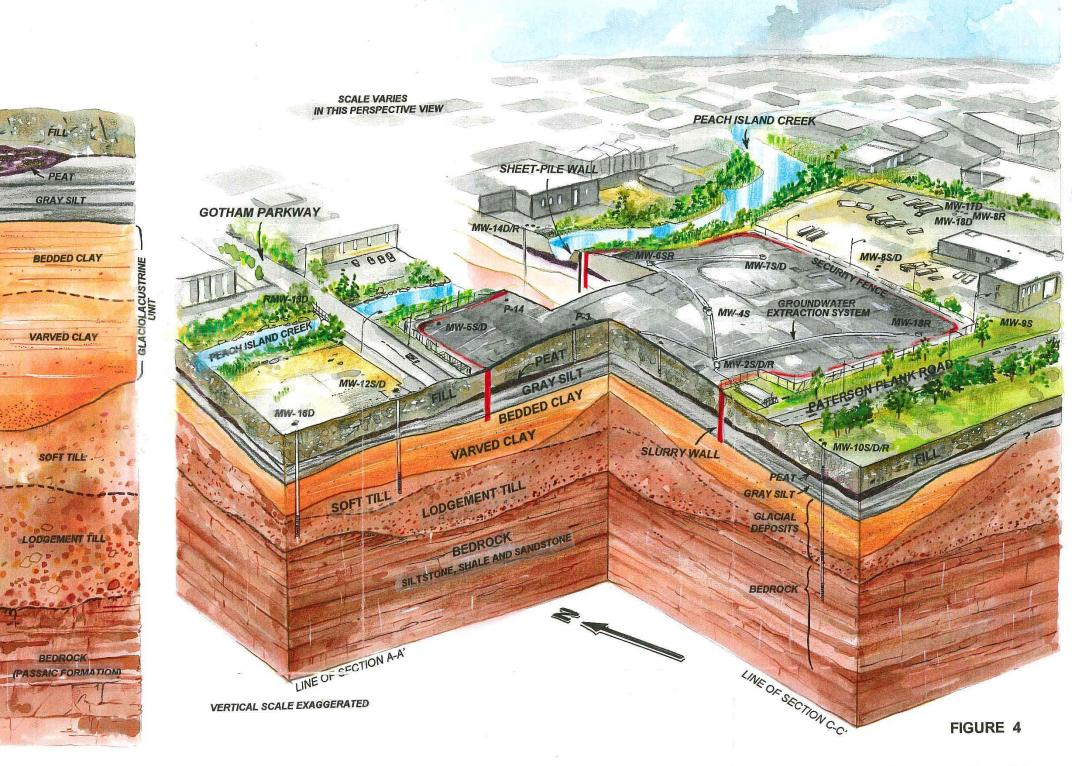
PEAT: laterally persistant and correlatable meadow mat unit, locally removed during site activities, variable thickness, dark brown to gray color, organic silt, clay and sand, fibres common, low SPT blow counts, grades down into Gray Silt.

GRAY SILT: uniform thickess, intertidal unit, mottled dark gray to brownish gray color, with silt and fine sand seams, bedded to laminated; upper contact grades into peat, lower contact grades into the uppermost glacial sediments; SPT blow counts variable but generally N=5 or higher.

GLACIOLACUSTRINE VARVED UNIT: stratified glacial deposits; upper horizon sandier and varved with local zones of fine silt and sand, set in a stiff to very stiff matrix of silty clay and clay, variagated color ranging from brownish gray, dark gray, to brownish red. Lower horizon consists of deep red, reddish brown and locally brick red, high plasticity, massive clay; varved structure apparent when dry but clastic content much lower than upper horizon. SPT blow counts in upper horizon generally higher than N=5; lower horizon is commonly N=0 or weight of hammer; local sandier zones present near lower geologic contact with underlying unit. Both horizons tentatively correlated with the Glacial Lake Hackensack and Glacial Lake Bayonne sediments, upper horizon possibly desiccated.

GLACIAL TILL: two unstratified basal horizons recognized, characteristically red to reddish brown, brick red and locally dark brown in color; *upper horizon* is softer somewhat weathered less dense, glacial till, SPT blow counts generally less than N=25, soft sandy to silty glacial till with matrix supported clasts which include metamorphic rock fragments; *lower horizon*, a lodgement till, consists of very hard, SPT blow counts ranging from N=50 to N=200, dominated by in-situ rock fragments including siltstone and shale, and sandstone of local bedrock; the upper geologic contact with varved unit is sharp, and marked by distinct change in geotechnical character; lower geologic contact grades imperceptably into bedrock; This unit correlatable with the Rahway Till.

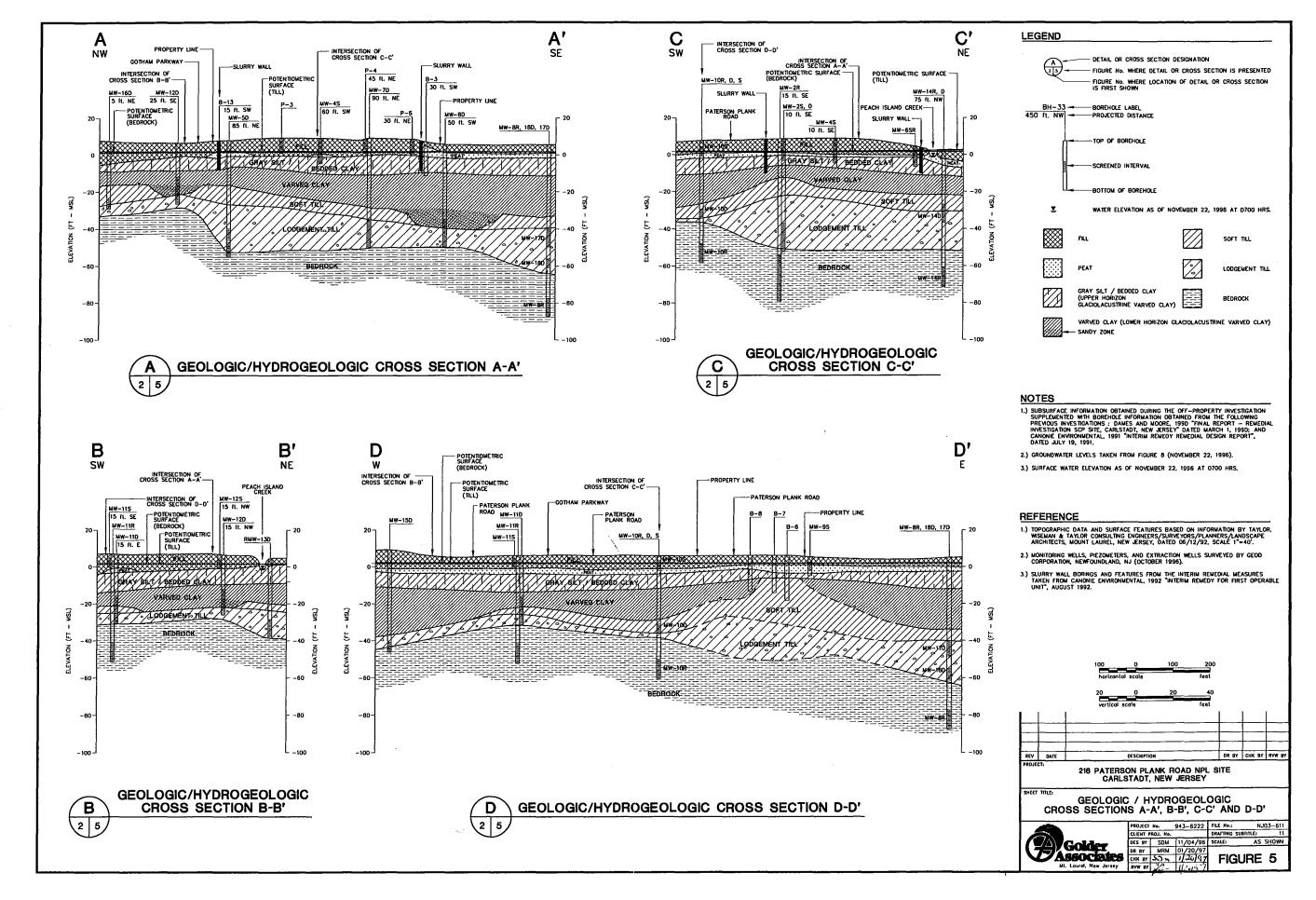
BEDROCK: bedrock consists of brick red and brown, and red, speckled and mottled by green reduction haloes and spots, horizontally bedded, laminated and fissile shale, siltstone and fine sandstone of the Passaic Formation. The basal lodgement till of overlying unconsolidated deposits grades into the bedrock. Bedrock includes several carbonate-bearing horizons; carbonate occurs as vugs, nodules; fracture and bedding-planes sometimes infilled and coated with calcite and/or dolomite.

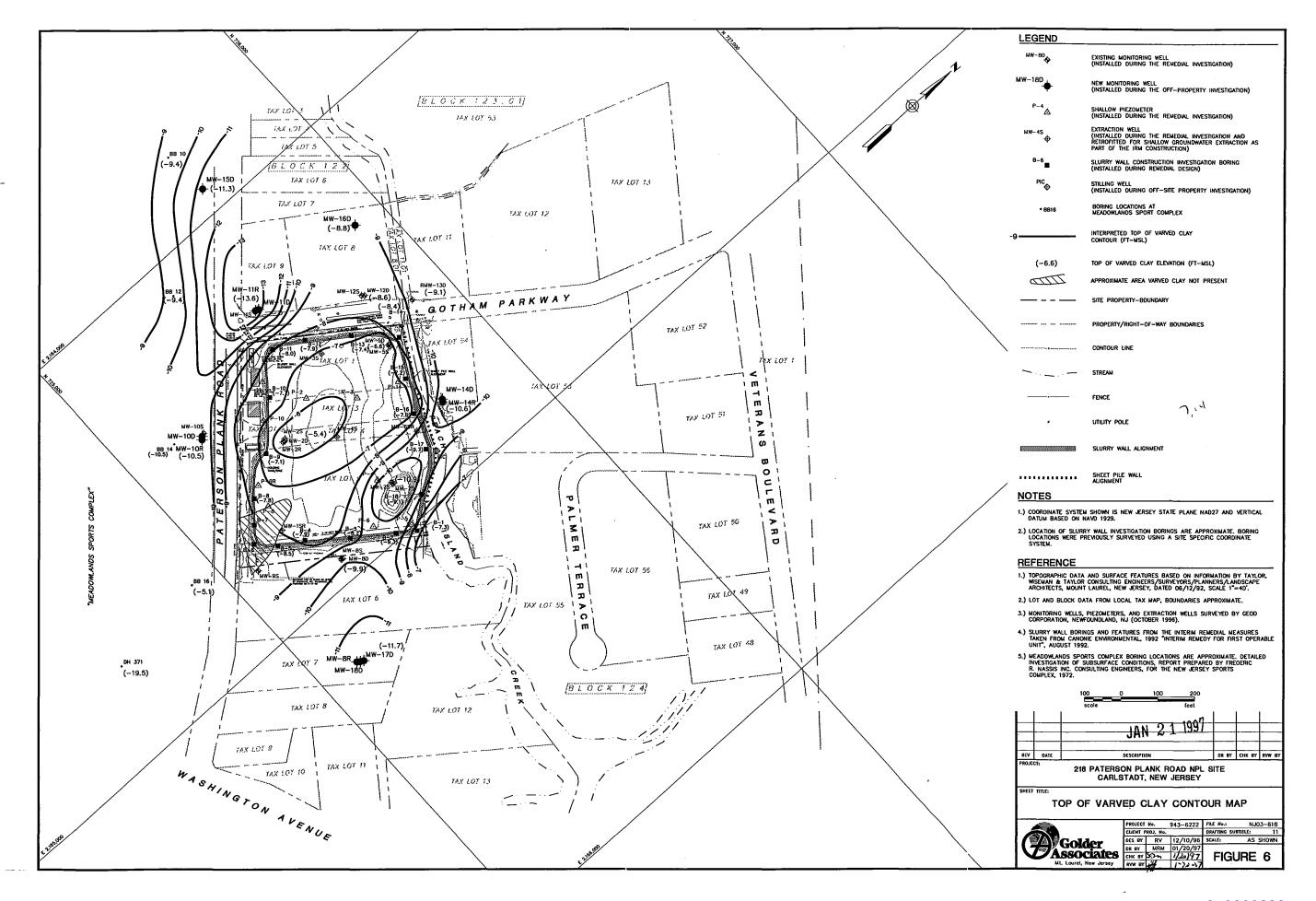


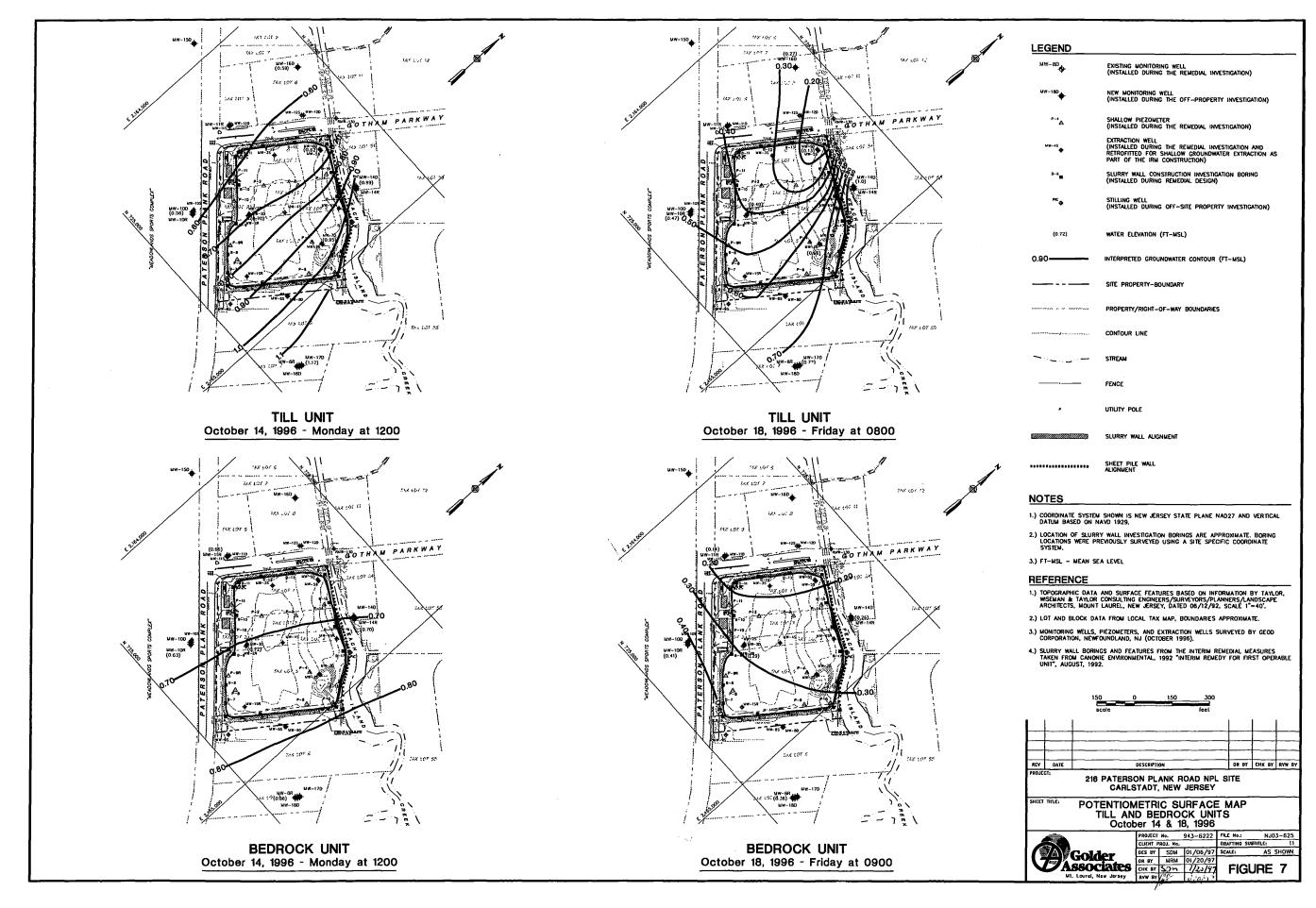
CONCEPTUAL BLOCK DIAGRAM 216 PATERSON PLANK ROAD SITE

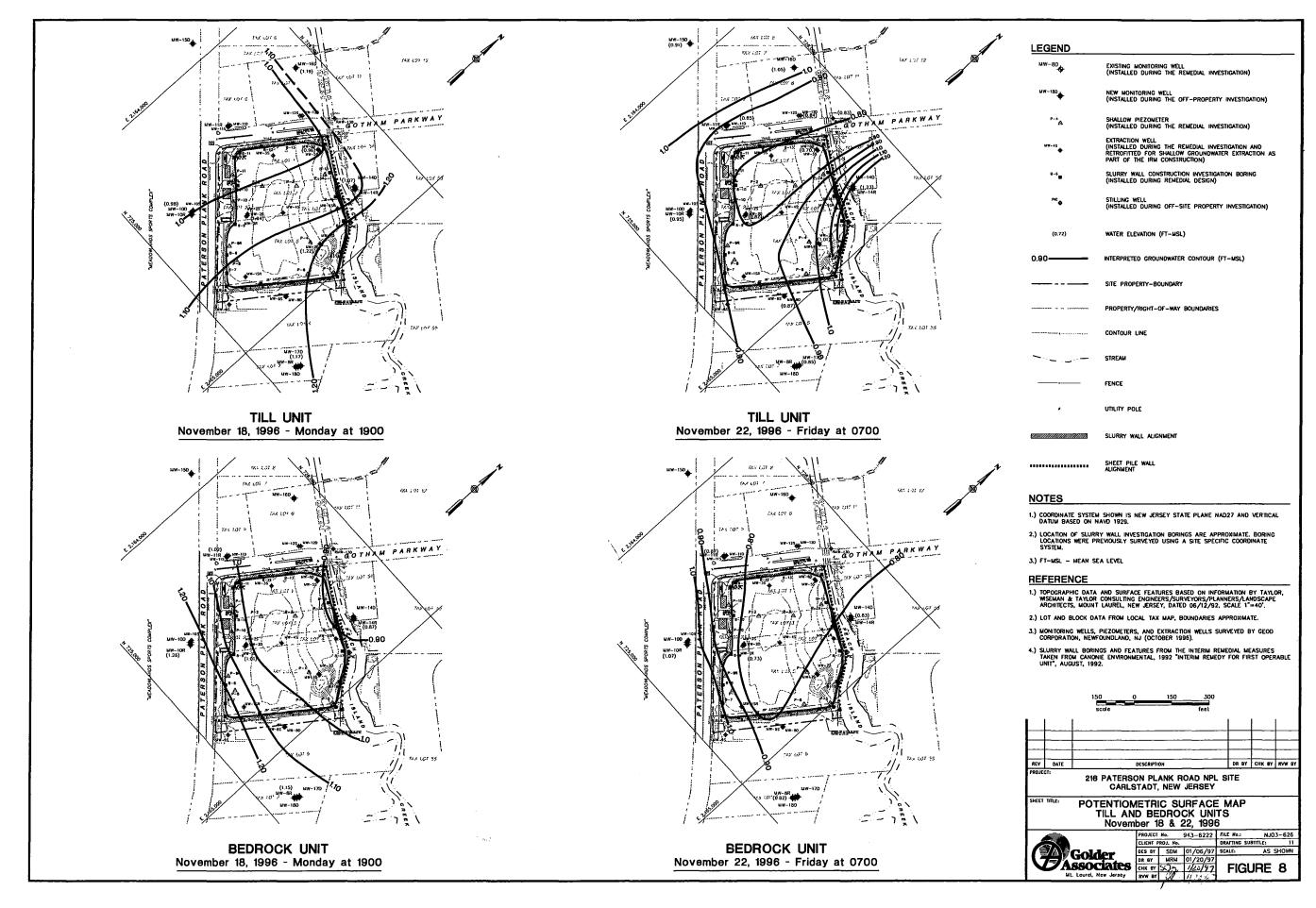


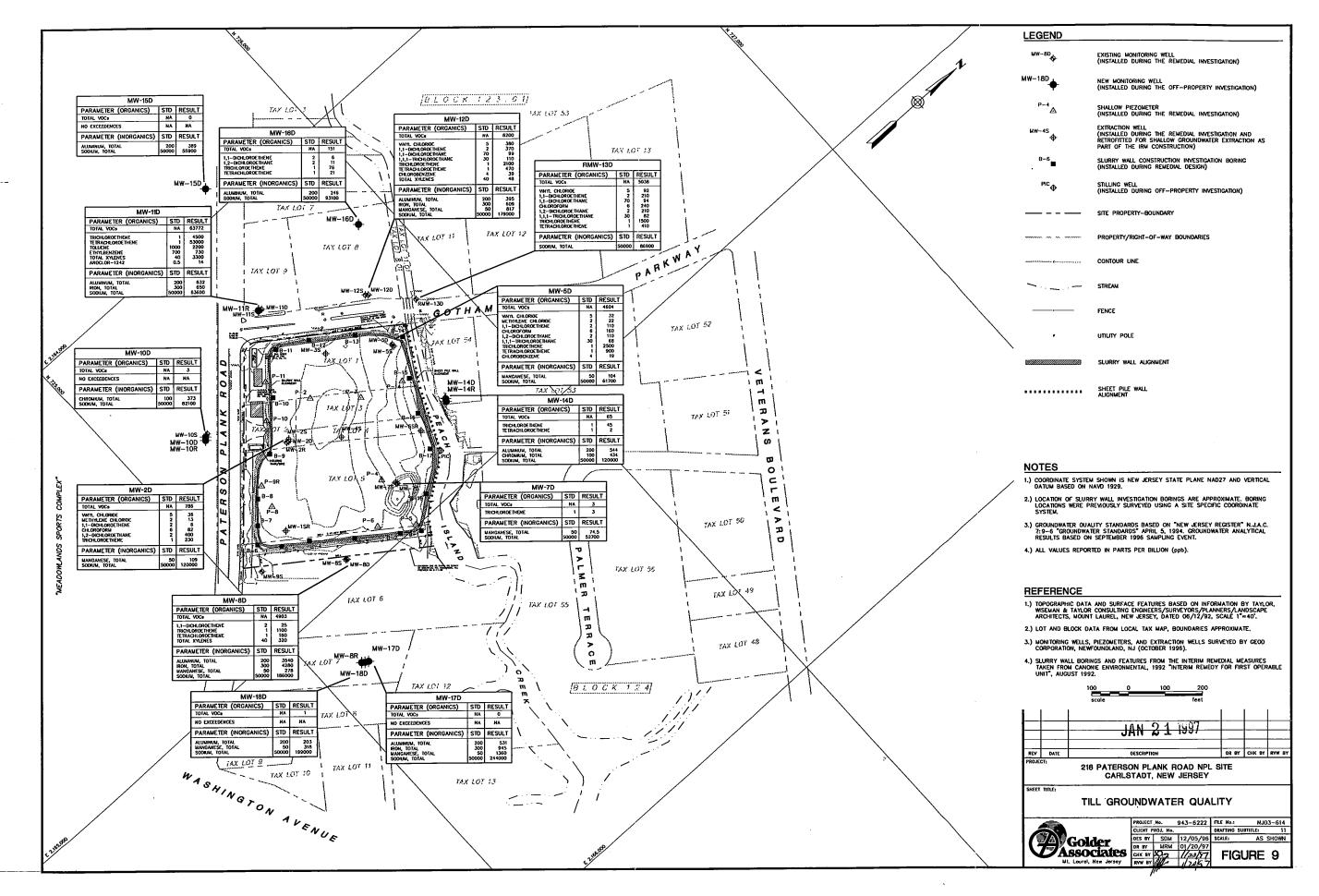
Ramesh Ventatalham

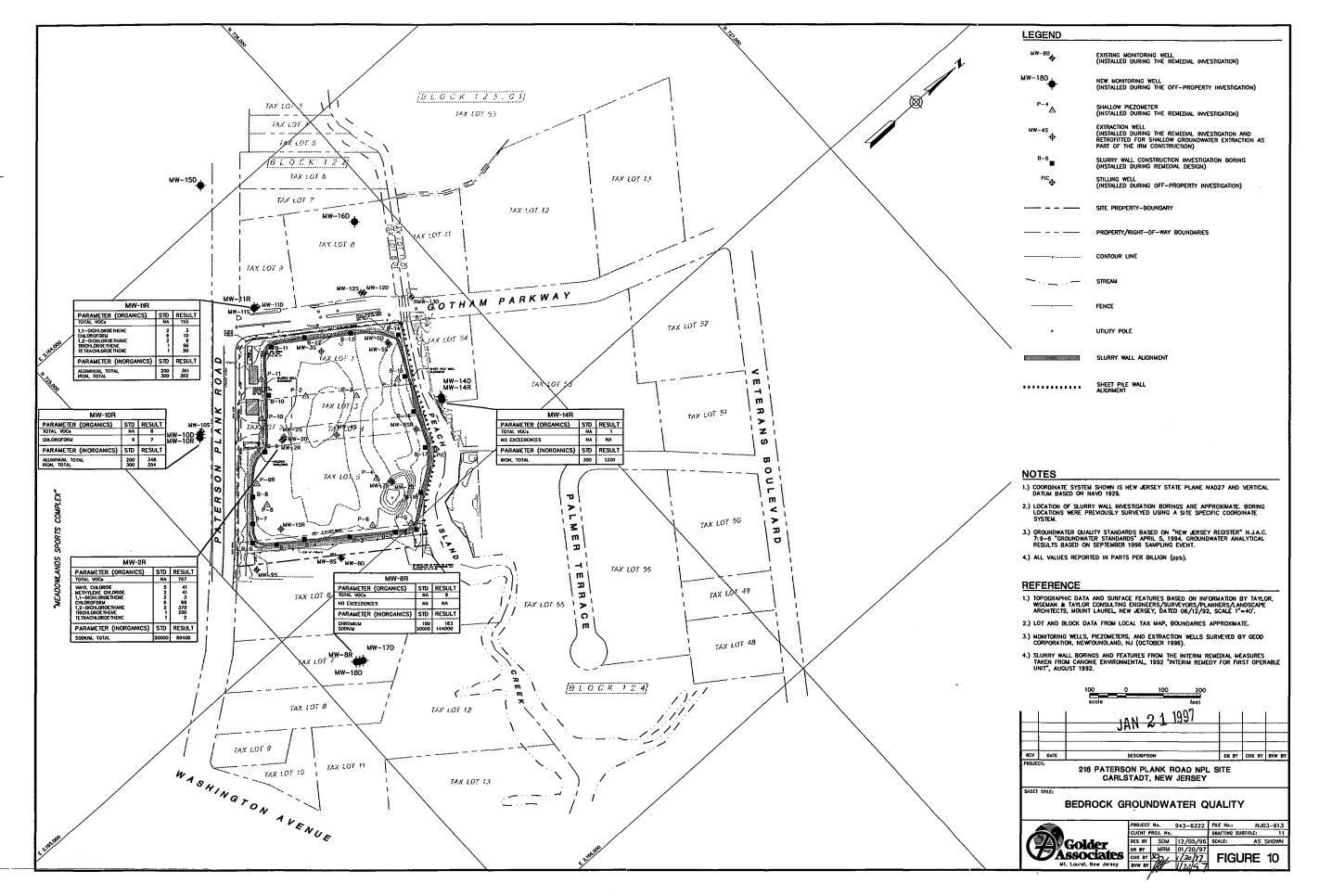


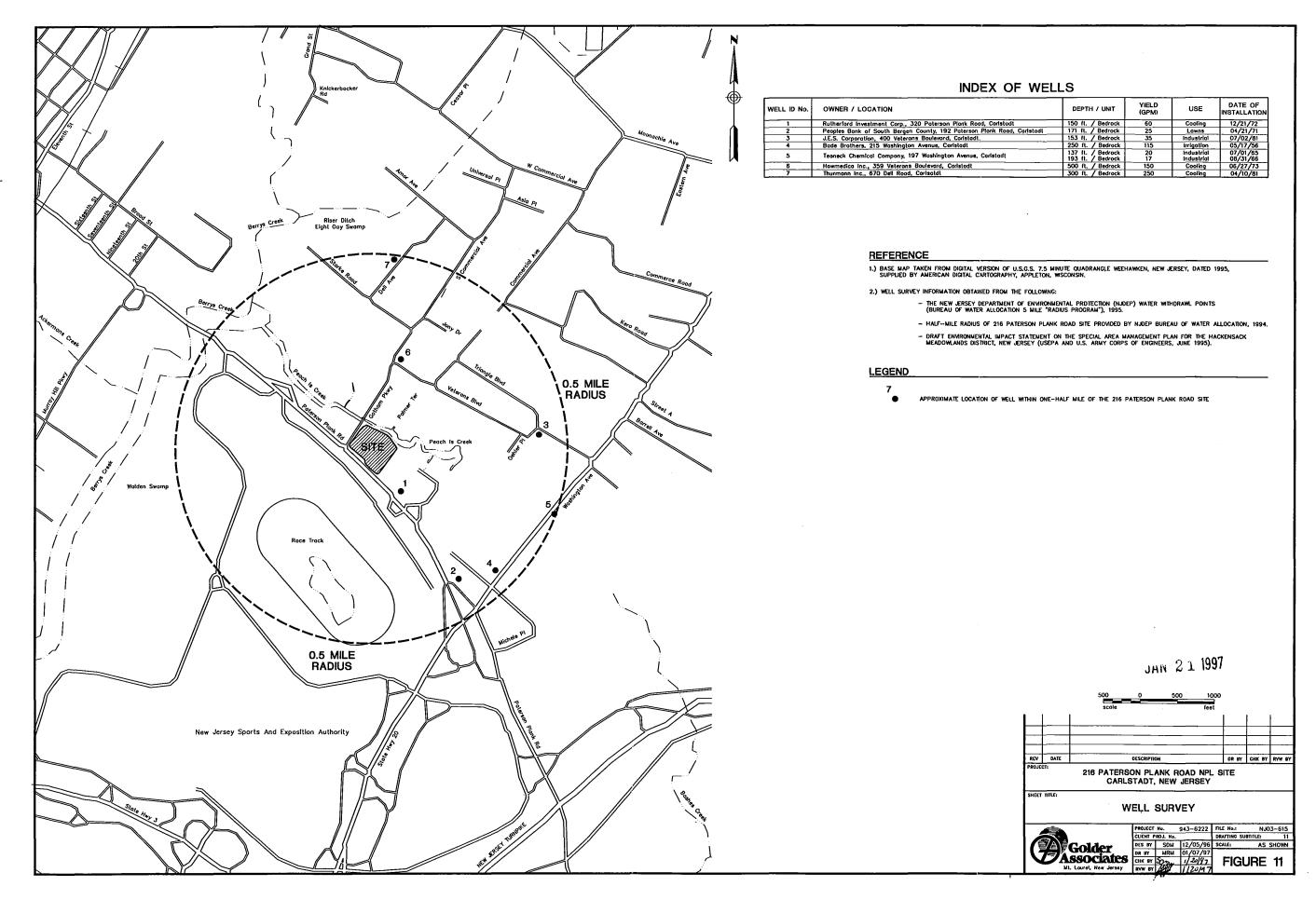












### APPENDIX A

Well Decommissioning Form

New Jersey Department of Environmental Protection Water Supply Element — Bureau of Water Allocation

## WELL ABANDONMENT REPORT

	MAIL TO: Bureau of Water Allocation CN 426 Trenton, NJ 08625-0426  DATE WELL PERMIT # UKNOWN of well sealed DATE WELL SEALED 8-11-94	
	PROPERTY OWNER GOTHOM TIXLUSTIC / Park Property  ADDRESS 320 GOTHOM Parkuay Carlstodt ny  WELL LOCATION 320 GOTHOM Parkuay Carlstodt ny  Street & No., Township, County  MUD13 L+ 11 B1k 123.01  Well No. Lot & Block No.	
	WAS A NEW WELL DRILLED? YES NO PERMIT # OF NEW WELL: 26-42132	· · · · · · · · · · · · · · · · · · ·
)	TOTAL DEPTH OF WELL 43  DIAMETER CASING LENGTH SCREEN LENGTH NUMBER OF CASINGS  MATERIAL USED TO SEAL WELL:  28  Gallons of Water 400  Lbs. of Cement 20  Lbs. of Sand/Gravel (none if well is contaminated)  FORMATION:  Consolidated Unconsolidated  Unconsolidated	展展的主要な主要以来を表現を表現を表現という。 1987年 - 1987年 - 19874年 - 1987年 - 19
	To permit adequate grouting, the casing should remain in place, but ungrouted liner pipes or any other obstructions must be removed. Pressure grouting is the only accepted method.  WAS CASING LEFT IN PLACE? YES NO CASING MATERIAL: Steintess trei	
	WERE OTHER OBSTRUCTIONS LEFT IN WELL? YES YES NO WHAT WERE THE OBSTRUCTIONS:	
)	IF "YES", AUTHORIZATION GRANTED BY  (NJDEP Official)  I certify that this well was sealed in accordance with N.J.A.C. 7:9-9.1 et seq.  (DOX EXINCHES PLOWS  Name of NJ Certified Well Sealer  Address  Mailing Date	
	Performing Work (Print or Type)  Signature of NJ Certified Well Sealer Characteristics #  Performing Work	

90088

COPIES:

White - Water Allocation

Yellow - Owner

Pink - Health Dept.

Goldenrod - Driller

## APPENDIX B

Borehole & Monitoring Well Construction Logs and Forms A & B

R2-0000346

Monitoring Well Construction Logs

	943-6222 PROJECT			MW-8R SHEET 1 of 1
				, 5.35 WATER DEPTH 1.90 BGS
				5.11 DATE/TIME 07-24-96/1135
			T. BROWN STARTED O	740/07-18-96 COMPLETED 1515/07-18-96
LOCATION	/ COORDINATES N 2165174.99		<del></del>	
		MATERIALS I		
				NONE USED NONE USED
H				TALLATION METHOD N/A
•	•			TER PACK QTY, 250 LBS. #1/85 LBS. #0
				TER PACK TYPE MORIE SAND
GROUT TYP	E 2% CEMENT/BENTONITE	DRILLING MUD TYPE	N/A INS	TALLATION METHOD GRAVITY
ELEV./DEPTH	SOIL/ROCK DESCRIPTION	WELL	SKETCH	INSTALLATION NOTES
	For detailed lithologic description,			Drilled using 14" HSA to 13' below
	see boring and drithole log MW-8R.	well cap	–12" dia. flush	ground surface. Pushed 10' steel
-		w/lock-	/ mount steel	casing to 14' bas and grouted in
	GROUND SURFACE		/ protective cover	place. Orilled using 10" HSA to 59'
0.00	0.0-1.0 ft. ASPHALT.	1.00	77777	L[
	1.0-5.0 ft. SAND, some silt with pieces of brick material.		14" dia.	bgs. Cored using NQ barrel to 64' bgs. Drilled using 10" HSA to 65'
-	5.0-7.5 ft. PEAT grading to a		borehole	
	silty clay. 7.5-11.0 ft. Fine SAND, some			bas. Drilled using 4" wash rotary to 59' bas. Cored using NQ barrel to
- 10.00	silt grading to medium sand.			79' bas, Reamed to 79' using 10"
	11.0-17.0 ft. Bedded CLAY grading from fine sand to silt	13.00	10" dia.	wash rotary and set 6" steel casing
-	to clay.		steel casing	and grouted in place. Cored using
	17.0-38.7 ft. Massive CLAY.			NQ barrel to 129' bgs. Grouted to
20.00	<u> </u>		2" dìg.	97' bas and reamed hale to 6" to
	ļ į		stainless steel	a depth of 97'. Installed filter pack
			riser	to 94' bas. Suspended casing and
70.00	ļ <u></u>			screen in hole and installed sand
- 30.00	<u> </u>			pack to 81'. Installed filter pack to
:	ļ <u></u>			80' and grouted to surface using a
	<u> </u>		6" dia.	side discharge tremie pipe. Completed
: ,,,,,,	38.7-45.0 ft. SILTY CLAY,		steel casing	well with a 12" flush mount protective
40.00	trace to little fine to coarse sand, trace to little fine to			cover,
	coarse gravel.			
	45.0-69.0 ft. SILTY CLAY to clayey silt and fine to coarse			
: - 50.00	sand, little to some fine to		-10" dia.	
: 30.00	coarse gravel.		borehole	WELL DEVELOPMENT NOTES
[	Ē			
:	ļ <b>i</b>			-
: - 60.00	<u> </u>			
	ŧ			
-	<b>.</b>		grout density	
	Ę		14.0 lb/gal	
70.00	69.0-123.5 ft. Thinly bedded			-
	brick red SILTSTONE.			
-	<u> </u>			-
	E	79.00	6" dia.	
80.00	<u>t</u>	80.00	steel casing	
	Ę.	83.00	2" dia.	
	<u>E</u>		- <del>  2   a</del> la. -   continuous wrap	LEGEND
	Ę		_   stainless steel	LEGEND
90.00	Ė		well screen	CONCRETE PAD
	Ę.	93.00	flush threaded	
.	Ę	97.00	end cap	CEMENT/BENTONITE GROUT
	Ę.	97.00	6" dia.	
100.00	_ <b>_</b>	[//	borehole	#0 FILTER PACK
	123.5-129.0 ft. Massive brick			70 12121 7001
	red, fine SANDSTONE.	[ //	4" dia. corehole	#1 MORIE SAND
	BORING TERMINATED AT 129.0 FT. BELOW GROUND SURFACE.	129.00 🗸	ر ،	
		<u></u>		<u> </u>

<del></del>		HORING WELL INSTALLATION I	
	943-6222 PROJECT		
ii .		HOLLOW STEM AUGER/WASH ROTARY GROUND ELEV.	
		AQUIFER DRILLING AND TESTING COLLAR ELEV.	•
	75° F DRILL RIG FAILING S COORDINATES N 725213.48		50/08-21-96 COMPLETED 1525/08-21-96
LOCATION	COORDINATES 14 723213.46	MATERIALS INVENTORY	<del></del>
CASB	4 h dla 37	MATERIALS INVENTORY  I.f. WELL SCREEN 4 n. dlo, 5 I.f. BEN	NONE USED
		SCREEN TYPE 304 STAINLESS STEEL INST	
Н		NGS SLOT SIZE	
		CENTRALIZERS NONE USED FILT	
		DRILLING MUD TYPE N/A INST	
ELEV./DEPTH	SOIL/ROCK DESCRIPTION	WELL SKETCH	INSTALLATION NOTES
	For detailed lithologic description,	-1	<u> </u>
ŧ	see boring and drillhole log MW-10R.	well cap —12" dia. flush	Drilled using 12" hollow stem auger to 20' below ground surface. Pushed
Ė		w/lock-\ / mount steel	8" steel casing to 21' bas and
	GROUND SURFACE	protective cover	grouted in place. Drilled using 8"
0.00	0.0-0.2 ft. TOPSOIL. 0.2-4.0 ft. SILT, ironstone	-1.00	wash rotary to 42' bas. Placed
Ė	from 3.0-4.0 ft.		screen and casing in hole and
ŧ	4.0-6.5 ft. CLAYEY SILT. 6.5-10.0 ft. PEAT grading to	12" dia.	installed sand pack to 36.5° bgs.
10.00	silty clay.	borehole	Installed filter pack to 35.5' and
ŧ	10.0-14.0 ft. Firm SAND and SILT, interlayered clay.	grout density	grouted to surface using a side
ŀ	14.0-18.0 ft. Bedded CLAY, grading from fine sand to silt	14.0 lb/gal	discharge tremie pipe. Completed
•	nto clay.		well with a 12" flush mount
20.00	18.0-26.0 ft. Massive CLAY.	20.00 8" dia.	protective cover.
ŧ		steel cosing	
ŧ	26,0-42,0 ft. SILTY CLAY,	grout_density 8" dia.	
70.00	trace to some fine to coarse sand, trace gravel.	13.7 lb/gal borehole	
30.00	sulla, trace gravel.	4" dia.	
Ė		35.50 stainless steel	
		37.00	
40.00		4" dia.	
	BORING TERMINATED AT 42.0 FT.	42.00 stainless steel well screen	
<u> </u>	BELOW GROUND SURFACE.	flush threaded	
ł		end cap	
50.00			WELL DEVELOPMENT NOTES
		-	
ŧ			
60.00		-	
60.00			
<u> </u>			<u> </u>
		<u> </u>	
70.00		<u> </u>	
80.00		·	
		Í	LEGEND
- 90.00			CONCRETE PAD
			CEMENT/BENTONITE GROUT
100.00			#O FILTER PACK
-  -  -  -			#1 MORIE SAND

			MW-10R SHEET 1 of 1
		LOW STEM AUGER/WASH ROTARY/CORING GROUND	
		AQUIFER DRILLING AND TESTING COLLAR E	
ТЕМР	80° F DRILL RIG FAILING	STRATA STAR 10 DRILLER T. BROWN STARTED	0837/08-23-96 COMPLETED 1353/08-26-96
LOCATION	/ COORDINATES N 725207.45		THE Y DATE
į		MATERIALS INVENTORY	
WELL CASE	NG 2 In. dla. 55.5	I.f. WELL SCREEN 2 in. dia 10 i.f.	BENTONITE SEAL NONE USED
		SCREEN TYPE 304 STAINLESS STEEL	
		INGS SLOT SIZE 0.010" MACHINE SLOTTED	•
		CENTRALIZERSNONE_USEDORILLING MUD_TYPEN/A	
GROOT TIP		OKILLING MOD TIPE	INSTALLATION METHOD
ELEV./DEPTH		WELL SKETCH	INSTALLATION NOTES
Ė	For detailed lithologic description, see boring and drillhole log NW-10R.		Drilled using 12" hollow stem auger
ļ.		well cap12" dia, flush w/ lock mount steel	to 20' below ground surface. Pushed
<b>!</b>		protective cov	
- 0,00	GROUND SURFACE	1.00	grouted in place. Drilled using 8"
F 0.00	0.2-4.0 ft. SILT, ironstone from 3.0-4.0 ft.		HSA to 45.5' bgs. Cored using NQ
	4.0-6.5 ft. CLAYEY SILT.		barrel to 55.5' bas. Reamed using
	6.5—10.0 ft. PEAT grading to silty clay.	12" dia. borehole	8" air ratary to 55,5' bgs. Installed 4" steel casing in hole and grouted
- 10.00	10.0-14.0 ft. Firm SAND and		in place. Cored using HQ barrel to
<u>E</u>	SiLT, interlayered clay.	grout dens 14.0 lb/ga	ity L
Ē	14.0—18.0 ft. Bedded CLAY, grading from fine sand to silt to clay.		Completed with a 12" flush mount
- 20,00	18.0-26.0 ft. Massive CLAY.	20.00 8" dig.	protective cover.
-		21.00 8" dia. steel cosing	<u>[</u>
ļ			
	26.0-42.0 ft. SILTY CLAY, trace to some fine to coarse	8" dia. borehole	
30.00	sand, trace gravel.		<u>[</u>
		4" dig.	[
		steel casing	
			[
40.00		grout density	
	42.0-44.0 ft. SILTY CLAY and	14.0 lb/gal	
	fine to coarse SAND, some fine to coarse gravel.	2" dia.	
50.00	44.0-65.5 ft. Moderately weathered, thinly bedded, brick	stainless ster	91
- 55.55	red SILTSTONE.		WELL DEVELOPMENT NOTES
			Ę
		- 4" dia.	[
60.00		corehole	
		2" dla.	[
	BORING TERMINATED AT 65.5 FT.	65.50 — continuous wr	
:	BELOW GROUND SURFACE.	well screen	
70.00		flush threaded end cap	, E
-		J.1.5 3.4p	
-			
- 80.00			
	ŧ		
-			
			<u> </u>
90.00	<u> </u>		
•	Ì		
-	ļ.		LEGEND
	ļ		
- 100.00			CONCRETE PAD
<u> </u>	<b>‡</b>		
:	Į.		CEMENT/BENTONITE GROUT
110.00	<u></u>		FI —

	MON	HORING WELL	INSTALLATION	LUG	
	943-6222 PROJECT				
	S. MITCHELL DRILLING METHOD HO				
	SUNNY DRILLING COMPANY				
ТЕМР	85° F DRILL RIG FAILING	STRATA STAR 10 DRILLER	T. BROWN STARTED	1052/08-07-96	COMPLETED 1530/08-07-9
LOCATION	/ COORDINATES N 725551.44	E 2164273.24		IME / DATE	TME / DATE
		MATERIALS	— —		
	NG <u>4</u> In. dla. <u>47.9</u>				
CASING TY	PESTEEL	SCREEN TYPEOI	PEN BOREHOLE IN	ISTALLATION METHOD	N/A
JOHNT TYPE	WELDED	SLOT SIZE	N/A n	LTER PACK QTY	N/A
	ANTITYN/A				
GROUT TYP	E N/A	DRILLING MUD TYPE	<u> </u>	ISTALLATION METHOD	N/A
ELEV./DEPTH	SOIL/ROCK DESCRIPTION	WELL	SKETCH	INSTALL	ATION NOTES
-	For detailed lithologic description,	-		Ll .	
ŧ	see boring and drillhole log MW-11R.	well cap	_24" square flust	<u> </u>	8" hollow stem auger t
F		w/lock-	/ mount steel	F #	round surface. Pushed
ŧ	GROUND SURFACE		protective cover	+1	ing to 21.5' bas and
0.00	10.0-0.5 ft. TOPSOIL.	1.50	////	L	oce. Drilled using 12"
F "	0.5-8.0 ft. SAND, some silt,			F-1	gs. Pushed 8" steel
1	trace to some fine gravel.		18" dia		bas and grouted in
E	8.0-10.0 ft. PEAT.		barehali	P blace nulled	using 8" HSA to 38'.
10.00	10.0-20.0 ft. CLAYEY SILT		<i>[XXX</i> ]		IQ barrel to 48'.
ŧ	grading to a bedded clay grading from fine sand to sit		grout	F	8" wash rotary to
ŀ	clay.		14.0 lb/g	JI	talled 4" steel casing
Ė				· · · · · · · · · · · · · · · · ·	grouted in place.
20.00	20.0-27.7 ft. Massive CLAY.	20.50	-12" dia.		IQ barrel to 58' bas.
ŧ		grout density	steel casing	1-1-	II with a 24" square
-	i i	14.5 lb/gal	-12" dia.	Flush mount v	rell voult.
Ē	27.7-32.0 ft. SILTY CLAY,	30,00	borehole	<u> </u>	<del></del>
30.00	trace to little fine to coarse sand, trace fine gravel.	31.00	8" dia.	<u> </u>	
Ē	32.0-38.0 ft. CLAYEY SILT,		steel casing	E	
ļ:	little to some fine to coarse sand, little to some fine to		→- 8" dìa.	<u> </u>	
ŧ	coorse grovel. 138.0-38.6 ft. SILTSTONE.		borehole	El	
40.00	38.6-43.6 ft. Fine grained		grout density	<u> </u>	
ŀ	massive SANDSTONE.		14.2 lb/gal	<u> </u>	
ŧ	43.6-58.0 ft. SILTSTONE."		4" dia.	<u> </u>	
Ē		48,00	steel casing		
50.00		-		WELL DEVI	ELOPMENT NOTES
£ .			4" dia.		
ŧ		50.00	open corehole	E	
	BORING TERMINATED AT	58.00		-	
60.00	58.D FT. BELOW GROUND	]		E	
	SURFACE.			<u> </u>	
Ē		]		E	
70.00				F -	_
70.00		]		E	
ļ .		:		EL	
Ę l	<b>!</b>	[			
80.00				E	
80.00					
		:			
Ę į		:		F	
00.00				[	
90.00		:		-	
F				<u> </u>	LEGEND
100.00		]		El (4500)	
100.00	}			CONC	CRETE PAD
E :					
<b>t</b>				CEME	ENT/BENTONITE GROUT
110.00				FI —	

	MON	IITORING WELL INSTALLATION	LOG
JOB NO.		CARLSTADT/FAC. COORD./NJ WELL NO.	
		HOLLOW STEM AUGER/WASH ROTARY GROUND ELE	
ii .		AQUIFER DRILLING AND TESTING COLLAR ELEV	•
ТЕМР,	80° F ORILL RIG MC	DBILE B-59 DRILLER T. BROWN STARTED 1	TIME / BATE COMPLETED 1415/07-26-96
LOCATION	/ COORDINATES N 725767.51	MATERIALS INVENTORY	
WGII CASA	uc 4 batta 30		ENTONITE SEAL NONE USED
CASING TY	E 304 STAINLESS STEEL	SCREEN TYPE 304 STAINLESS STEEL IN	STALLATION METHODN/A
		INGS_SLOT SIZEO.010"_MACHINE_SLOTTEDFIL	
		CENTRALIZERSFIL	
GROUT TYP	E5% CEMENT/BENTONITE	DRILLING MUD TYPE BENTONITE IN	STALLATION METHOOGRAVITY
<u></u>			
ELEV./DEPTH	SOIL/ROCK DESCRIPTION	WELL SKETCH	INSTALLATION NOTES
	For detailed lithologic description, see boring and drillhole log MY-14R.		Drilled using 12" hollow stem auger
Ē.	300 3000 300 300 300 300 300	well cap12" dia. flush	to 14' below ground surface. Pushed
ŧ		w/lock-/mount steel protective cover	8" steel casing to 15' and grouted
	GROUND SURFACE 0.0-1.0 ft. ASPHALT.	1.00 (24/ ) / (24	in place. Orilled using 8" wash
0.00	1.0-5.0 ft. CLAYEY SILT and	-12" dia.	rotary to 41'. Suspended casing and
Ē.	SILTY CLAY. 5.0-8.5 ft. PEAT.	borehole	screen in hole and installed sand
	8.5-13.0 ft. Bedded CLAY		pack to 28' bgs. Installed filter pack to 27' bgs and grouted to
10.00	grading to fine sand, silt and clay.	15.0 lb/gal	the surface using a side discharge
	13.0-24.3 ft, Massive CLAY.	14.00 15.00 8" dia.	tremie pipe. Completed well with a
		steel casing	12" flush mount protective cover.
20.00		grout density 8" dia.	
		13.8 lb/gal borehole	E
-	24.3-29.0 ft. SILTY CLAY,	4" dig.	<u> </u>
	little to some fine to coarse sand, trace fine gravel.	27.00 stoinless steel	[
30.00	29.0—34.5 ft. CLAYEY SILT, some to and fine to coarse	30.00 riser	
	sand, little fine gravel. (33.0- 34.5 ft. Medium to coarse	- 4° dia. continuous wrap stainless steel	)[
	SAND, some silt.)	stoinless steel	
- 40.00	34.5-41.0 ft. SILTY CLAY and CLAYEY SILT, little to some	40.00 flush threaded	
+0.00	fine to coarse sand, trace to some fine to coarse gravel.	41,00 end cap	
	BORING TERMINATED AT 41.0 FT. BELOW GROUND SURFACE.		F
	DEZON OROOND DOM ACE.	-	[
50.00			WELL DEVELOPMENT NOTES
			=
-			
60.00			=
00.00			[]
-			F
			[[
70.00		-	<u></u>
			E
		-	
- 80.00 [			
		<u>-</u>	LEGEND
90.00	:		CONCRETE PAD
<u>-</u> - - -			CEMENT/BENTONITE GROUT
100.00			#0 FILTER PACK
ŧ l			#1 MORIE SAND

JOB NO	943-6222 PROJECT	CARLSTADT/FAC. COORD./NJ WELL	NO. MW-14R SHEET 1 of 1
GA INSP	M. ELSNER DRILLING METHOD HO	DLLOW STEM AUGER/AIR ROTARY/CORING GROUP	NO ELEV. 2.37 WATER DEPTH 2.26' BGS
WEATHER _	CLOUDY DRILLING COMPANY	AQUIFER DRILLING AND TESTING COLLA	R ELEV. 2.22 DATE/TIME 07-23-96/1420
TEMP	70° F DRILL RIG MOBILE B	-59 DRILLER T. BROWN START	ED 0945/07-23-96 COMPLETED 1328/07-23-96
LOCATION	/ COORDINATES N 725763.51	E 2164802.30	TIME / DATE TIME / DATE
,		MATERIALS INVENTORY	•
WELL CASE	uc 4 h dla 34	Lf. WELL SCREEN 4 In. dfg. 10	L.C. RENTONITE SEAL NONE USED
		SCREEN TYPE OPEN BOREHOLE	
		SLOT SIZEN/A	
		CENTRALIZERS NONE USED	
		DRILLING MUD TYPE N/A	
GROOT THE		DRICCING MOD THE	
ELEY./DEPTH	SOIL/ROCK DESCRIPTION	WELL SKETCH	INSTALLATION NOTES
	For detailed lithologic description,		Drilled using 12" hollow stem auger to
£ .	see boring and drillhole log MW-14R.	well cap12" dia. flu	
F		w/lock- / mount stee	
	GROUND SURFACE	protective	Drilled using 8" HSA to 54' bgs.
0.00	10.0-1.0 ft. ASPHALT.	1.00	Cored using NQ barrel to 64' bas.
£	1.0-5.0 ft. CLAYEY SILT and	12" die	
ļ.	SILTY CLAY. 5.0-8.5 ft. PEAT.	boreho	10
ļ.		[	64' bgs. Installed 4" steel casing
10.00	8.5-13.0 ft. Bedded CLAY grading to fine sand, silt and	grout d 14,0 lb	, , ,
ļ:	člay.	14.00	using no parrer to 74 bas.
E	13.0-24.3 ft. Massive CLAY.	15'10" 8" dia.	Completed well with a 12" flush
		steel casi	ng mount protective cover.
20.00	i l		E/
E			Ē
<b>:</b>	24.3-29.0 ft. SILTY CLAY,		F
Ę	little to some fine to course sand, trace fine gravel.	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	<u> </u>
30.00	29.0-34.5 ft. CLAYEY SILT,	—8" dia.	
ļ	some to and fine to coarse sand, little fine gravel. (33.0-	borehole	<u> </u>
E	34.5 ft. Medium to coorse	! W M	<u> </u>
ţ	SAND, some silt.) 34.5-54.0 ft. SILTY CLAY and		<u> </u>
40.00	CLAYEY SILT, little to some	l 1911	. <u>[</u>
+0.00	fine to coarse sand, trace to some fine to coarse gravel.	grout densi	
ļ.	<b>,</b>		<u> </u>
Ē			ţ.
50.00	<b> </b>	4" dia.	WELL DEVELOPMENT NOTES
Į.		steel casi	ng F
F	54.0—74.0 ft. Moderately weathered, thinly bedded, brick	1 1 1 1 1 1	
E .	red SILTSTONE.		
- 60.00		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	
		54.00	
ļ .		.	
E		4" dia.	
70.00		open core	hole F
E		74.00	£
t i	BORING TREMINATED AT 74.0 FT. BELOW GROUND SURFACE.		<u> </u>
F	DELOW GROUND SURFACE.		[
80.00			
<b>!</b>			<u>[</u>
E .		1	
ļ: '			El
90.00			[ <del></del>
ţ.			ţ <del> </del>
ļ.		{	LEGEND
E			ELOCINO
100.00			CONCRETE PAD
Ē.			
<u> </u>			CEMENT/BENTONITE GROUT
E			E CEMENT DENTONITE GROOT
110.00	ı F		<u> </u>

JOB ND	943-6222 PROJECT	CARLSTADT/FAC. COORD./NJ WELL NO.	MW-15D SHEET 1 of 1
GA INSP	M. ELSNER DRILLING METHOD HOL	LOW STEM AUGER/WASH ROTARY/CORING GROUND ELEV	9.68 WATER DEPTH 5.80 BGS
WEATHER _	CLOUDY DRILLING COMPANY	AQUIFER DRILLING AND TESTING COLLAR ELEV.	9.47 DATE/TIME 08-19-96/1034
темр		RRA CT-250 DRILLER T. BROWN STARTED 12	20/08-16-96 COMPLETED 1358/08-16-96
LOCATION	/ COORDINATES N 725666.52	E 2163930.32	TIME / DATE TIME / DATE
ĺ	•	MATERIALS INVENTORY	
WELL CASIN	vG4 In. dla50		ITONITE SEAL NONE USED
CASING TY	PE304 STAINLESS STEEL	SCREEN TYPE 304 STAINLESS STEEL INS	TALLATION METHODTREMIE_PIPE
JOINT TYPE	FLUSH THREADED W/ Q-R	NGS SLOT SIZEO.010" MACHINE SLOTTEOFILT	ER PACK QTY. 50 LBS. #1/10 LBS. #0
GROUT OU	ANTITY 110 GALLONS	CENTRALIZERS NONE USED FILT	ER PACK TYPE MORIE SAND
GROUT TYP	E 5% CEMENT/BENTONITE	DRILLING MUD TYPE N/A INS	FALLATION METHODGRAVITY
l ——	····		
ELEV./DEPTH	SOIL/ROCK DESCRIPTION	WELL SKETCH	INSTALLATION NOTES
ELEV./DEP IN	For detailed lithologic description,	WEEL SKETON	
i.	see boring and drillhole log MW-15D.		Augered to 21' below ground surface.
-		well cap12" dia, flush w/ lock / mount steel	Pushed 8" steel casing to 23' bas
ŧ		protective cover	and grouted in place. Sampled to
0.00	GROUND SURFACE  1 0.0-0.5 ft, TOPSOIL.	1.00	53.5'. Cored to 58.5'. Grouted
ŧ "."	0.5-6.0 ft. Fine to medium	:	6 gallons up to 52'. Reamed to
F	SAND, little fine gravel ngrading to silty sond.		52' using 8" wash rotary.
F	6.0–10.0 ft. FILL.	12" dia. borehole	Suspended casing in hole and installed sand pack to 49.5'.
10.00	10.0-13.0 ft. PEAT.		Installed filter pack to 49.5' and
ŧ.	13.0-16.0 ft. CLAYEY SILT	grout density	grouted to the surface using a side
ŧ	and SILTY CLAY.	13.9 lb/gal	discharge tremie pipe. Completed
	16.0-21.0 ft. Bedded SILTY CLAY grading to fine sand		well with a 12" flush mount
20.00	to silt to clay.		protective cover.
	21.0-42.0 ft. Mossive CLAY.	steel casing	
į.			
- 30.00			
30.00		8" dig. borehgle	
		grout density	
40.00			·
	42.0-47.0 ft. CLAY, some	4" dia.	
-	fine to coarse sand.	stoinless steel riser	
	47.0-53.5 ft. CLAYEY SILT	48.50	
50.00	grading to silty clay, some tine to coarse sand, some	50.00 4" dia.	WELL DEVELOPMENT NOTES
	fine to coarse gravel. 53.5-58.5 ft. SILTSTONE.	52.50 continuous wrap	
	55.5-56.5 ft. SILISTONE.	well screen	
50.00	BORING TERMINATED AT 58.5		
60.00	FT. BELOW GROUND SURFACE.	end cap	
	Į.	-4" día. corehole	
;	<b>]</b>	]	
70.00		[	
	ŧ		
	<u> </u>	<u> </u>	
80.00			
	Ė		
-	<u> </u>	 	LEGEND
	[		
90.00		Į	CONCRETE PAD
[	Į.	[	[77]
	ļ	[	CEMENT/BENTONITE GROUT
100.00	· E	ļ Ē	[2000000]
	ţ	[	#0 FILTER PACK
-	ŧ	<u> </u>	#1 MORIE SAND
110.00	. [	[	#1 MORIE SANO
110.00	<u></u>	<u> </u>	

				_
JOB NO	943-6222 PROJECT			
				7.25 WATER DEPTH 5.87 BGS
				6.59 DATE/TIME 08-01-96/0910
темР	80° F DRILL RIG MOBILE	B-59 DRLLER T.	BROWN STARTED 11	05/07-29-96 COMPLETED 1445/07-29-96
LOCATION	/ COORDINATES N 725909.76	E 2104281.37		TIME / DATE
		MATERIALS INV		
				ITONITE SEALNONE_USED
	PE 304 STAINLESS STEEL			
8	-			er pack qty. <u>450 LBS. #1/50 LBS. #0</u>
				ER PACK TYPEMORIE_SAND_
GROUT TYP	E 5% CEMENT/BENTONITE	DRILLING MUD TYPE	N/A INS	TALLATION METHOD GRAVITY
ELEV./DEPTH	SOIL/ROCK DESCRIPTION	WELL SI	KETCH	INSTALLATION NOTES
	For detailed lithologic description,			D.Wd 40" b-W
ŧ	see boring and drillhole log MW-16D.	well cap	,—12" día, flush	Drilled using 12" hollow stem auger
-		w/ lock-	/ mount steel	to 16' below ground surface. Pushed  8" steel casing to 17' bas and
ŀ	GROUND SURFACE		protective cover	grouted in place. Drilled using 8"
0.00	0.0-4.0 ft. Fine SAND, some	1.00	V	HSA to 40' bas. Cored using NQ
[	silt, trace coarse gravel.		-12" dia.	borrel to 45' bgs. Grouted up to
Ē	4.0-12.0 ft. CLAYEY SILT, some to and fine to coarse		borehole	37' bgs. Suspended casing in hole
10.00	sand, trace to little fine to coarse gravel.		grout density	TI
10.00			14.0 lb/gal	Installed filter pack to 27' and
Ė	12.0-15.0 ft. Bedded CLAY grading to silt to clay.			grouted to the surface using a side
Į.	16.0-20.0 ft. Mossive CLAY.	<u>16.00</u>	8" dia.	discharge tremie pipe. Completed
20.00		grout density	steel casing	well with a 12" flush mount
20.00	20.0-23.8 ft. SILTY CLAY.	14.2 lb/gal	8" dia. borehole	protective cover.
1	23.8-33.5 ft. SILTY CLAY,		<i>V 1</i>	
È	some fine to coarse sand, trace fine to coarse gravel.	27.00 28.00	4" dia.	<u> </u>
30.00		31.00	riser	- 
Ē	]		4" dio.	
ŀ	33.5-36.0 ft. CLAYEY SILT and	36.00	-{} continuous wrop}	] <del></del>
Ī	trace to little fine to coarse	37.00	stainless steel well screen	
40.00	gravel. 36.0-38.0 ft. SILTY CLAY,	40.00	<del>[</del> * ]	-
ŧ	some fine to coarse sand,		flush threaded end cop	
F	BORING TERMINATED AT 45.0 FT.	45.00 Y//	₹ end cop	<del></del>
ŧ	BELOW GROUND SURFACE.		4" dig.	
50.00			corehole	WELL DEVELOPMENT NOTES
ŀ	i I			
-	[		È	
f	i F			
60.00	1			
ļ.	]			
E	j			
- 70.00	ļ			
70.00				·
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	l E			
80.00	) <u>}</u>			·
	l			
	[		į	LEGEND
	\			LEGEND
90.00				CONCRETE PAD
[			‡	OUNCE TAIL
	į į		E	CEMENT/BENTONITE GROUT
·	]		ļ	
100.00			E	#0 FILTER PACK
			ŧ	70
<u> </u>	<u> </u>		Ē	#1 MORIE SAND
t			ļ.	"

JOB NO	943-6222 PROJECT	CARLSTADT/FAC. COORD./NJ WELL NO.	
и		AQUIFER DRILLING AND TESTING COLLAR ELEV.	
	N/A DRILL RIG MOI	BILE 8-59 DRILLER T. BROWN STARTED OF	030/07-11-96 COMPLETED 1110/07-11-96 TAVE / DATE
LOCATION	/ COORDINATES N 725130.54	E 2165184.87	<del> </del>
Ĭ	4 45	MATERIALS INVENTORY	NONE HEED
		LIT, WELL SCREEN 4 In. dio. 10 I.I. BEN SCREEN TYPE 304 STAINLESS STEEL INS	
T.		NGS SLOT SIZE	
R	•	CENTRALIZERS NONE USED FILT	
	_		
ELEV (SERRI	SOIL/ROCK DESCRIPTION	WELL SKETCH	INSTALLATION NOTES
ELEY./DEPTH	For detailed lithologic description,	THEE SILE FOR	
ŧ	see boring and drillhole log NW-8R.	well cap —12" dia. flush	Augered to 14' below ground surface.
F		well cap —12" dia, flush w/ lock — / mount steel	Pushed 8" steel casing to 15' bgs
Į.	GROUND SURFACE		and grouted in place. Drilled using 3" wash rotary to 56' bgs. Reamed
0.00	0.0-1.0 ft. ASPHALT.	1.00	to 8" using wash rotary. Suspended
<u>E</u>	1.0-5.0 ft. SAND, some silt with pieces of brick moterial.	12" dia. barehole	casing in hole and installed sand
ŀ	5.0-7.5 ft. PEAT grading to a silty clay.	E Darenois	pack to 43' bgs. Installed filter
10.00	7.5-11.0 ft. Fine SAND, some silt grading to medium sand.	grout density 14.8 lb/gal	pack to 42' bas and grouted to
ŧ	11.0-17.0 ft. Bedded CLAY	14.8 107 901	surface using a side discharge
-	grading from fine sand to silt to clay.	15.00 8" dia.	tremie pipe. Completed well with
-	17.0-38.7 ft. Massive CLAY.	steel casing	a 12" flush mount protective cover.
20.00			
Ė		- 8" dia. borehole	<u> </u>
-			
70.00		grout density	
- 30.00		14,2 lb/gal	
ŧ			
		4" dia. stainless steel	
40.00	38.7-45.0 ft. SILTY CLAY,	riser	*
	trace to little fine to coarse sand, trace to little fine to	43.00	
Ė	coarse gravel. 45.0-56.0 ft. SILTY CLAY to	45.00 4" dia.	
	clayey silt and fine to coarse sand, little to some fine to	continuous wrap	
50.00	coarse gravel.	stainless steel	WELL DEVELOPMENT NOTES
		55.00	
	BORING TERMINATED AT	- 11ush threaded end cap	
60.00	56.0 FT, BELOW GROUND		
60.00	SURFACE.		
70.00		·	
		-	
- 80.00 [		]	
Ē			LEGEND
90.00	,		CONCRETE DAD
		1	CONCRETE PAD
<u>.</u>		<u> </u>	CEMENT/BENTONITE GROUT
			CEMENT/ BENTONITE GROOT
100.00		1	#0 FILTER PACK
		[	" " " " " " " " " " " " " " " " " " " "
-		j	#1 MORIE SAND
F		I F	انتنتا

	943-6222 PROJECT			MW-18D SHEET 1 of 1
				5.23 WATER DEPTH 3.34' BGS
				4.51 DATE/TIME 07-30:-96/1407
			J. JAWORSKI STARTED 11.	38/07-18-96 COMPLETED 1426/07-18-96
HOMADON	/ COORDINATES N 725121.40	E 2165180.32		IIME / DATE
		MATERIALS IN	NVENTORY	
				TONITE SEALNONE_USED
CASING TO	PE304 STAINLESS STEEL	SCREEN TYPE304	STAINLESS STEEL INST	TALLATION METHODN/A
				ER PACK OTY. <u>150 LBS. #1/25 LBS. #0</u>
GROUT QUA	ANTITY 50 GALLONS	CENTRALIZERS	NONE USED FILT	ER PACK TYPE MORIE SAND
GROUT TYP	E 5% CEMENT/BENTONITE	DRILLING MUD TYPE	N/AINS1	TALLATION METHODGRAVITY
ELEV./DEPTH	SOIL/ROCK DESCRIPTION	WELL	SKETCH	INSTALLATION NOTES
-	For detailed lithologic description,		- I	
ļ:	see boring and drillhole log MW-8R.			Augered to 13' below ground surface.
E	!	well cap w/lock-	12" dia. flush mount steel	Pushed 8" steel casing to 15' bas
ļ.		. \	protective cover	and grouted in place. Reamed to
0.00	GROUND SURFACE	1.00		67' using 8" air rotary. Installed
£ 0.00	1.0-5.0 ft. SAND, some silt		12" dia.	well screen and riser. Bottom of
F	with pieces of brick material. 5.0-7.5 ft. PEAT grading to a	: 1/1/	borehole	well at 66.5' bas. Installed sand
E	silty clay. 7.5-11.0 ft. Fine SAND, some		grout density	pack to 61' and filter pack to 60'.
10.00	silt grading to medium sand.		14.5 lb/gol	Grouted to the surface using a side
E	11.0-17.0 ft. Bedded CLAY grading from fine sand to silt	13.00	8" dia.	discharge tremie pipe. Completed well with a 12" flush mount
ļ:	to clay.	- 15.00	steel cosing	protective cover.
Ė	17.0-38.7 ft. Massive CLAY.			protective cover.
20.00				
E			8" dia.	
Ė	ĺ		borehole	
F				
- 30.00 E				
ţ	1		grout density	
E			13.6 lb/gal	
1000	38.7-45.0 ft. SILTY CLAY.			
40.00	trace to little fine to coarse			
F	sand, trace to little fine to coarse gravel.		4" dio.	
Ę	45.0-67.0 ft. SILTY CLAY to clayey silt and fine to coarse		stainless steel	
50.00	sand, little to same fine to		riser	
\$ 50.00	coorse gravel.		<b>1</b> /2 <b>1</b>	WELL DEVELOPMENT NOTES
E				
ļ:			E E	
60.00		60.00	<b>A</b> :	
Ė į		61.50	4" dia.	
-	F	66.50	continuous wrap	
-	BORING TERMINATED AT	67.00	well screen	ļ
70.00	67.0 FT. BELOW GROUND		-flush threaded	
	SURFACE.		end cop	ļ
Ė		•	Į.	
	ļ		<b>\$</b>	
80.00	ļ <u></u>		Ę	
ļ .	<u> </u>		È	[
[	ļ		ļ	LEGEND
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90.00			F	CONCRETE PAD
Ē	ļ Ē		ţ	المقادة المقاد
E			<u>t</u>	CEMENT/BENTONITE GROUT
[ i			Ę	
100.00	ļ		Ę	#0 FILTER PACK
Ę	Į į		Ę	
Ė			· [	#1 MORIE SAND
110.00	ļ Ē		Į.	<u> </u>

Borehole Logs

63

DRILLER: T. BROWN

## **RECORD OF BOREHOLE MW-8R**

BORING START: 06-25-96

SHEET: 1 OF 2

DATUM: MSL



PROJECT LOCATION: CARLSTADT, NEW JERSEY PROJECT NUMBER: 943-6222 BORING LOCATION: N 725114.3 E 2165175.0

	무	SOIL PROFILE		I (1)				SAMPLES				PIEZOMETER
FEET	BORING METHOD	DESCRIPTION	nscs	GRAPHIC LOG	ELEV DEPTH	NUMBER	TYPE	BLOWS / 6 in	z	REC/ATT	REMARKS	OR STANDPIPE INSTALLATION
٥		0.0-1.0 ft. ASPHALT and crushed rock subbase.	_	1444	5.35 0.00 4.35		ĺ				HEAD SPACE READINGS	
		1.0-5.0 ft. Very dense reddish-brown SAND, some silt with pieces of red-brick material. (FILL)			1.00	S-1	88	10,14,50/0	>64	7*/18*	1-2.5 ft. 0.0 ppm	
5					0.35						2.5-5 ft. 0.0 ppm	
		5.0-6.8 ft. Very soft, black organic CLAY with vegetative matter (PEAT). Gray clayey silt is present within the organic clay near the bottom.	PT ML		5.00 -1.45 6.80	S-3	88	1,1,1,1	2	23'/24'	5-7 ft. 0.0·ppm	
		_6.8-7.5 ft. Very soft, gray CLAYEY SILT 7.5-10.8 ft. Stiff to very stiff, greenish-gray, fine SAND, some silt with rusty yellow mottling.	SM		7.50	S-4	SS	5,5,9,7	14	13'/24'	7-9 ft. 0.0 ppm	
10					-5.45	S-5	SS	10,11,16,17	27	13'/24'	9-11 ft. 0.0 ppm	
		10.8-11.0 ft. Compact, reddish-brown, medium SAND, some silt. 11.0-13.0 ft. Very stiff, bedded brownish-gray CLAY, grading from fine sand to silt to clay. Each couplet several mm thick with the fine sand	CL		-7.65 13.00	S-6	SS	11,12,14,16	26	8'/24'	11-13 ft. 0.0 ppm	
15		consisting of gray and yellowish-brown.	CL		13.00	S-7	SS	4,4,3,4	7	20"/24"	13-15 ft. 0.0 ppm	
		13.0-17.0 ft. Firm, bedded gray CLAY, grading from silt to clay.			-11,65	S-8	SS	4,3,4,4	7	18'/24'	15-17 ft. 0.0 ppm	
	CORING	17,0-38.7 ft. Soft, pinkish-gray to light reddish-gray massive CLAY.			17.00	S-9	ss	4,4,4,3	8	24*/24*	17-19 ft. 0.0 ppm	
20	H.S.A./AIR ROTARY/CORING					S-10	SS	3,2,2,2	4	17*/24*	19-21 ft. 0.0 ppm	-
	H.S.A./All					S-11	SS	3,1,3,2	4	21"/24"	21-23 ft. 0.0 ppm	
25						S-12	SS	3,1,1,1	2	12"/24"	23-25 ft. 0.0 ppm	
						S-13	SS	1,1,1,1	2	24"/24"	25-27 ft. 0.0 ppm	
			СН			S-14	SS	1,2,2,2	4	24"/24"	27-29 ft. 0.0 ppm	
30						S-15	SS	2,1,1,1	2	24*/24*	29-31 ft. 0.0 ppm	
						S-16	SS	1,1,2,1	3	24"/24"	31-33 ft. 0.0 ppm	
35						S-17	SS	0,0,1,1	1	241/241	33-35 ft. 0.0 ppm .	
						S-18	SS	0,1,1,1	2	24"/24"	35-37 ft. 0.0 ppm	
		38.7-45.0 ft. Firm to stiff, reddish- brown SILTY CLAY, trace to little fine to coarse sand, trace to little fine to coarse gravel.	CL		-33.35 38.70	S-19 S-20	SS	1,1,1,1	5	24'/24'	37-39 ft. 0.0 ppm 39-41 ft. 0.0 ppm	
40		coalse gravel.		אאו	-34.65 40.00					7	· · · · · · · · · · · · · · · · · · ·	

**Golder Associates** 

#### **RECORD OF BOREHOLE MW-8R**

BORING LOCATION: N 725114.3 E 2165175.0

PROJECT LOCATION: CARLSTADT, NEW JERSEY

PROJECT NUMBER: 943-6222

BORING START: 06-25-96

SHEET: 2 OF

DATUM: MSL



SOIL PROFILE SAMPLES DEPTH SCALE FEET BORING METHOD PIEZOMETER OR STANDPIPE INSTALLATION REMARKS ELEV GRAPHIC DESCRIPTION BLOWS / N 6 in DEPTH -34.65 40.00 38,7-45.0 ft. Firm to stiff, reddish-brown SILTY CLAY, trace to little fine to coarse sand, trace to little fine to 5 201/241 39-41 ft. 0.0 ppm S-20 SS 1,2,3,4 coarse gravel. SS 18'/24" 41-43 ft. 0.0 ppm 5,4,4,4 CL 5,5,6,5 11 19'/24" 43-45 ft. 0.0 ppm 45.0-49.0 ft. Hard, brick red SILTY CLAY, some to and fine to coarse sand, trace to little fine to coarse gravel. S-23 SS 4,36,24,38 60 16"/24" 45-47 ft. 0.0 ppm S-24 SS 25,33,41,50 74 21'/24" 47-49 ft. 0.0 ppm -43.65 49.0-53.0 ft. Hard, brick red to reddish-brown CLAYEY SILT and fine to coarse SAND, little to some fine to coarse gravel. 49.00 49-51 ft. 0.0 ppm 50 S-25 SS 26,72,84,122 156 20'/24" S-26 SS 80,183 183 8'/12' 51-52 ft. 0.0 ppm <u>-47.65</u> 53.00 53.0-59.0 ft. Hard, reddish-brown SILTY CLAY and fine to coarse GRAVEL, some S-27 SS 100/5',100/3' >100 6'/8' 53-53.8 ft. 0.0 ppm 55 15'/17' S-28 SS 46,75,150/5 >225 55-56.5 ft. 0.0 ppm ML-GW S-29 SS 200/5 >200 5'/5' 57-57.5 ft. 0.0 ppm H.S.A./AIR ROTARY.CORING Augered to 59.0 ft. Begin 59.0-60.0 ft. Red SILTSTONE boulder with green alteration and reduction zones. -<u>54.6</u>5 60.00 60.0-69.0 ft. Red brick SILTY CLAY with angular, red siltstone fragments (>2" in diameter) and red siltstone boulders, thinly laminated. CL 65 BORING TERMINATED AT 59.0 FT. BELOW GROUND SURFACE. CORING BEGAN AT 59.0 FT. AND TERMINATED 70 AT 129.0 FT. 75 LOGGED: SDM/MME/RV DRILL RIG: MOBILE B-59 DRILLING CONTRACTOR: AQUIFER DRILLING & TEST. CHECKED: RY **Golder Associates** DATE: 12-02-96 DRILLÉR: T. BROWN

PF	OJECT NO: 943-6222	ORING	RECO	D: H	Q 6-27-9		DR	RIL	Lŀ	10	LE	,	M	W-8R DATUM: COORDI	NATES N	: 72	511	4.3			Sheet 1 of 4 REFERENCE ELEV: E: 2165175.0
DEPTH SCALE (FEET)	CATION: CARLSTADT, NEW JERSEY  ROCK TYPE  DESCRIPTION	GRAPHIC LOG	ELEV DEPTH (F1)	B-Be BR-E C-Cu CA-C	3-59 dding koken rved Calcite Chlorifi	c R	CL-C CO-C F-Fre FA-F FE-Ir	Cont osh ault on	FERACTURES DE	G- I-Ir J-J K-1	R-Frak Grou Tegul Joint Slicke	nd ar nsid	bei	AZIMUTH LI-Limonite MN-Manganese PL-Planar OTZ-Quartz R-Rough SCONTINUITY TYPE A SURFA DESCRIP	SM-Smc SP-Step ST-Step UE-Une W-Wavy DATA ND CE	ped ped ven		CONDICTIVITY	CONDOCINAL CONTRACT		NOTES WATER LEVELS INSTRUMENTATION
- o	For lithologic description from 0.0-59.0 ft., see soil boring log MW-8R.		<b>V</b> 17			09	20		1	8		90	09	DECOM!							
- - - - - -																					-
- 10																					-
																		ì			-
- 20	-																				_
25																					-
30												-									-
<b>-</b> 35																					<u>-</u>
- 40	CONTINUED ON NEXT PAGE										-	-						-			
DF	PTH SCALE: 1 INCH = 5 FEET IILLING CONTRACTOR: AQUIFER DRILLING & TEST IILLER: T. BROWN	ī. <sub>-</sub>	CHE	CKE	: EL D: <b>Q</b> v	1		MA		ı				(	<i>∰</i> G	olde	er.	As	SS	oc	ciates

PR	OJECT NO: 943-6222	BORING	RECC METHOR	D: F	{Q 6-27-9		DF	RIL	LI	10	DL	 E	N	<u></u>	V-8R DATUM: M COORDINAT	TES N:	72	5114	.3		Sheet 2 of 4 REFERENCE ELEV: E: 2165175.0
DEPTH SCALE (FEET)	CATION: CARLSTADT, NEW JERSEY  ROCK TYPE  DESCRIPTION	GRAPHIC LOG	ELEV DEPTH (FT)	B-Be BR-I C-Ce CA-C	edding Broken urved Calcite Chloriti	c R	CL-C CO-C F-Fre FA-F FE-Ir	Con esh ault ron	PACTURES	ER FOOT	Ŧ	kens	OORE AXIS	DIS	MN-Manganese Si PL-Planar S' DTZ-Quartz U	M-Smoo P-Stepp T-Stepp E-Unev /-Wavy	ed be	HYDBALLING	CONDUCTIVITY	cm/sec	NOTES WATER LEVELS INSTRUMENTATION
- 40	CONTINUED FROM PREVIOUS PAGE For lithologic description from	-		-		88	48	-	Ī	-  -	<u>۽ ا</u>	-		-				7.	Н	7	
<b>-</b> 45	0.0-59.0 ft., see soil boring log MW-8R.																				
- 50																					
55	59.0-60.0 ft. Brick red SILTSTONE boulder.		59.00																		
- 60	60.0-61.5 ft. Brick red SILTY CLAY till, very hard. 61.5-62.0 ft. Boulder, 62.0-64.0 ft. Till.		60.00 61.50 62.00	1																	
65	64.0-69.0 ft. No sample.		64.00	2																	300 gallons lost at 64.0 ft.
- 70 - 75	69.0-123.5 ft. Slightly weathered, thinly bedded, calcareous, brick red, slightly micaceous SILTSTONE with greenish-gray reduction spotting. Dissolution vugs <1/2" dia. at 69.0-80.5 ft., 84.0-92.0 ft., and 98.0-111.0 ft. White calcareous spotting within matrix and along fractures.		69.00	3	90																
80	CONTINUED ON NEXT PAGE	1"	80.00					Ĭ		11								Π.		1	
DF	EPTH SCALE: 1 INCH = 5 FEET RILLING CONTRACTOR: AQUIFER DRILLING & TES RILLER: T. BROWN	т.	LOC CHI DAT	GGEE ECKE [E: (	): EL :D: <b>/</b> 2: :01-17-	.SNI √ •97	ERVE	RAN.	/ES	H		٠	•-		E	G	olde	er /	\s:	so	ciates

PROJECT: CARLSTADT/FAC. COORD./I	J BORING DRILLIN	METHOD	): HQ 06-	27-96	RILLH	IOLE	M	W-8R  DATUM: MSL COORDINATES N	l: 725	5114.3		Sheet 3 of 4 REFERENCE ELEV: E: 2165175.0
LOCATION: CARLSTADT, NEW JERSEY  ROCK TYPE  ROCK TYPE  DESCRIPTION	GPAPHIC LOG	ELEV DEPTH (FT)	B-Bedd BR-Bro C-Curv CA-Ca CH-Ch	ding CL- oken CO- red F-Fr lotte FA-	RACTURES	FR-Fracture G-Ground I-Irregular J-Joint K-Sickens	idedi	AZIMUTH: 000  LI-LImorvite SM-Sm MN-Manganese SP-Step PL-Planar ST-Step OTZ-Quartz UE-Une R-Rough W-Way SCONTINUITY DATA  TYPE AND SURFACE DESCRIPTION	ped ped ven	HYDRAULIC	cm/sec	NOTES WATER LEVELS INSTRUMENTATION
- 80 CONTINUED FROM PREVIOUS PA	SE	80.00	4	90								Interconnected fracture/vug zones at 80-81 ft., 83-85 ft., 88-89 ft., and 97-98 ft.
- 90 - 95 - 97.5-98.0 ft. Decomposed.			5	94								100 gallons lost at 96.0 ft.
98.0-99.0 ft. Highly weathered I		99.00	6	32								
113.0-114.0 ft. Missing.  115 115.0 ft. 1 mm Dolomite seam.		115.00	7 1	00								-
CONTINUED ON NEXT PAGE  DEPTH SCALE: 1 INCH = 5 FEET		<u></u>	GED:	ELŞNEFV		<u>                                      </u>	1	<u> </u> (@) G	Щ	Ш		

PR	OJECT NO: 943-6222 D CATION: CARLSTADT, NEW JERSEY D	ORING RILLIN	RECO METHO IG DATE:	D: H	IQ 6-27-1		RI	LL	HC	DL	E	M	W-	BR DATUM COOR AZIMU	DINATI	ES N:	72	5114	.3		Sheet 4 of 4 REFERENCE ELEV: E: 2165175.0 INCLINATION: -90
DEPTH SCALE (FEET)	ROCK TYPE  DESCRIPTION	GRAPHIC LOG	ELEV DEPTH (F1)	BR-I C-Ci CA-C	Broken Broken Broken Calcite Chloriti	F F	O-Co -Fres A-Fa E-Iro	U SOUTTON	ER FOOT X C T D	3-Gre -Irreg I-Joir (-Siic	nt kensi	ded	MN-M PL-P1 QTZ- R-Ro	Quartz ugh VTINUIT TYPE SURI	SO SP ST- UE W-1	-Stepp -Unev Wavy	ed ed	HYDRAUIIC	CONDUCTIVITY	cm/sec	NOTES WATER LEVELS INSTRUMENTATION
- 120 - 125	CONTINUED FROM PREVIOUS PAGE 69.0-123.5 ft. Slightly weathered, thinly bedded, calcareous, brick red, slightly micaceous SILTSTONE with greenish-gray reduction spotting. Dissolution vugs <1/2" dia. at 69.0-80.5 ft., 84.0-92.0 ft., and 98.0-111.0 ft. White calcareous spotting within matrix and along fractures. 121.0-122.0 ft. Dolomite seams. 123.5-129.0 ft. Fresh, massive, calcareous, micaceous, brick red, fine SANDSTONE with white calcareous spotting within matrix and along fractures.		123.50	8	100																
<b>–</b> 130	CORING TERMINATED AT 129.0 FT. BELOW GROUND SURFACE.		129.00																		
- 135																					
- 145																					
- 150																					<u>-</u>
155																					-
DE DR	PTH SCALE: 1 INCH = 5 FEET ILLING CONTRACTOR: AQUIFER DRILLING & TEST.		LOG	CKE	: EL	1	∐ VRA	WES	н	Ш		<u>.</u>			<u>(</u>	Go		r A	L Ass	;os	ciates

PROJECT LOCATION: CARLSTADT, NEW JERSEY

## RECORD OF BOREHOLE MW-10R

BORING START: 08-14-96

SHEET: 1 OF 2 DATUM: MSL



PROJECT NUMBER: 943-6222

BORING LOCATION: N 725207.5 E 2164440.1

ш	۵	SOIL PROFILE	•			Γ		SAMPLES				
DEPTH SCALE FEET	BORING METHOD	DESCRIPTION	SOSN	GRAPHIC LOG	ELEV DEPTH	NUMBER	TYPE	BLOWS / 6 in	N	REC/ATT	REMARKS	PIEZOMETER OR STANDPIPE INSTALLATION
- o		70.0-0.2 ft. Black SANDY SILT with roots. (Topsoil). 0.2-3.0 ft. Hard, brown SILT, little fine to coarse sand, little gravel.	OL ML		0.20	S-1	SS	12,23,25,20	48	12"/24"	HEAD SPACE READINGS 0-2 ft. 0.0 ppm	-
		3,0-4,0 ft. Reddish-brown cemented SILT. (Ironstone?)			4.48 3.00 3.48	S-2	SS	18,30,28,32	58	12'/24'	2-4 ft. 0.0 ppm	
- 5		4.0-6.5 ft. Hard, reddish-brown CLAYEY SILT, trace to little fine to medium sand with pieces of coal and ironstone (up to 1/2" in diameter) at 5.8-6.0 ft., grayish-white cemented, fine to medium			4.00	S-3	ss	18,38,150/5	>150	12'/17'	4-6 ft. 0.0 ppm	
		grayish white cemented, fine to medium sand and fragments of concrete block at 6.0-6.5 ft. 6.5-8.0 ft. Firm, black PEAT, slightly	PT		0.98 6.50 -0.52	S-4	SS	24,5,3,3	8	6*/24*	6-8 ft. 0.0 ppm	
		micaceous. 8.0-10.0 ft. Black, organic SILTY CLAY with vegetative matter (Peat).	OL·PT		8.00 -2.52	S-5	ss	3,5,6,8	11	16'/24'	8-10 ft. 0.0 ppm	
- 10 -		10.0-14.0 ft. Loose to dense, greenish, fine SAND and SILT interlayered clay with yellow-brown mottling. Greenish sandy clay with 1/2" thick layer of brown, fine	SM		10.00	S-6	SS	3,4,5,6	9	16'/24'	10-12 ft. 0.0 ppm	
		sand at 13.0-14.0 ft.			-6.52	S-7	ss	5,15,19,18	34	16'/24'	12-14 ft. 0.0 ppm	
T 15		14.0-18.0 ft. Stiff to very stiff, bedded, grayish-yellowish-brown CLAY, grading from fine sand to silt to clay. Each couplet several mm thick with the fine	CL		14.00	S-8	SS	9,7,8,14	15	20"/24"	14-16 ft. 0.0 ppm	-
	DN:	sand layers < 1/2" mm thick. Coloring varigated consisting of gray and yellow brown.			-10.52	S-9	SS	7,8,8,7	16	24'/24'	16-18 ft. 0.0 ppm	
- 20	rary/cor	18.0-26.0 ft. Stiff to very soft, massive CLAY with alternating colors of gray and pinkish-gray.			18.00	S-10	ss	6,9,5,5	14	24'/24'	18-20 ft. 0.0 ppm	
ì	H.S.A./AIR ROTARY/CORING		СН			S-11	ss	10,3,3,3	6	24'/24'	20-22 ft. 0.0 ppm	
	H.S./					S-12	ss	4,2,2,2	4	24'/24'	22-24 ft. 0.0 ppm	
<b>-</b> 25					-18.52 26.00	S-13	ss	WOR	0	24'/24'	24-26 ft. 0.0 ppm	
		26.0-34.0 ft. Very soft to soft, reddish- brown SILTY CLAY, trace to some fine to coarse sand, trace gravel.			20.00	S-14	SS	WOR,1,1,1	2	24"/24"	26-28 ft. 0.0 ppm	÷
- 30			CL			S-15	SS	2,2,1,2	3	24'/24'	28-30 ft. 0.0 ppm	
						S-16	SS	wor	0	24'/24'	30-32 ft. 0.0 ppm	
		24.0.40.06 Eiro briot and CUTY OLAY			-26.52 34.00	S-17	SS	2,2,2,2	4	24*/24*	32-34 ft. 0.0 ppm	
35		34.0-42.0 ft. Firm, brick red SILTY CLAY, some fine to coarse sand, trace gravel.				S-18	SS	WOR,2,2,3	4	24*/24*	34-36 ft. 0.0 ppm	-
			CL			S-19	SS	2,2,3,3	5	24"/24"	36-38 ft. 0.0 ppm	
- 40			_		-32.52 40.00	S-20	SS	21,3,3,4	6	24'/24'	38-40 ft. 0.0 ppm	
DDI	I BIG	CANTERRA 250/STARR 10	<u> </u>	<u> </u>	Ь.			<u> </u>	<u>.                                    </u>	٠ - دي .	LOGGED: MI	ICHELL/ELSNER
DRI	LLING	CONTRACTOR: AQUIFER DRILLING & TEST. T. BROWN					Gold	er Associa	tes		CHECKED: /2v DATE: 12-02-9	

PROJECT NUMBER: 943-6222

DRILLER: T. BROWN

PROJECT LOCATION: CARLSTADT, NEW JERSEY

## RECORD OF BOREHOLE MW-10R

BORING LOCATION: N 725207.5 E 2164440.1

BORING START: 08-14-96

URING START: 08-14-96

SHEET: 2 OF 2

DATUM: MSL



$T_{i}$		SOIL PROFILE				_		SAMPLES				<del></del>
FEET FEET FOR METHOD	3 METHOD	DESCRIPTION	nscs	GRAPHIC LOG	ELEV	NUMBER	TYPE	BLOWS /	N	REC/ATT	REMARKS	PIEZOMETER OR STANDPIPE
_ <u> </u> ~	BORIN		Sn.	GRAPH	DEPTH	NUN	Ϋ́	6 in		REC		INSTALLATION
40		34.0-42.0 ft. Firm, brick red SILTY CLAY, some fine to coarse sand, trace gravel.	CL		-32.52 40.00 -34.52	S-21	SS	1,2,3,3	5	24'/24'	40-42 ft. 0.0 ppm	
		42.0-44.0 ft. Hard, brick red SILTY CLAY and fine to coarse sand, some fine to coarse gravel.	CL-SW	177	42.00	S-22	SS	18,34,100/4	>134	15'/15'	42-43.4 ft. 0.0 ppm	
45		BORING TERMINATED AT 45.0 FT. BELOW GROUND SURFACE. CORING BEGAN AT 45.0 FT. AND TERMINATED AT 65.0 FT. BELOW GROUND SURFACE.			44.00	S-23	SS	200/4	>200	4*/4*		
50 02	HING											
S S S S S S S S S S S S S S S S S S S	.A./AIR ROTARY/CO											
	H.S											
60											·	
55												
0									-			
5												
BO								11				

**Golder Associates** 

	PR	OJECT NO: 943-6222	BORING DRILLIN	RECO METHO IG DATE: IIG: STA	D: N	IQ/HQ 8-20-9	)	DR	IL	LH	10	LE		M	COOR	M: MSL DINATES N TH: 000	l: 72	5207	.5		Sheet 1 of 2 REFERENCE ELEV: E: 2164440,1 INCLINATION: -90
)	DEPTH SCALE (FEET)	ROCK TYPE  DESCRIPTION	GRAPHIC LOG	ELEV DEPTH (FT)	BR-6 C-Ca CA-0 CH-0	BECONER PROPERTY OF THE PROPER	R	CL-C CO-C F-Fre FA-F: FE-In	contacts	4 FRACTURES 25 A	EH FOOT   3X という 25 に 15 で 1	Frac Groun reguli loint Siicke	nd er nside	ed	LI-Limonite MN-Mangane PL-Planar OTZ-Quartz R-Rough SCONTINUIT TYPE SURI DESCF	ST-Step UE-Une W-Wavy	ped ven	CI #I WORK	CONDUCTIVITY	cm/sec	NOTES WATER LEVELS INSTRUMENTATION
	. 5	For lithologic description from 0.0-44.5 ft., see soil boring log MW-10R.																			
	• 10																				-
)	15	-																			<u>-</u>
	25																				,
	30																				
-		CONTINUED ON NEXT PAGE  PTH SCALE: 1 INCH = 5 FEET  IILLING CONTRACTOR: AQUIFER DRILLING & TES				: МП D: <b>Р</b> :		ELL	/ELS	SNE	R						old:				

Г			RECO				ILLI	HC	LE		M۱	W-10R					Sheet 2 of 2
1 (	PROJECT: CARLSTADT/FAC. COORD./NJ PROJECT NO: 943-6222 LOCATION: CARLSTADT, NEW JERSEY	DRILLIN	METHOR G DATE: NG: STA	0	IQ/HC 8-20-1	96						DATUM: M COORDINA AZIMUTH:	TES N:	728	5207.	5	REFERENCE ELEV: E: 2164440.1 INCLINATION: -90
DEPTH SCALE	DESCRIPTION	GRAPHIC LOG	ELEV DEPTH (FT)	BR-E C-Cc CA-C CH-C	Broken Broken Lived Calcite Chloriti	CO-C F-Fre: FA-Fa	onlact sh suit on	ER FOOT X C II S	F	indi iar	DIS	MN-Manganese S PL-Planar S QTZ-Quartz U	SM-Smoo SP-Steppe ST-Steppe JE-Uneve W-Wavy ATA	ed ed	HYDRAULIC	CONDUCTIVITY cm/sec	NOTES WATER LEVELS INSTRUMENTATION
- 44	0.0-44.5 ft., see soil boring log MW-10R.																
50	pedged, calcareous, prick fed, signity micaceous SILTSTONE with greenish-gray reduction spotting. Dissolution vugs <1/2" dia. at 51.0-53.0 ft. and 55.5-65.5 ft.		44.50	1	83												Lost 150 gallons of water to formation during run 1.
- 5: - 6:				3	90												Lost 400 gallons of water to
- 6	CORING TERMINATED AT 65.5 FT. BELOW GROUND SURFACE.		65.50														formation during run 4.
$\vdash$	DEPTH SCALE: 1 INCH = 5 FEET DRILLING CONTRACTOR: AQUIFER DRILLING & TE	ST.	LOC	GGED	: MI	TCHELL	ELSNI	ER					A) Go	olde	er A	Asso	ociates

PROJECT NUMBER: 943-6222

DRILLER: T. BROWN

PROJECT LOCATION: CARLSTADT, NEW JERSEY

#### RECORD OF BOREHOLE MW-11R

BORING START: 07-26-96

BORING LOCATION: N 725551.4 E 2164273.2

SHEET: 1 OF 2

DATUM: MSL



SOIL PROFILE SAMPLES PIEZOMETER DEPTH SCA FEET SORING MET OR STANDPIPE REMARKS **ELEV** DESCRIPTION BLOWS / N INSTALLATION 6 in DEPTH 6.41 0.0-0.5 ft. Very stiff, black organic SILT and fine SAND. (Topsoil) 0.5-2.0 ft. Very dense, reddish-brown OL 0.00 HEAD SPACE READINGS 0-2 ft. 0.0 ppm 241/241 S-1 SS 10.15.27.19 42 SAND, some silt, some pieces of concrete 2.00 2.0-3.5 ft. Very dense, reddish-brown SAND, some silt, some fine to coarse SM 2-4 ft. 0.0 ppm 241/24 SS 21,25,29,29 S-2 2.91 3.50 gravel. 3.5-8.0 ft. Very dense to loose, brown to tan, fine to medium SAND, some silt, little to trace fine gravel. SS 20,37,15,11 52 241/241 4-6 ft. 0.0 ppm SM SS 4,4,4,3 241/241 6-8 ft. 0.0 ppm 8.00 8.0-10.0 ft. Soft, dark brown organinc SILT with vegetative matter, trace fine 2,2,2,2 24'/24' 8-10 ft. 2.5 ppm sand. (Peat) 10 10.0-14.0 ft. Very stiff, bluish-gray and brownish-red CLAYEY SILT, trace to little fine sand, trace to little fine 10.00 10-12 ft. 0.0 ppm SS 10,11,13,20 24"/24" ML SS 14,11,10,15 21 24'/24' 12-14 ft. 0.0 ppm S-7 14.0-16.0 ft. Stiff to firm, bedded, bluish-gray CLAYEY SILT grading to a silty clay with layers of fine sand 14.00 ML S-8 SS 5,6,8,9 14 241/241 14-16 ft. 60.0 ppm >1/2 mm thick. 16.0-20.0 ft, Stiff to firm, bedded, -9.59 16.00 holibush-gray CLAY grading from fine sand to silt to clay. Each couplet several mm thick with fine sand layers < 1/2 mm thick. Coloring varigated consisting of gray and yellowish-brown. Discoloration S-B SS 5,7,7,6 24"/24" 16-18 ft. 100.0 ppm ROTARY/CORIN CL SS 4,4,3,4 241/241 18-20 ft. 140.0 ppm noted within the fine sand and silt layers (black). 20 20.0-24.0 ft. Firm to very soft, reddish-brown and pinkish-gray, massive CLAY. 20.00 .. WASH SS 4,4,4,4 24"/24" 20-22 ft. 0.0 ppm СН SS 241/241 22-24 ft. 0.0 ppm S-12 1.1.1.1 2 -17.59 24.00 24.0-27.7 ft. Firm, pinkish-gray CLAY, trace to little fine to coarse sand, trace gravel, trace fine sand in < 1/2 mm thick layer. At 27.5 ft., < 1/2 mm thick fine sand layer with black discoloration. 241/241 24-26 ft. 1.3 ppm 25 SS 2,2,2,2 СН SS 241/24 26-28 ft. 350.0 ppm 5 1,2,3,4 -21.29 27.70 27.7-30.0 ft. Firm to very stiff, brick red SILTY CLAY, trace to little fine to coarse sand, trace fine gravel. 24"/24" SS 12 28-30 ft. 0.0 ppm 3,4,8,4 30 30.0-31.8 ft. Stiff, pinkish-gray CLAY and brick red SILTY CLAY, trace fine to ÇL SS 2,5,4,5 9 24"/24" 30-32 ft. 0.0 ppm S-16 coarse sand, trace fine gravel. -25.39 31,8-32 ft. 0.0 ppm 31.8-32.0 ft. Stiff, brick red SILTY 32.00 CLAY, trace to little fine to coarse sand, trace fine gravel. SS 11,15,23,24 38 241/24 32.0-38.0 ft. Hard, brick red to reddish-brown CLAYEY SILT, little to some fine to coarse sand, little to some fine to coarse gravel. 2'/4' 34-34.2 ft. 0.0 ppm SS 100/4 > 100 S-18 ML 35 S-19 SS 28,54,78,34 132 12"/24" 37-37.3 ft. 0.0 ppm 7\*/9\* SS 41,100/5 > 100 S-20 BORING TERMINATED AT 38.0 FT BELOW GROUND SURFACE. CORING BEGAN AT 38.0 FT. AND TERMINATED AT 58.0 FT. 40.00 LOGGED: MITCHELL/ELSNER DRILL RIG: STARR 10 CHECKED: R√ DRILLING CONTRACTOR: AQUIFER DRILLING & TEST.

**Golder Associates** 

DATE: 12-06-96

## RECORD OF BOREHOLE MW-11R

PROJECT LOCATION: CARLSTADT, NEW JERSEY

BORING START: 07-26-96

SHEET: 2 OF 2

DATUM: MSL



PROJECT NUMBER: 943-6222 BORING LOCATION: N 725551.4 E 2164273.2

	_	SOIL PROFILE						SAMPLES				
DEPTH SCALE FEET	BORING METHOD	DESCRIPTION	SOSO	GRAPHIC LOG	ELEV DEPTH	NUMBER	TYPE	BLOWS / 6 in	ĸ	нес/Атт	REMARKS	PIEZOMETER OR STANDPIPE INSTALLATION
40					-33.59 40.00				-			-
· 45											·	-
	ORING											
	TARY/C											
- 50	H.S.A./WASH ROTARY/CORING											ļ -
	H.S.A.V											
- 55								:				-
-		BORING TERMINATED AT 38.0 FT.			-51.59 58.00							
- 60		BORING TERMINATED AT 38,0 FT. BELOW GROUND SURFACE, CORING BEGAN AT 38,0 FT. AND TERMINATED AT 58,0 FT.										
												-
	ļ							,				] :
- 65			ļ									<u> </u>
70												:
	ļ	:										
75												_
′3												
								!			,	
- 80 -	BIG:	STARR 10									LOGGED: MI	TCHELL/ELSNER
DRILL	ING C	STARR 10 CONTRACTOR: AQUIFER DRILLING & TEST. T. BROWN				(	Golde	er Associa	tes		CHECKED: ADATE: 12-06:	<b>v</b>

PR	OJECT NO: 943-6222 CATION: CARLSTADT, NEW JERSEY	BORING DRILLIN	RECO METHOR IG DATE: IIG: STA	D: N	1Q/HC 8-02-9	(WA			LH	Οl	E	1	11	DATUM: COORDIN AZIMUTH	NATES N	l: 72	_			Sheet 1 of 2 REFERENCE ELEV: 6.41 E: 2164273.2 INCLINATION: -90
(FEET)	ROCK TYPE  DESCRIPTION	GRAPHIC LOG	ELEV	BR-I C-Ci CA-C	edding Proken Irved Calcite Chloriti	F F	L-Cl O-C -Free A-Fa E-Iro	onta sh suit xn	ict	G-G I-Irre J-Jo K-Si	icken	i sided	DIS	LI-Limonite MN-Manganese PL-Planar QTZ-Quartz R-Rough	SM-Sm SP-Ster ST-Ster UE-Une W-Way	oped oped oven	000	CONDUCTIVITY	cm/sec	NOTES WATER LEVELS INSTRUMENTATION
		GRA	DEPTH (FT)	BUN NO.	CORE RECOVERY	RO 88		2	FRACTURES	0.	٥	CORE 60 AXIS	å	TYPE AN SURFAC DESCRIPT	Œ	GRAPHIC LOG		_		
	For lithologic description from 0.0-38.0 ft., see soil boring log 11-R.		0.00																	
5																				
10																				
15																				
20																				
25														·						
30																				
35	38.0-38.6 ft. Slightly weathered, thinnly laminated, calcareous, reddish-brown JSILTSTONE.		-31.59 -32.19																	
40	J38.6-43.6 ft. Slightly weathered, massive, calcareous, dark reddish-brown, line grained, micaceous SANDSTONE.  CONTINUED ON NEXT PAGE	1:::	38.60 -33.59 40.00	<u>'</u> _	100	#	-	ļļ.	-					ļ					+-	
	CONTINUED ON NEXT PAGE  PTH SCALE: 1 INCH=5 FEET  ILLING CONTRACTOR: AQUIFER DRILLING & TES	<u> </u>	LOG	CKE	: S. D: <b>&amp;</b> V 2-06-		HEL	Щ т	Ц.	Ш				L		olde	∐ er A	∐ As:	soc	ciates

PR	OJECT NO: 943-6222 D	ORING RILLIN	RECO METHOR IG DATE: IIG: STA	D: N 0 ARR-10	IQ/HC 8-02-9 0	(WATE	R)			DATUM: MS COORDINATE AZIMUTH: (	SN: 72			<sub>1</sub>	Sheet 2 of 2 REFERENCE ELEV: 6.41 E: 2164273.2 INCLINATION: -90
DEPTH SCALE (FEET)	DESCRIPTION	GRAPHIC LOG	ELEV DEPTH (FT)	BR-E C-Cu CA-C	CORE PACONERY CONTROL PROVIDE CONCERY CONCERY CONCERY CONCERY CONCERY CONCERY CONCERY CONCERY CONCERN	F-Fre	SHOTONES ACTURES ON SHOOT SHOT SH	FR-Fractur G-Ground I-Irregular I-Joint K-Sickensi	N P C ded F	AN-Manganese SP- PL-Planar ST- OTZ-Quartz UE	Stepped -Uneven Wavy A	HYDRAULIC	CONDUCTIVITY	cm/sec	NOTES WATER LEVELS INSTRUMENTATION
- 40	CONTINUED FROM PREVIOUS PAGE 38.6-43.6 ft. Slightly weathered, massive, calcareous, dark reddish-brown, fine grained, micaceous SANDSTONE.		-33.59 40.00												
· 45	43.6-58.0 ft. Thinnly laminated, calcareous, reddish-brown, slightly micaceous SILTSTONE. (43.6-44.4 ft. Moderately weathered; 44.4-48.0 ft. Fresh to faintly weathered; 48.0-56.0 ft. Slightly weathered; 56.0-58.0 ft. Moderately to highly weathered with vugs notably at 56.0-56.3 ft., 56.5 ft., and 57.4-57.8 ft.)		43.60	1	100										
- 50	, ,			2	100										
- 55			-51,59	3	100										
60	BORING TERMINATED AT 38.0 FT. BELOW GROUND SURFACE. CORING BEGAN AT 38.0 FT. AND TERMINATED AT 58.0 FT.		58.00												·
• 65															
70										•					
75			:												
- 60															

DRILL RIG: MOBILE B-59R

DRILLER: T, BROWN

DRILLING CONTRACTOR: AQUIFER DRILLING & TEST.

#### RECORD OF BOREHOLE MW-14R

PROJECT LOCATION: CARLSTADT, NEW JERSEY BORING

PROJECT NUMBER: 943-6222 BORING LOCATION: N 725763.5 E 2164802.3

BORING START: 07-17-96

SHEET: 1 OF 2

DATUM: MSL



SOIL PROFILE SAMPLES BORING METHOD DEPTH SCAL FEET PIEZOMETER OR STANDPIPE REMARKS ELEV GRAPHIC DESCRIPTION BLOWS / N INSTALLATION DEPTH 2.37 0.00 0 0.0-1.0 ft. ASPHALT with crushed stone **HEAD SPACE READINGS** as subbase 1.0-5.0 ft. Hard, dark gray CLAYEY SILT and SILTY CLAY, some fine to coarse sand, little fine to coarse gravel. (Pieces of rock material up to 1" in diameter). SS 12,25,15,9 40 81/241 1-3 ft. 0.0 ppm S-2 SS 12,25,10,9 35 41/24 3-5 ft. 0.0 ppm 5.0-7,0 ft. Firm, dark gray, organic, SILTY CLAY, trace fine sand with vegetative matter. (PEAT) 15'/24' S-3 SS 2.4.3.4 7 5-7 ft. 0.0 ppm 7.00 7.0-8.5 ft. Stiff, dark gray to black, organic PEAT, very fibrous with some clay and layers of dark gray, fine sand. 24"/24" 7-9 ft. 5.0 ppm S-4 SS 4,5,4,10 8.5-13.0 ft. Stiff to very stiff, bedded, brownish-gray SILTY CLAY grading to clay, grading to fine sand to silt to clay. Each couplet several mm thick with fine sand layers < 1/2 mm thick. Coloring 241/241 9-11 ft. 54.0 ppm SS 9,9,12,13 21 10 S-5 CL varigated, consisting of gray and yellowish-brown. 10'/24' 11-13 ft. 25.0 ppm SS 11 S-6 7,7,4,4 10.63 13.00 13.0-24.3 ft. Firm to soft, gray to pinkish-gray, massive CLAY, trace fine sand in <1/2 mm thick layer. 13-15 ft. 0.0 ppm S-7 SS 3,3,2,2 15 15'/24' 15-17 ft. 0.0 ppm 1,1,1,1 ROTARY/CORING 2,2,1,2 24'/24' 17-19 ft. 0.0 ppm СН SS 2 24"/24" 19-21 ft. 0.0 ppm 1,1,1,1 S-1 SS 2 24"/24" 21-23 ft. 0.0 ppm 2,1,1,1 SS 2,2,2,1 24'/24' 23-25 ft. 0.0 ppm 24,3-29.0 ft. Soft to firm, reddish-brown SILTY CLAY, little to some fine to coarse sand, trace fine gravel. 25 S-13 SS 1,1,2,1 3 121/241 25-27 ft. 0.0 ppm CL 151/241 S-14 SS 3,3,3,5 6 27-29 ft, 0.0 ppm -26.63 29.00 29.0-33.0 ft. Firm to very stiff, reddish-brown CLAYEY SILT, some to and fine to coarse sand, little fine gravel. 9'/24' 30 SS 7,8,17,37 25 29-31 ft. 0.0 ppm 74 61/241 31-33 ft. 0.0 ppm S-16 SS 20,30,44,46 33.0-34.5 ft. Very dense, reddish-brown, medium to coarse SAND, some silt, trace 33.00 SS >127 121/171 22,27,100/5 S-17 33-34.5 ft. 0.0 ppm fine to coarse gravel. 34.5-39.0 ft. Hard, reddish-brown SILTY CLAY, trace to little fine to coarse sand, 35 trace fine to coarse gravel. NR 35-37 ft. N/A SS 100/5 > 100 S-18 CL 48 31/241 29.8.40.68 37-39 ft. 0.0 ppm S-19 SS 39.0-49.0 ft. Hard, reddish-brown CLAYEY SILT, some fine to coarse sand, little -36.63 39.00 ML S-20 17,92,37,39 129 15'/24' 39-41 ft. 0.0 ppm to some fine to coarse gravel. -37.63 40.00

**Golder Associates** 

CHECKED: ₽V

DATE: 12-02-96

LOGGED: MITCHELL/ELSNER

## **RECORD OF BOREHOLE MW-14R**

SHEET: 2 OF 2

PROJECT LOCATION: CARLSTADT, NEW JERSEY

DATUM: MSL

BORING START: 07-17-96 BORING LOCATION: N 725763.5 E 2164802.3 PROJECT NUMBER: 943-6222

	_			_								
FEET	BORING METHOD	SOIL PROFILE  DESCRIPTION	SOSN	GRAPHIC LOG	ELEV	NUMBER	TYPE	SAMPLES  BLOWS / 6 In	N	REC/ATT	REMARKS	PIEZOMETER OR STANDPIPE INSTALLATION
40	$\overline{}$	39.0-49.0 ft. Hard, reddish-brown CLAYEY SILT, some fine to coarse sand, little to some fine to coarse gravel.			-37.63 40.00	S-21	ss	17,92,37,39	129	15*/24*	39-41 ft. 0.0 ppm	
						S-22	SS	42,69,100,100/5	169	17"/23"	41-43 ft. 0.0 ppm 43-45 ft. 0.0 ppm	
45			ML			S-23	SS	110,100/4	>100	8*/10*	45-45.8 ft. 0.0 ppm	
					<u>-46.63</u> 49.00	S-24	SS	100,100/3	>100	9*/9*	47-47.8 ft. 0.0 ppm	
50		49.0-54.0 ft. Hard, reddish-brown CLAYEY SILT with siltstone fragments grading to a reddish-brown, highly weathered, thinnly bedded siltstone interlayered with silty clay.			49.00	S-25 S-26	SS	200/3	>200		49-49.3 ft. 0.0 ppm 51-51.3 ft. 0.0 ppm	
		. ,	ML		-51.63							
55	Y/CORING	BORING TERMINATED AT 54.0 FT. BELOW GROUND SURFACE. CORING BEGAN AT 54.0 FT. AND TERMINATED AT 74.0 FT. BELOW GROUND SURFACE.			54.00							
	H.S.A./AIR ROTARY/CORING											
60	H.S.A											
65												
70												
									]			
75												
										,		
80 DRILL	gic.	MOBILE 8-59R									LOGGED: M	TICHELL/ELSNER
DRILL	ING (	: MOBILE B-59H CONTRACTOR: AQUIFER DRILLING & TEST. T. BROWN	٠.	•		(	Gold	er Associa	tes		CHECKED: PV DATE: 12-02-	'

PF	IOJECT: CARLSTADT/FAC. COORD./NJ IOJECT NO: 943-6222 CATION: CARLSTADT, NEW JERSEY	BORING	RECO METHOR IG DATE: RIG: MOR	D: 0	7-19-9		DR	IL	LH	Ol	E		M۱	W-14R DATUM: COORDI AZIMUTI	NATES N	l; 72	5763	.5		Sheet 1 of 2 REFERENCE ELEV: E: 2184802.3 INCLINATION: -80
DEPTH SCALE (FEET)	ROCK TYPE  DESCRIPTION	GRAPHIC LOG	ELEV DEPTH (FT)	BR-B C-Co CA-C CH-C	Broken Lived Calcite Chloriti	í í		ont sh ault on	4 FRACTURES 25 C	G-G J-Jc G-S	licker	ď	d Dis	LI-Limonite MN-Manganese PL-Planar QTZ-Quartz R-Rough CONTINUITY TYPE A SURFA DESCRIP	ST-Step UE-Une W-Wav DATA ND CE	ped ped ven	CHUBARTH	CONDUCTIVITY	cm/sec	NOTES WATER LEVELS INSTRUMENTATION
- 0	For lithologic description from 0.0-54.2 ft., see soil boring log MW-14R.						42	2	4			3	<u> </u>							
<b>-</b> 5																				
- 15																				
20																				-
- 25																				
- 30 - 35																				
- 40	CONTINUED ON NEXT PAGE																-			
DF	PTH SCALE: 1 INCH = 5 FEET ILLING CONTRACTOR: AQUIFER DRILLING & TE	<b>1</b>	CHE	CKE	: MI D: AV	'	ELL/	ELS	NÉF	1		<u>.</u>	٠.	(		olde	er /	\ss	<u>l</u>	ciates

PR	OJECT: CARLSTADT/FAC. COORD./NJ OJECT NO: 943-6222 CATION: CARLSTADT, NEW JERSEY	BORING	RECC METHOO G DATE: IG: MOS	D: 0'	7-19-8		ILLH	10	LE	N	CC	ATUM:	ATES N	72	5763.	5		Sheet 2 of 2 REFERENCE ELEV: E: 2164802.3 INCLINATION: -90
DEPTH SCALE (FEET)	ROCK TYPE  - DESCRIPTION	GRAPHIC LOG	ELEV DEPTH (FT)	BR-E C-Cu CA-C CH-C	CORE COVERY Security	F-Fre FA-Fa	contact sh autt on	ER FOOT SY CHIES	- 1	d r sided	LI-Limoni MN-Many PL-Plana QTZ-Qua R-Rough	ganese r vtz	D E	bed	HYDRAULIC	CONDUCTIVITY CM/Sec	225/112	NOTES WATER LEVELS INSTRUMENTATION
- 45 - 45	CONTINUED FROM PREVIOUS PAGE For lithologic description from 0.0-54.2 ft., see soil boring log MW-14R.																	
- 55 - 60	54.2-57.2 ft. Fresh, thinly laminated, calcareous, reddish-brown SILTSTONE.  57.2-58.2 ft. Slightly weathered, thinly laminated, calcareous, reddish-brown SILTSTONE. (Also from 59.0-59.8 ft.)  58.2-59.8 ft. Moderately weathered, thinly laminated, calcareous, reddish-brown SILTSTONE with pitting. (Also from 60.9-64.2 ft.)  59.8-60.4 ft. Moderately weathered, thinly laminated, calcareous, reddish-brown, fine grained SANDSTONE.  60.4-64.2 ft. Slightly weathered, thinly laminated, calcareous, red SILTSTONE with vugs.  64.2-74.2 ft. Fresh, thinly laminated, calcareous, slightly micaceous, nearly horizontal bedded, brick red SILTSTONE with greenish-gray reduction spotting. Dissolution vugs up to 1" dia. 64.8-65.2 ft., 69.8-70.3 ft., 73.2-74.2 ft.		54.20 57.20 58.20 59.80 60.40	2	100													
- 75 - 80	CORING TERMINATED AT 74.2 FT. BELOW GROUND SURFACE.  PTH SCALE: 1 INCH = 5 FEET		74.20	4	100	TCHELL	(5)											iates

PROJECT NUMBER: 943-6222

#### RECORD OF BOREHOLE MW-15D

BORING LOCATION: N 725666.5 E 2163930.3

SHEET: 1 OF 2

PROJECT LOCATION: CARLSTADT, NEW JERSEY

BORING START: 08-12-96

DATUM: MSL



SOIL PROFILE SAMPLES BORING METHOD DEPTH SCAL FEET PIEZOMETER REMARKS **ELEV** STANDPIPE GRAPHIC DESCRIPTION BLOWS / N INSTALLATION DEPTH 9.68 0.00 0.50 0.0-0.5 ft. Gray, fine to medium SAND, some silt and roots. **HEAD SPACE READINGS** SS 11,9,7,7 16 241/241 0-2 ft. 0.0 ppm 0.5-5.7 ft. Dense, grayish-tan, fine to medium SAND, little fine gravel, trace silt. 2.0-4.0 ft. 1 mm thick orangebrown sand layers. 5.5 ft. 5 mm thick, dark brown, medium sand layer. SS 21,20,19,17 39 24"/24" 2-4 ft. 0.0 ppm SW SS 15,8,25,75 33 24"/24" 4-6 ft. 20.0 ppm 15.7-6.0 ft. Dense, dark gray, silty, medium to fine SAND, little fine gravel, some root fragments.
6.0-10.0 ft. Very dense, grayish-blue, reddish-brown, dark gray FILL consisting of sand, silt, clay and fine gravel with 6.00 8.25,43,56 241/24 6-8 ft. 20.0 ppm SS 68 4'/6' 8-8.3 ft. 0.0 ppm 100/4 pieces of decomposed wood and asbestos -0.32 10.00 10 10.0-13.0 ft. Firm, dark brown to black, sandy and silty, organic PEAT. S-6 SS 3,2,3,5 5 2424" 10-12 ft. 0.0 ppm РΤ -3.32 13.00 S-7 SS 3,5,9,16 14 24'/24" 12-14 ft. 0.0 ppm 13.0-14.0 ft. Stiff, grayish-green CLAYEY SILT, trace fine sand, trace fine gravel with reddish-brown, 1 mm thick layers, some wood fragments. ML CL SS 1,2,4,8 24/24 14-16 ft. 0.0 ppm S-8 15 14.0-16.0 ft. Firm, bluish-gray SILTY -CLAY with orange staining.

16.0-21.0 ft. Very stiff to stiff, bedded, orange-tan-brown SILTY CLAY grading to fine sand to silt to clay. Each couplet several mm thick with fine sand layers < 1/2 mm thick. 13,11,12,15 23 24"/24" 16-18 ft. 0.0 ppm CL S-10 SS 7,6,6,7 12 24"/24" 18-20 ft. 0.0 ppm ő -11.32 21.00 21.0-42.0 ft. Very soft, massive CLAY with alternating layers of pinkish-gray and gray, trace fine sand in <1/2 mm thick layers. H.S.A./WASH S-11 SS 5,6,6,5 12 241/241 20-22 ft. 0.0 ppm SS 1,1,1,1 2 24'/24' 22-24 ft. 0.0 ppm 25 SS WOH,2,1,1 3 241/241 24-26 ft. 0.0 ppm SS 1,1,1,1 2 24"/24" 26-28 ft. 0.0 ppm S-15 SS 1,WOH,1,WOH 1 24'/24' 28-30 ft. 0.0 ppm 30 СH S-16 SS 1,1,1,1 2 24"/24" 30-32 ft. 0.0 ppm S-17 SS WOH,1,1,WOH 2 24'/24' 32-34 ft. 0.0 ppm WOH.1.WOH 24"/24" 35 S-18 SS 34-36 ft. 0.0 ppm 2 24'/24' S-19 SS 1.1.1.1 36-38 ft, 0.0 ppm 38-40 ft. 0.0 ppm S-20 SS 1,1,1,2 2 241/241 -30.32 40.00 LOGGED: M. ELSNER DRILL RIG: MOBILE B-59 CHECKED: &V DRILLING CONTRACTOR: AQUIFER DRILLING & TEST. DRILLER: T. BROWN **Golder Associates** DATE: 12-02-96

**RECORD OF BOREHOLE MW-15D** 

BORING START: 08-12-96

SHEET: 2 OF 2

DATUM: MSL



PROJECT LOCATION: CARLSTADT, NEW JERSEY
PROJECT NUMBER: 943-6222

BORING LOCATION: N 725666.5 E 2163930.3

		SOIL PROFILE						SAMPLES			·	<u> </u>
DEPTH SCALE FEET	BORING METHOD	DESCRIPTION	SOSO	GRAPHIC LOG	ELEV DEPTH	NUMBER	TYPE	BLOWS / 6 In	N	REC/ATT	REMARKS	PIEZOMETER OR STANDPIPE INSTALLATION
- 40	<u> </u>	21.0-42.0 ft. Very soft, massive CLAY with alternating layers of pinkish-gray and gray, trace fine sand in <1/2 mm	СН		-30.32 40.00	S-21	SS	1,1,2,2	3	24'/24'	40-42 ft. 0.0 ppm	-
		thick layers. 42.0-47.0 ft. Soft, reddish-gray CLAY, some fine to coarse sand, trace medium to coarse sand grading to a silty clay matrix.			-32.32 42.00	S-22	SS	1,2,2,2	4	24'/24'	42-44 ft. 0.0 ppm	
<b>-</b> 45		Iliquia.	CL			S-23	SS	2,1,2,3	3	24'/24'	44-46 ft. 0.0 ppm	_
	Y/CORING	47.0-53.5 ft. Hard, reddish-brown CLAYEY SILT grading to a brick red silly clay, some fine to coarse sand, some fine to			-37.32 47.00	S-24	SS	5,4,13,31	17	24'/24'	46-48 ft. 0.0 ppm	
- 50	H.S.A./WASH ROTARY/CORING	coarse gravel.	ML			S-25	SS	65,100/4	> 100	10*/10*	48-48.8 ft. 0.0 ppm	-
· •	H.S.A./W#					S-26 S-27	SS	25,33,36,43	69 >100	24'/24'	50-52 ft. 0.0 ppm 52-52.8 ft. 0.0 ppm	
55		53.5-58.5 ft. Brick red SILTSTONE and fine-grained SANDSTONE.			-43.82 53.50							
8												
- 60		BORING TERMINATED AT 58.5 FT. BELOW GROUND SURFACE. CORING BEGAN AT 58.5 FT. AND TERMINATED AT 63.5 FT. TO CONFIRM BEDROCK			-48.82 58.50							- -
65												-
- 70												
75												-
											·	
DRI	ШNG	: MOBILE B-59 CONTRACTOR: AQUIFER DRILLING & TEST.									Logged: M. Checked: & V	,
DRI	LLER:	T. BROWN					iold	er Associa	tes		DATE: 12-02-	98

## **RECORD OF BOREHOLE MW-16D**

PROJECT LOCATION: CARLSTADT, NEW JERSEY

BORING START: 07-22-96

SHEET: 1 OF 2

PROJECT NUMBER: 943-6222

DRILLER: T. BROWN

BORING LOCATION: N 725909.8 E 2164281.6

DATUM: MSL

	0	SOIL PROFILE						SAMPLES				
FEET	BORING METHOD	DESCRIPTION	sosn	GRAPHIC LOG	ELEV	NUMBER	TYPE	BLOWS / 6 in	z	REC/ATT	REMARKS	PIEZOMETEF OR STANDPIPE INSTALLATIO
0 -		0.0-4.0 ft. Compact to very dense, dark brown to reddish-brown, fine SAND, some silt, trace coarse gravel.			7.25	S-1	ss	11,12,11,13	23	2'/24'	HEAD SPACE READINGS 0-2 ft. 0.0 ppm	
					3.25	S-2	SS	44,31,31,23	62	6"/24"	2-4 ft. 0.0 ppm	
5		4.0-12.0 ft. Hard, brownish-gray to reddish-gray CLAYEY SILT, some to and fine to coarse sand, trace to little fine to coarse gravel.			4.00	S-3	ss	19,23,23,24	46	13'/24'	4-6 ft. 0.0 ppm	
			мн∙ѕм			S-4	SS	27,23,43,43 60,32,27,23	66 59	12°/24°	6-8 ft. 0.0 ppm 8-10 ft. 0.0 ppm	
٥						3-3	33	60,32,27,23		0724	6-10 II. 0.0 ppiii	
		12.0-16.0 ft. Stiff, bedded, brownish-	ļ		-4.75 12.00	S-6	SS	12,10,10,12	20	3'/24'	10-12 ft. 0.0 ppm	
		gray CLAY grading to silt to clay. Each couplet several mm thick. Coloring varigated, consisting of gray and yellowish-brown.	CL			S-7	SS	20,17,13,14	30	NR	12-14 ft. N/A	
5		16.0-20.0 ft. Stiff to firm, massive CLAY	_		-8.75 16.00	S-8	ss	4,5,8,8	13	5/24*	14-16 ft. 0.0 ppm	
	DRING	with alternating layers of pinklsh-gray and gray, trace fine sand in < 1/2 mm thick layers.	СН			S-9	SS	6,6,6,4	12	4*/24*	16-18 ft. 0.0 ppm	
0	ROTARY/CORING	20.0-23.8 ft. Firm to soft, reddish-gray	-		-12.75 20.00	S-10	SS	4,3,3,3	6	12*/24*	18-20 ft. 0.0 ppm	
	A./AIR	SILTY CLAY.	СН			S-11	SS	3,2,2,3	4	24"/24"	20-22 ft. 0.0 ppm	
	H.S.	23.8-33.5 ft. Firm, reddish-brown SILTY			-16.55 23.80	S-12	SS	2,2,2,3	4	24*/24*	22-24 ft. 0.0 ppm	
5		CLAY, some fine to coarse sand, trace fine to coarse gravel.				S-13	SS	3,2,7,3	9	24"/24"	24-26 ft. 0.0 ppm	
						S-14	SS	8,2,4,3	6	24"/24"	26-28 ft. 0.0 ppm	
٥			CL			S-15	SS	4,5,5,16	10	24"/24"	28-30 ft. 0.0 ppm	
			i			S-16	SS	6,4,5,6	9	24"/24"	30-32 ft. 0.0 ppm	
5		33.5-36.0 ft. Hard, reddish-brown CLAYEY SILT and to some fine to coarse sand, trace to little fine to coarse gravel.	CL		-26.25 33.50	S-17 S-18	SS	11,23,23,40 69,200/6	46 >200	12"/12"	32-34 ft. N/A 34-35 ft. 0.0 ppm	
		36.0-38.0 ft. Hard, reddish-brown SILTY CLAY, some fine to coarse sand, little fine to coarse gravel.	CL		-28.75 36.00	S-19	SS	41,100/5	>100	11"/12"	36-36.9 ft. 0.0 ppm	
۰		38,0-40,0 ft. Hard, reddish-brown SILTSTONE fragments with gray reduction zones.			-30.75 38.00 -32.75 40.00	S-20	_ss_	100/2	>100	212	38-38.2 ft. 0.0 ppm	

**Golder Associates** 

DATE: 01-20-97

DRILLER: T. BROWN

## **RECORD OF BOREHOLE MW-16D**

SHEET: 2 OF

PROJECT LOCATION: CARLSTADT, NEW JERSEY

BORING START: 07-22-96

DATUM: MSL

BORING LOCATION: N 725909.8 E 2164281.6 PROJECT NUMBER: 943-6222 SOIL PROFILE SAMPLES DEPTH SCALE FEET PIEZOMETER OR STANDPIPE INSTALLATION GRAPHIC LOG ELEV REMARKS BLOWS / 6 in DESCRIPTION DEPTH 40.0-45.0 ft. Brick red, thinnly bedded SILTSTONE. 1SA/AIR ROT./CORING BORING TERMINATED AND CORING BEGAN AT 40.0 FT. BELOW GROUND SURFACE. 55 60 65 75 DRILL RIG: MOBILE B-59 LOGGED: MITCHELL/ELSNER CHECKED: PV DRILLING CONTRACTOR: AQUIFER DRILLING & TEST.

**Golder Associates** 

DATE: 01-20-97

Form A

NAME OF PERMITTEE: 216 Actorson Plank Ad. Comp
NAME OF FACILITY: 216 Patron Planked Sitc
LOCATION: 216 Patrison Plunked Beigency Refunctod Burd
NJDEPE PERMIT NO: 53423 OR ECRA CASE NO.:
CERTIFICATION
WELL PERMIT NUMBER(as assigned by NJDEPE) 26.44015
OWNER'S WELL NUMBER(as shown on plan) mw8R
WELL COMPLETION DATE 8-2896
DISTANCE FROM TOP OF CASING TO GROUND SURFACE O
DEPTH TO TOP OF SCREEN FROM TOP OF CASING83'
SCREEN LENGTH IN FEET 10'
SCREEN OR SLOT SIZE00
CODERN OR STOT MATERIAL ROY STOWNESS STOW
CASING MATERIAL(pvc, steel or other specify) 35040 Steel - 79' 6"  CASING DIAMETER 10 Steel 2
CASING DIAMETER 10'Street 2'Stanless Street
STATIC WATER LEVEL S.O
YIELD GPM/
DEVELOPMENT TECHNIQUE SUPPLY
LENGTH OF TIME WELL IS DEVELOPED SUS PUMPED OR BAILED
LENGTH OF TIME WELL IS DEVELOPED & MS PUMPED OR BAILED LITHOLOGIC LOG 6-4"/FPH
40,70° rectaeuntill
AUTHENTICATION 16.7.5' prat 70'-129' Siteston C
I certify under penalty of law that I have personally examined and am
familiar with the information submitted in this document and all
attachments and that, based on my inquiry of those individuals immediately
responsible for obtaining the information, I believe the submitted
information is true, accurate and complete. I am aware that there are
significant penalties for submitting false information, including the
possibility of fine and imprisonment.
Thomas Brown Mun Dru
NAME SIGNATURE
1311
CERTIFICATION OR LICENSE NO. seal
CERTIFICATION BY EXECUTIVE OFFICER OR DULY AUTHORIZED REP
Dennise Moore Slugare
NAME SIGNATURE
General Muncieger 12-13-96
TITLE DATE

NAME OF PERMITTEE: 216 Paterson Plank Rd-Coup
NAME OF FACILITY: 216 Poiterson Plank Rd Sitc
LOCATION: 216 Paterson Plank Rd. Bergen Cty Ruther Food Boro
NJDEPE PERMIT NO:5362 OR ECRA CASE NO.:
CERTIFICATION
WELL PERMIT NUMBER(as assigned by NJDEPE) 26-44013
OWNER'S WELL NUMBER(as shown on plan)
WELL COMPLETION DATE
DISTANCE FROM TOP OF CASING TO GROUND SURFACE
DEPTH TO TOP OF SCREEN FROM TOP OF CASING 3?
SCREEN LENGTH IN FEET 5
SCREEN OR SLOT SIZE .C/O
SCREEN OR SIDT MATERIAL 304.Stunics 55td
CASING MATERIAL(pvc, steel or other specify) 30455  CASING DIAMETER
CASING DIAMETER ("Steel"
STATIC WATER LEVEL 45
YIELD GPM/
DEVELOPMENT TECHNIQUE Subpump
LENGTH OF TIME WELL IS DEVELOPED & he PUMPED OR BAILED
TITHOTOCIC TOC O'C POESON IN TOPY YELD SITT
10',12' peat 34',421 lee to till
AUTHENTICATION
I certify under penalty of law that I have personally examined and am
familiar with the information submitted in this document and all
attachments and that, based on my inquiry of those individuals immediately
responsible for obtaining the information, I believe the submitted
information is true, accurate and complete. I am aware that there are
significant penalties for submitting false information, including the
possibility of fine and imprisonment.
Thomas Brown Mills
NAME SIGNATURE LE
1311
CERTIFICATION OR LICENSE NO. seal
CERTIFICATION BY EXECUTIVE OFFICER OF DULY AUTHORIZED REP
Dennis C. Moore Illus Cypal
NAME SIGNATURE
General Manager 12-13-94
TITLE DATE

NAME OF PERMITTEE: 2/6+afcrson Hank Rd. Corp
NAME OF FACILITY: 214 Paterson Plank R. Sitt
LOCATION: 216 Paterson Plankld, Bengenety, Rutinenforder
NJDEPE PERMIT NO: 53622 OR ECRA CASE NO.:
CERTIFICATION
WELL PERMIT NUMBER(as assigned by NJDEPE) 26.44014
OWNER'S WELL NUMBER(as shown on plan) MWIOR
WELL COMPLETION DATE82896
DISTANCE FROM TOP OF CASING TO GROUND SURFACE $Q$
DEPTH TO TOP OF SCREEN FROM TOP OF CASING 55.5
SCREEN LENGTH IN FEET
SCREEN OR SLOT SIZE .OLO
SCREEN OR SLOT MATERIAL 304 Stewniess Steel
CASING MATERIAL(pvc, steel or other specify)
STATIC WATER LEVEL 3.5
YIELD GPM /
DEVELOPMENT TECHNIQUE Schoune
LENGTH OF TIME WELL IS DEVELOPED 845. PUMPED OR BAILED
LITHOLOGIC LOG 0-6" topsoil 121-191 queyersilt
1.019=7
AUTHENTICATION  1012. Peat  34-445' Red by till 44.5'-655 Silt stone
I certify under penalty of law that I have personally examined and am
familiar with the information submitted in this document and all
attachments and that, based on my inquiry of those individuals immediately
responsible for obtaining the information, I believe the submitted
information is true, accurate and complete. I am aware that there are
significant penalties for submitting false information, including the
possibility of fine and imprisonment.
Thomas Brown Suntine
NAME SIGNATURE
CERTIFICATION OR LICENSE NO. seal
CERTIFICATION BY EXECUTIVE OFFICER OR DULY AUTHORIZED REP
Dennes Comocre June Worl
NAME SIGNATURE
Gencial manager 1213-96
TITLE DATE
ITTEL

NAME OF PERMITTEE: 216 PC	cite ison AUNK Rd. Corp
NAME OF FACILITY: 216 PC	itison Agni alsite
	1th Bengency Ruthenfordsons
NJDEPE PERMIT NO: 53425 OR E	CRA CASE NO.:
<u>CERTIFICATION</u>	
WELL PERMIT NUMBER(as assigned	
OWNER'S WELL NUMBER(as show WELL COMPLETION DATE	on plan) <u>MWIIR</u>
WELL COMPLETION DATE	8-2896
DISTANCE FROM TOP OF CASING TOP TOP OF SCREEN FROM	TO GROUND SURFACE
DEPTH TO TOP OF SCREEN FROM	TOP OF CASING48'
SCREEN LENGTH IN FEET	10' open roctholc
SCREEN OR SLOT SIZE	
SCREEN OR SLOT MATERIAL_	
CASING MATERIAL(pvc, steel or o	ther specify) Sch403Fect 21.5-12+
SCREEN OR SLOT MATERIAL_ CASING MATERIAL(pvc, steel or o CASING DIAMETER	Stel 12" 55-4"
STATIC WATER LEVEL	4.5
YIELD GPM	/
DEVELOPMENT TECHNIQUE	Sibpinp
LENGTH OF TIME WELL IS DEVELO	PED 8h PUMPED OR BAILED
LITHOLOGIC LOG OG FOR	16'-28' G-ca(ceg
81-165 DEC	4 25'38' Radbytiu
DEVELOPMENT TECHNIQUE  LENGTH OF TIME WELL IS DEVELOR  LITHOLOGIC LOG  8'-10' PCC  AUTHENTICATION	grysilt 38'-58' silts tone
I certify under penalty of law that I have	personally examined and am
familiar with the information submitted	in this document and all
attachments and that, based on my inqu	
responsible for obtaining the information	n, I believe the submitted
information is true, accurate and comple	
significant penalties for submitting false	information, including the
possibility of fine and imprisonment.	
<i>f</i> m	
TromasBrown	The cit
1 11 11 12	SIGNATURE
	-
CERTIFICATION OR LICENSE NO.	seal
CERTIFICATION BY EXECUTIVE OFFICE	
Dennisc. Moorc	_ Llus Coffre
NAME	SIGNATURE
6 cneval manager	12-13-96
TITLE	DATE

NAME OF PERMITTEE: 216 PORTES A PROPERTY OF A
NAME OF FACILITY: 216 Paterson Aconked Sitc
LOCATION: 216 Paterson Planked. Bergin Cry Luther Bon
NJDEPE PERMIT NO: 53623 OR ECRA CASE NO.:
CERTIFICATION
WELL PERMIT NUMBER(as assigned by NJDEPE) 26-44016
WELL PERMIT NUMBER(as assigned by NJDEPE) 26-94016  OWNER'S WELL NUMBER(as shown on plan) MW14D  WELL COMPLETION DATE 8-28-96
DISTANCE FROM TOP OF CASING TO GROUND SURFACE O
DEPTH TO TOP OF SCREEN FROM TOP OF CASING 30'
SCREEN LENGTH IN FEET /0'
SCREEN OR SLOT SIZE
SCREEN OR SIOT MATERIAL 304. Stanless Stall
CASING MATERIAL(pvc, steel or other specify)  CASING DIAMETER  STATIC WATER LEVEL
CASING DIAMETER
STATIC WATER LEVEL
YIELD GPM/
DEVELOPMENT TECHNIQUE SUSPUMP
LENGTH OF TIME WELL IS DEVELOPED 845 PUMPED OR BAILED
LITHOLOGIC LOGsuppump
LENGTH OF TIME WELL IS DEVELOPED She QUMPED OR BAILED  LITHOLOGIC LOG Suppose 13.28 9.77 (244)  AUTHENTICATION 7.75. Pear 13.28 9.77 (244)  I certify under penalty of law that I have personally examined and am
AUTHENTICATION Constitution 28'41' redsountil
familiar with the information submitted in this document and all
attachments and that, based on my inquiry of those individuals immediately
responsible for obtaining the information, I believe the submitted
information is true, accurate and complete. I am aware that there are
significant penalties for submitting false information, including the
possibility of fine and imprisonment.
54 D. S460 1 7 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
Thomas Bours Mew Du
NAME SIGNATURE
131(
CERTIFICATION OR LICENSE NO. seal
CERTIFICATION BY EXECUTIVE OFFICER OR DULY AUTHORIZED REP
NAME General Manager SIGNATURE 12-13-94
TITLE DATE
1111 E

NAME OF PERMITTEE: 216 Patersovi Hane Ro. Corps
NAME OF FACILITY: 216 Perterson Aunk Rd: 5.12
LOCATION: 216 Paterson Plank Rd Bryger Chy.
NJDEPE PERMIT NO.53623 OR ECRA CASE NO.:
CERTIFICATION
WELL PERMIT NUMBER(as assigned by NJDEPE) 24-44017
OWNER'S WELL NUMBER(as shown on plan) mwyk
WELL COMPLETION DATE 8-28-96
DISTANCE FROM TOP OF CASING TO GROUND SURFACE O
DEPTH TO TOP OF SCREEN FROM TOP OF CASING 645'
SCREEN LENGTH IN FEET 10' Open rock hold
SCREEN OR SLOT SIZE
SCREEN OR SLOT MATERIAL  CASING MATERIAL(pvc, steel or other specify)  9'50405tc1645'  5'00
CASING DIAMETER 54 +8" Steel
STATIC WATER LEVEL
YIELD GPM
DEVELOPMENT TECHNIQUE SUPUM
LENGTH OF TIME WELL IS DEVELOPED & NOS. PUMPED OR BAILED
LITHOLOGIC LOG O-4" Asphait 7.5" 13 bours "H
AUTHENTICATION 6'-75' prot 25'-44' led bown kill
AUTHENTICATION 6'-7.5' prot 28.44' led bio win kill
I certify under penalty of law that I have personally examined and am
familiar with the information submitted in this document and all
attachments and that, based on my inquiry of those individuals immediately
responsible for obtaining the information, I believe the submitted
information is true, accurate and complete. I am aware that there are
significant penalties for submitting false information, including the
possibility of fine and imprisonment.
Tromas Brown Mulle
NAME SIGNATURE 9º
CERTIFICATION OR LICENSE NO. seal
CERTIFICATION BY EXECUTIVE OFFICER OR DULY AUTHORIZED REP
NAME SIGNATURE 1-2097
TITLE DATE

NAME OF PERMITTEE: 216 Paterson Aank Rd. Coop
NAME OF FACILITY: 216 Paterson Plank Rd site
LOCATION: 216 Paterson Plank Rd. Bergenery Rumarowskie
NJDEPE PERMIT NO:53424 OR ECRA CASE NO.:
CERTIFICATION
WELL PERMIT NUMBER(as assigned by NJDEPE) 26-94012
OWNER'S WELL NUMBER(as shown on plan) MUISO
WELL COMPLETION DATE 82896
DISTANCE FROM TOP OF CASING TO GROUND SURFACE O
DEPTH TO TOP OF SCREEN FROM TOP OF CASING 50'
SCREEN LENGTH IN FEFT
SCREEN OR SLOT SIZE  SCREEN OR SLOT MATERIAL 304 Stairless Stace  CASING MATERIAL(pvc, steel or other specify) 304 SS  CASING DIAMETER  STATIC WATER LEVEL
SCREEN OR SLOT MATERIAL 304 Stainless steel
CASING MATERIAL(pvc, steel or other specify) 30455
CASING DIAMETER Substitution of the control of the
STATIC WATER LEVEL 5'
YIELD GPM/
DEVELOPMENT TECHNIQUE Subamp
LENGTH OF TIME WELL IS DEVELOPED 8 hrs. PUMPED OR BAILED
LITHOLOGIC LOG O-6" ROPEON 21-47 9 MLY CLOCK
LENGTH OF TIME WELL IS DEVELOPED & hrs. PUMPED OR BAILED LITHOLOGIC LOG O-6" topsoil 21'-47' quay clay  (0'-13' part  AUTHENTICATION 13' 21" brail 53.5'-58 5, its tone
I certify under penalty of law that I have personally examined and am
familiar with the information submitted in this document and all
attachments and that, based on my inquiry of those individuals immediately
responsible for obtaining the information, I believe the submitted
information is true, accurate and complete. I am aware that there are
significant penalties for submitting false information, including the
possibility of fine and imprisonment.
Thomas Brown Than
NAME SIGNATURE
CERTIFIC ATION OR LICENSE NO. 502
CERTIFICATION OR LICENSE NO. seal
CERTIFICATION BY EXECUTIVE OFFICER OR DULY AUTHORIZED REP
Dennis C. moure Illus Eyour
NAME SIGNATURE
General Manager 12-1096
TITLE DATE

NAME OF PERMITTEE: 216A	eterson Acuked Corp
NAME OF FACILITY: 216 Poit	tronflunkldstc
LOCATION: 216 PatrosonPlace	nked. Beigen Cty Rither Food Bod
NJDEPE PERMIT NO: 53625 OR 1	
CERTIFICATION	
WELL PERMIT NUMBER(as assigned	d by NJDEPE) 24-44021
OWNER'S WELL NUMBER(as show	
WELL COMPLETION DATE	8-2894
DISTANCE FROM TOP OF CASING	TO GROUND SURFACE
DEPTH TO TOP OF SCREEN FROM	TOP OF CASING 3
SCREEN LENGTH IN FEET	5'
SCREEN OR SLOT SIZE	.0(05/01
COPERI OR SIOT MATERIAL	3>いくたいのはらら 5k.4
CASING MATERIAL(pvc, steel or of	other specify) 504705tcc18"20"  9tcc1-8" 3045tcumess5tc1/ -55-4"
CASING DIAMETER	Steel = 8" - 2 - 1 - 2 - 1 - 2 - 2 - 2 - 2 - 2 - 2
STATIC WATER LEVEL	<u> </u>
YIELD GPM	7
DEVELOPMENT TECHNIQUE	Schamp
LENGTH OF TIME WELL IS DEVELO	PED Shy PLIMPED OR BAILED
LITHOLOGIC LOG OG" top	2501 11-15 grey & cf
9'-11' pc	icit 15'-25'944'0004
AUTHENTICATION	25 40 red by till
I certify under penalty of law that I have	e personally examined and am
familiar with the information submitted	l in this document and all
attachments and that, based on my inqu	iry of those individuals immediately
responsible for obtaining the information	
information is true, accurate and comple	
significant penalties for submitting false	
possibility of fine and imprisonment.	
	(2)110
Thomas Brown	melle
NAME	SIGNATURE &
43//	
CERTIFICATION OR LICENSE NO.	seal
CERTIFICATION BY EXECUTIVE OFFICE	CER OR DULY/AUTHORIZED REP
Dennisc. modre	1) HUS CAJOCIE
NAME	SIGNATURE CO
Ocneral Managa	121396
TITLE	DATE

NAME OF PERMITTEE: 2/6 Paterson Manked Corp
NAME OF FACILITY: 214 Porte-son Planked Site
LOCATION: 216 Parterson Planked Breigen Chy Retrictord Boro
NJDEPE PERMIT NO: 53423OR ECRA CASE NO.:
CERTIFICATION
WELL PERMIT NUMBER(as assigned by NJDEPE) 26-44018
OWNER'S WELL NUMBER(as shown on plan)
WELL COMPLETION DATE \ \&\sigma_2\sigma_4\\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\
DISTANCE FROM TOP OF CASING TO GROUND SURFACE 0
DEPTH TO TOP OF SCREEN FROM TOP OF CASING 45
SCREEN LENGTH IN FEET
SCREEN OR SLOT SIZE
SCREEN OR SLOT MATERIAL 304 Stewness Steet
CASING MATERIAL (pvc, steel or other specify)
CASING MATERIAL(pvc, steel or other specify)  CASING DIAMETER  9" 5 5
STATIC WATER LEVEL
YIELD GPM/
DEVELOPMENT TECHNIQUE SUPPLY
LENGTH OF TIME WELL IS DEVELOPED 8hs. PUMPED OR BAILED
LITHOLOGIC LOG 0-4" Aspiral 7.5 Moouth & (+12/scird)
4'.75' Prat 40'-54' redbountil
AUTHENTICATION
I certify under penalty of law that I have personally examined and am
familiar with the information submitted in this document and all
attachments and that, based on my inquiry of those individuals immediately
responsible for obtaining the information, I believe the submitted
information is true, accurate and complete. I am aware that there are
significant penalties for submitting false information, including the
possibility of fine and imprisonment.
Manas Brown eller
NAME SIGNATURE
_13/
CERTIFICATION OR LICENSE NO. seal
CERTIFICATION BY EXECUTIVE OFFICER OR DULY AUTHORIZED REP
NAME SIGNATORE
TITLE DATE

NAME OF PERMITTEE: 216 Paterson Plank Rd-Corp
NAME OF FACILITY: 216 Paterson Planked site
LOCATION: 216 Actuson Plankld. Buyencky Ruther Bure
NJDEPE PERMIT NO: 53,23OR ECRA CASE NO.:
CERTIFICATION
WELL PERMIT NUMBER(as assigned by NJDEPE) 26,44019
OWNER'S WELL NUMBER(as shown on plan) MULS WELL COMPLETION DATE \$2896
WELL COMPLETION DATE \$2896
DISTANCE FROM TOP OF CASING TO GROUND SURFACE O
DEPTH TO TOP OF SCREEN FROM TOP OF CASING 41.5'
SCREEN LENGTH IN FEET 5' SCREEN OR SLOT SIZE 20/0
SCREEN OR SLOT SIZE
CODERNI OD CIOT MATERIAI $200 < 500 < 100 < 500 < 100 < 500 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100 < 100$
CASING MATERIAL (pvc, steel or other specify) 201/205/205/205/205/205/205/205/205/205/205
CASING DIAMETER SCORE
STATIC WATER LEVEL5.0
YIELD GPM/
DEVELOPMENT TECHNIQUE Shown
LENGTH OF TIME WELL IS DEVELOPED SWIS PUMPED OR BAILED
LITHOLOGIC LOG WAS FILL 75 12/6/6 CAN IT FISCA
LENGTH OF TIME WELL IS DEVELOPED SAVE PUMPED OR BAILED LITHOLOGIC LOG 4 12 12 10 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9
<u>AUTHENTICATION</u>
I certify under penalty of law that I have personally examined and am
familiar with the information submitted in this document and all
attachments and that, based on my inquiry of those individuals immediately
responsible for obtaining the information, I believe the submitted
information is true, accurate and complete. I am aware that there are
significant penalties for submitting false information, including the
possibility of fine and imprisonment.
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Thomas Brown allemen
NAME SIGNATURE SIGNATURE
CERTIFICATION OR LICENSE NO. seal
CERTIFICATION BY EXECUTIVE OFFICER OR DULY AUTHORIZED REP
NAME SIGNATURE OF 12-13-94
TITLE DATE

Form B

#### **GROUND WATER MONITORING WELL CERTIFICATION - FORM B - LOCATION CERTIFICATION**

Name of Permittee: 216 Paterson Plank Road Cooperating PRP Group							
Name of Facility:	216 Paterson Plank Road Site						
Location:	216 Paterson Plank Road, Carlstadt Boro, Bergen County						
NJPDES Number:							
LAND SURVEYOR'S CERTIF	<u>ICATION</u>						
Well Permit Number (As assigned	by NJDEP's Bureau of Water	26-4	44015		<del></del>		
Allocation):					<del></del>		
This number must be permanently	affixed to the well casing.						
Datum NAD 1927		***		-	400 4111 550		
Longitude (one-tenth of a second):			West 74°04'11.57"				
Latitude (one-tenth of a second):		North	North 40°49'20.79"				
Elevation of Top of Casing (cap off) (one-hundreth of a foot):		WC =	5.35	/IC =	5.11 / GRD = 5.35	5	
Owners Well Number (As shown of	on application or plans):	MW-8R		<u> </u>			
BENCHMARK - GEOGRAPHIC POSITION -	G.P.S. NETWORK	ELEVAT	ION -				
PATE OF SURVEY -	9/23/96						

#### **AUTHENTICATION**

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PROFESSIONAL LAND SURVEYOR'S SIGNATURE

Paul J. Emilius, Jr.

PROFESSIONAL LAND SURVEYOR'S NAME
(Please print or type)

SEAL

New Jersey P.L.S. License No. 37186

PROFESSIONAL LAND SURVEYOR'S LICENSE #

The Department reserves the right in cases of violation of permit specified ground water limits or Ground Water Quality Standards C<sup>++</sup> A.C. 7:9-6.1 et seq.) to require that wells be resurveyed to an accuracy of one-hundredth of a second latitude and longitude. shall not be considered to be a major modification of the N.J.P.D.E.S. permit.

### GROUND WATER MONITORING WELL CERTIFICATION - FORM B - LOCATION CERTIFICATION

Name of Permittee:	216 Paterson Plank Road	Cooperat	ing PRP	Group				
Name of Facility:	216 Paterson Plank Road Site							
Location:	216 Paterson Plank Road	, Carlsta	dt Boro	, Berge	en County			
NJPDES Number:								
LAND SURVEYOR'S CERTIF	<u>ICATION</u>							
Well Permit Number (As assigned Allocation):	by NJDEP's Bureau of Water	26-4	4013					
This number must be permanently	affixed to the well casing.		-					
Datum NAD 1927	-							
Longitude (one-tenth of a second):		West		7	'4°04'21.21"			
Latitude (one-tenth of a second):		North		40°49'21.82"				
Elevation of Top of Casing (cap off) (one-hundreth of a foot):		WC =	7.49	/IC =	7.09 / GRD = 7.49			
Owners Well Number (As shown o	n application or plans):	MW-10D						
BENCHMARK -	G.P.S. NETWORK	ELEVAT	ION -					
<b>GEOGRAPHIC POSITION</b> -								
P^TE OF SURVEY -	9/23/96							

#### **AUTHENTICATION**

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Paul J. Emilius, Jr.
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#### **GROUND WATER MONITORING WELL CERTIFICATION - FORM B - LOCATION CERTIFICATION**

Name of Permittee:	216 Paterson Plank Roa	d Cooperat	ing PR	P Group	•		
Name of Facility:	216 Paterson Plank Road Site						
Location:	216 Paterson Plank Roa		dt Bor	o. Rero	en County	<del></del>	
NJPDES Number:	210 Taterson Trank Roa	u, variaca	uc bor	O, Derg	ch county		
1101 DEG Tramoer.			•				
LAND SURVEYOR'S CERTIF	<u>FICATION</u>						
Well Permit Number (As assigned	l by NJDEP's Bureau of Water	26-	44014				
Allocation):			-			-	
This number must be permanently Datum NAD 1927	affixed to the well casing.				-		
Longitude (one-tenth of a second):	:	West		•	74°04'21.12"		
Latitude (one-tenth of a second):		North		4	40°49'21.76"		
Elevation of Top of Casing (cap o	off) (one-hundreth of a foot):	WC =	7.48	/IC =	7.01 /GRD =	7.48	
Owners Well Number (As shown	on application or plans):	MW-10R					
BENCHMARK -	G.P.S. NETWORK	ELEVAT	ION -				
<b>GEOGRAPHIC POSITION -</b>							
<b>DATE OF SURVEY</b> -	9/23/96						
<u>. HENTICATION</u>							
I certify under penalty of law that	I have personally examined and	am familiar v	vith the i	nformatio	n submitted in thi	is document and	
all attachments and that, based or							
the submitted information is true		aware that	there are	significa	int penalties for	submitting false	
information including the possibili	ity of fine and imprisonment.						
A115							
PROFESSIONAL LAND SUR	VEYOR'S SIGNATURE						
PROPESSIONAL LAND SUK	VETORY SIGNATURE						
Paul J. Emil	ius. Jr.						
PROFESSIONAL LAND S		SE	AL				
(Please print o		32					
New Jersey P.L.S. Lie	cense No. 37186						

The Department reserves the right in cases of violation of permit specified ground water limits or Ground Water Quality Standards (N.J.A.C. 7:9-6.1 et seq.) to require that wells be resurveyed to an accuracy of one-hundredth of a second latitude and longitude. "shall not be considered to be a major modification of the N.J.P.D.E.S. permit.

form-b.doc

PROFESSIONAL LAND SURVEYOR'S LICENSE #

#### GROUND WATER MONITORING WELL CERTIFICATION - FORM B - LOCATION CERTIFICATION

Name of Permittee:	_216 Paterson Plank Roa	d Cooperating	z PRP Group						
Name of Facility:	Name of Facility: 216 Paterson Plank Road Site								
Location:	216 Paterson Plank Roa	d. Carlstadt	Boro, Bergen County						
NJPDES Number:									
LAND SURVEYOR'S CERTIF	<u>FICATION</u>								
Well Permit Number (As assigned	by NJDEP's Bureau of Water	26-44020	)						
Allocation):		-		-					
This number must be permanently	affixed to the well casing.			•					
Datum NAD 1927									
Longitude (one-tenth of a second)		West	74°04'23.26"						
Latitude (one-tenth of a second):		North	40°49'25.17"						
Elevation of Top of Casing (cap of	ff) (one-hundreth of a foot):	WC = 6.41 / 1	IC = 8" 6.25 IC 4"=6.19	GRD=6.41					
Owners Well Number (As shown	on application or plans):	MW-11R							
BENCHMARK -	G.P.S. NETWORK	ELEVATIO	N -						
<b>GEOGRAPHIC POSITION</b> -									
TE OF SURVEY -	9/19/96								
<u>'</u>									

#### **AUTHENTICATION**

I certify under penalty of law that I have personally examined and am familiar with the information submitted in this document and all attachments and that, based on my inquiry of those individuals immediately responsible for obtaining the information, I believe the submitted information is true, accurate and complete. I am aware that there are significant penalties for submitting false information including the possibility of fine and imprisonment.

PROFESSIONAL LAND SURVEYOR'S SIGNATURE

Paul J. Emilius, Jr.

PROFESSIONAL LAND SURVEYOR'S NAME (Please print or type)

**SEAL** 

New Jersey P.L.S. License No. 37186

PROFESSIONAL LAND SURVEYOR'S LICENSE #

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#### GROUND WATER MONITORING WELL CERTIFICATION - FORM B - LOCATION CERTIFICATION

Name of Permittee:	216 Paterson Plank Ro	ad Cooperatin	g PRP Group				
Name of Facility:	216 Paterson Plank Road Site						
Location:	216 Paterson Plank Road, Carlstadt Boro, Bergen County						
NJPDES Number:							
LAND SURVEYOR'S CERTIF	<u>FICATION</u>						
Well Permit Number (As assigned Allocation):	d by NJDEP's Bureau of Water	26-44016					
This number must be permanently Datum NAD 1927	y affixed to the well casing.						
Longitude (one-tenth of a second)	<b>):</b>	West	74°04'16.45"				
Latitude (one-tenth of a second):		North	40°49'27.27"				
Elevation of Top of Casing (cap of	off) (one-hundreth of a foot):	WC <u>2.45</u> /I	C8" = 2.38  IC  4" = 2.19  GRD = 2.45				
Owners Well Number (As shown	on application or plans):	MW-14D					
BENCHMARK - GEOGRAPHIC POSITION -	G.P.S. NETWORK	ELEVATION	[				
PATE OF SURVEY -	9/19/96						
AUTHENTICATION							
all attachments and that, based o	n my inquiry of those individual e, accurate and complete. I an	s immediately resp	the information submitted in this document are onsible for obtaining the information, I believe are significant penalties for submitting false				
PROFESSIONAL LAND SUR	VEYOR'S SIGNATURE						
PROFESSIONAL LAND SUR	AVETOKŲ SIGIVATORE						
Paul J. Emil	lius, Jr.						
PROFESSIONAL LAND S	SURVEYOR'S NAME	SEAL					
(Please print	or type)						
New Jersey P.L.S. Li							
PROPESSIONAL LAND SH	R V B Y O R'N LICENNE #						

The Department reserves the right in cases of violation of permit specified ground water limits or Ground Water Quality Standard A.C. 7:9-6.1 et seq.) to require that wells be resurveyed to an accuracy of one-hundredth of a second latitude and longitud shall not be considered to be a major modification of the N.J.P.D.E.S. permit.

### **GROUND WATER MONITORING WELL CERTIFICATION - FORM B - LOCATION CERTIFICATION**

Name of Permittee:	216 Paterson Plank Ro	ad Cooperat	ting I	RP Grou	ıp		
Name of Facility:	216 Paterson Plank Road Site						
Location:	216 Paterson Plank Road, Carlstadt Boro, Bergen County						
NJPDES Number:						<del></del>	
LAND SURVEYOR'S CERTIF	FICATION				-		
Well Permit Number (As assigned Allocation):	l by NJDEP's Bureau of Water	26-44	4017 -			<u></u>	
This number must be permanently Datum NAD 1927	_						
Longitude (one-tenth of a second)	:	West			4°04'16.36"		
Latitude (one-tenth of a second):		North	40°49'27.23"				
Elevation of Top of Casing (cap of		_	2.37	_/IC =	2.22 /GRD =	2.37	
Owners Well Number (As shown	on application or plans):	<u>MW-14R</u>			<del></del>	<del></del> ,	
BENCHMARK - GEOGRAPHIC POSITION -	G.P.S. NETWORK	ELEVATIO	ON -		<del></del>	<del></del>	
PATE OF SURVEY -	9/19/96						
AUTHENTICATION							
I certify under penalty of law that all attachments and that, based or the submitted information is true information including the possibili	n my inquiry of those individuals e, accurate and complete. I am	immediately re	esponsi	ble for obt	taining the inform	ation, I believe	
PROFESSIONAL LAND SUR	VEYOR'S SIGNATURE						
71107220907112 21110 0010	is significant						
Paul J. Emil	ius. Jr.		-				
PROFESSIONAL LAND S		SEA	L				
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New Jersey P.L.S. Lie							
PROFESSIONAL LAND SUF	CVEYOR'S LICENSE#						

The Department reserves the right in cases of violation of permit specified ground water limits or Ground Water Quality Standards C \* A.C. 7:9-6.1 et seq.) to require that wells be resurveyed to an accuracy of one-hundredth of a second latitude and longitude. shall not be considered to be a major modification of the N.J.P.D.E.S. permit.

#### GROUND WATER MONITORING WELL CERTIFICATION - FORM B - LOCATION CERTIFICATION

Name of Permittee:	216 Paterson Plank Road	d Cooperat	ting P	RP Gro	up		
Name of Facility:	216 Paterson Plank Road Site						
Location:	216 Paterson Plank Road, Carlstadt Boro, Bergen County						
NJPDES Number:							
LAND SURVEYOR'S CERTIF	<u>ICATION</u>						
Well Permit Number (As assigned Allocation):	by NJDEP's Bureau of Water	26-44	401 <u>2</u>		•		
This number must be permanently Datum NAD 1927	affixed to the well casing.						
Longitude (one-tenth of a second):		West			74°04'27.71"		
Latitude (one-tenth of a second):		North			40°49'26.33"		
Elevation of Top of Casing (cap of		WC =	9.68	/IC =	9.47 /GRD = $9.68$		
Owners Well Number (As shown of	on application or plans):	MW-15D			<del></del>		
BENCHMARK - GEOGRAPHIC POSITION -	G.P.S. NETWORK	ELEVATI	ION -	<del></del>			
GEOGRAPHIC POSITION -							
DATE OF SURVEY -	9/23/96						
)							
<u>AUTHENTICATION</u>							
I certify under penalty of law that	I have personally examined and an	n familiar wi	ith the in	nformatio	on submitted in this document and		
all attachments and that, based on	my inquiry of those individuals in	nmediately r	esponsil	ole for o	btaining the information, I believe		
the submitted information is true	, accurate and complete. I am a	ware that th	пеге аге	significa	ant penalties for submitting false		
information including the possibilit	ty of fine and imprisonment.						
	/						
last and	¬ 1/2						
PROPESSIONAL LAND SURV	VEYOR'S SIGNATURE						
Paul J. Emili	us, Jr.						
PROFESSIONAL LAND SU		SEA	<b>\L</b>				
(Please print o	r type)						
New Jersey P.L.S. Lic	ansa No. 37186						
PROFESSIONAL LAND SUR							

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### **GROUND WATER MONITORING WELL CERTIFICATION - FORM B - LOCATION CERTIFICATION**

NI CD III							
Name of Permittee:	216 Paterson Plank Road Cooperating PRP Group						
Name of Facility:	216 Paterson Plank I	Road Site			<u></u>		
Location:	216 Paterson Plank I	Road, Carlst	adt Bo	oro, Bergen Count	У		
NJPDES Number:							
LAND SURVEYOR'S CERTIF	<u>FICATION</u>						
Well Permit Number (As assigned Allocation):	1 by NJDEP's Bureau of Water	26-4402	1	=	-		
This number must be permanently	y affixed to the well casing				<del></del>		
Datum NAD 1927	, armou to the won ousing.						
Longitude (one-tenth of a second)	:	West		74°04'23.12"			
Latitude (one-tenth of a second):		North		40°49'28.71"	·		
Elevation of Top of Casing (cap of	off) (one-hundreth of a foot):	WC = 7.58	/IC =	8" 7.50 IC 4"=6.59	GRD=7.25		
Owners Well Number (As shown	on application or plans):	MW-16D		· .			
BENCHMARK -	G.P.S. NETWORK	ELEVATIO	ON -				
<b>GEOGRAPHIC POSITION</b> -							
TE OF SURVEY -	9/19/96						
AUTHENTICATION							
I certify under penalty of law that all attachments and that, based of the submitted information is true information including the possibility	n my inquiry of those individuals e, accurate and complete. I an	s immediately re	sponsib	ole for obtaining the inf	formation, I believe		
PROFESSIONAL LAND CUD	VEVOD'S SIONATIDE						

Paul J. Emilius, Jr.

PROFESSIONAL LAND SURVEYOR'S NAME

(Please print or type)

**SEAL** 

New Jersey P.L.S. License No. 37186

PROFESSIONAL LAND SURVEYOR'S LICENSE #

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#### **GROUND WATER MONITORING WELL CERTIFICATION - FORM B - LOCATION CERTIFICATION**

Name of Permittee:	216 Paterson Plank Ro	ad Cooper	rating PRP Group	
Name of Facility:	216 Paterson Plank Ro	ad Site		
Location:			stadt Boro, Bergen County	
NJPDES Number:				
LAND SURVEYOR'S CERTIF	<u>ICATION</u>			
Well Permit Number (As assigned Allocation):	by NJDEP's Bureau of Water	26-	-44018	
This number must be permanently	affixed to the well casing.		<del></del>	_
Datum NAD 1927				
Longitude (one-tenth of a second):		West	74°04'11.44"	
Latitude (one-tenth of a second):		North	40°49'20.95"	
Elevation of Top of Casing (cap of	ff) (one-hundreth of a foot):	WC =	5.05 /IC = $4.75$ /GRD = $5.05$	
Owners Well Number (As shown of		MW-17I	D	
BENCHMARK -	G.P.S. NETWORK	ELEVA	TION	
GEOGRAPHIC POSITION -				
DATE OF SURVEY -	9/23/96			
A. THENTICATION				

I certify under penalty of law that I have personally examined and am familiar with the information submitted in this document and all attachments and that, based on my inquiry of those individuals immediately responsible for obtaining the information, I believe the submitted information is true, accurate and complete. I am aware that there are significant penalties for submitting false information including the possibility of fine and imprisonment.

PROFESSIONAL LAND SURVEYOR'S SIGNATURE

\_\_ Paul J. Emilius, Jr.

PROFESSIONAL LAND SURVEYOR'S NAME

**SEAL** 

(Please print or type)

New Jersey P.L.S. License No. 37186

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#### **GROUND WATER MONITORING WELL CERTIFICATION - FORM B - LOCATION CERTIFICATION**

Name of Permittee:	_216 Paterson Plank Ro	oad Cooperati	ng PRP Gro	oup				
Name of Facility:								
Location:	216 Paterson Plank R		t Boro, Be	ergen County				
NJPDES Number:								
LAND SURVEYOR'S CERTII	FICATION							
Well Permit Number (As assigned	l by NJDEP's Bureau of Water	26-4401	9					
Allocation):				<u> </u>				
This number must be permanently Datum NAD 1927	arrixed to the well casing.							
Longitude (one-tenth of a second)	•	West		74°04'11.50"				
Latitude (one-tenth of a second):	•	North		40°49'20.86"				
Elevation of Top of Casing (cap of	off) (one-hundreth of a foot):	$WC = \overline{5.2}$		4.51 /GRD = 5.23				
Owners Well Number (As shown	on application or plans):	MW-18D						
BENCHMARK -	G.P.S. NETWORK	ELEVATION	· -					
GEOGRAPHIC POSITION -								
DA <u>te of survey</u> -	9/23/96							
A - (THE PAIRS OF THE PAIR								
<u>AUTHENTICATION</u>								

I certify under penalty of law that I have personally examined and am familiar with the information submitted in this document and all attachments and that, based on my inquiry of those individuals immediately responsible for obtaining the information, I believe the submitted information is true, accurate and complete. I am aware that there are significant penalties for submitting false information including the possibility of fine and imprisonment.

PROFESSIONAL LAND SURVEYOR'S SIGNATURE

Paul J. Emilius, Jr.

PROFESSIONAL LAND SURVEYOR'S NAME (Please print or type)

SEAL

New Jersey P.L.S. License No. 37186
PROFESSIONAL LAND SURVEYOR'S LICENSE #

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## APPENDIX C

Well Development Forms

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<del></del>							· • • • • • • • • • • • • • • • • • • •	
JOB NAME	SCP Car	Istact		JOB NO.	94	3-6222	WELL NO.	MW-8R
DEVELOPED BY	M. Elsner		_	DATE OF	INSTALL		SHEET	/ OF I
DEVELOPED BY STARTED DEVEL	7/30/961	1452	_	COMPLE	TED DEVEL	7/30/	96116	05
	DATE	IME	-					
W.L. BEFORE DEV	/EL. 4,5 <i>0  </i>	7/30 11354	-	AFTER D	EVEL.		/ DATE TIME	<del></del>
	DEPTH D.	ATE TIME						
WELL DEPTH: BE	FORE DEVEL.	93,0	-	_				(n) 2.0
STANDING WATER	R COLUMN (FT.)	88.5	-					<u>O</u> gal.
SCREEN LENGTH	_ 10.0	HeeT	-	DRILLING	3 WATER LC		O g.	algal.
	-					<del></del>		
Í	VOLUME	FIELD	PARAME	ETERS	Turbidity	ł		
DATE/TIME	REMOVED	SPEC. COND.			(NTV) OTHER	1	REMARKS	1
	(GALS)	(umhos/cm)	(¢ <sub>F</sub> )	(s.u.)	OTHER			
7-30-96/1500		328		11.36		Begin po	umping =	2.0 apm Clear
11 /1520	30gal	2190	63.6	10.04	10.9	Water	Sample	Clear
11 /1530	45gal	2250	63.7	9,43	23.6 15.3	11	11	11
11 /1600	45gal 60gal 105gal	23.80	63.0	9.18	19,5	71	11	11
	J							
)	<del> </del>			<del> </del>		ļ		
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	·	_						
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<del></del>	<del> </del>	<del></del>		<del> </del>		<del> </del> -		
			<del></del>	<del> </del>				
								· · · · · · · · · · · · · · · · · · ·
ļ					L	L		<del>`</del>
L	105	= TOTAL V	OLUME R	EMOVED	(gal.)		<del></del>	
					0			
DEVELOPMENT M	ETHOD:	Grundfos_	<u>Redi F</u>	low 2	Pump,	<u>Αρριοχίι</u>	nately .	7 well
volumes rei	noved. Deve	lopment Com	pleted	as per	USEPA	oversig	ht (ICF	Kaiser).
<del></del>								
		<del></del>					<del></del>	
								<del></del>
NOTES:		<u>P</u>						
•								
							•	



DB NAME   SCP   Col + a) +   JOB NO.   9/3 - 6222   WELL NO.   M(b - 10)	OB NAME			DEVELO				
DATE OF INSTALL.  SHEET / OF STATEMENT OF STANDING WATER COLUMN (FT.)  DATE TIME  VILL BEFORE DEVEL. +0.4'		<b>:</b>	SCP Cab+	-16		JOB NO.	943-1	6272 WELL NO. MW-10)
COMPLETED DEVEL	EVELOPE	ED BY	5 mitches	ıl				
Volume	TARTED	DEVE	01-101	(2940	_	COMPLE	TED DEVEL	2 h 161 1 1534
Volume	.,,,,,,	DL V LL.	DATE	 TIMF	_	OOM EE		DATE TIME
VOLUME						AETED C	NEVEI	10 05 18/2/51 1 M740
VOLUME	.L. BEFO	THE DEV	DEDTH C	8/12/16/ 0/25	_	ALIENT	EVEL.	DEPTH DATE TIME
STANDING WATER COLUMN (FT.)								do determina ou de de
DATE/TIME   REMOVED   SPEC. COND.   TEMP.   ph   Turbishy   OJHER     1/2   96   0940							DEVEL.	17.01 WELL DIA. (III) 17.0
DATE/TIME   REMOVED   SPEC. COND.   TEMP.   ph   Turbishy   REMARKS     1/2   1/3   6940					_	STANDIN	NG WELL VO	DLUME 27 gal
DATE/TIME REMOVED (GALS)  (GALS)  (Umhos/cm)  (Su.)   CREEN L	ENGTH	: <u>* 5,0</u>	feet	_	DRILLIN	G WATER LO	OSS <u>0</u> gal.	
DATE/TIME REMOVED (GALS)  (GALS)  (JOHN COND. (JOHN COND.)	•							
DATE/TIME REMOVED (GALS)    DATE/TIME   REMOVED (GALS)   SPEC. COND.   TEMP.   DH   Turbish!   Surje (with Surje blink for Sometry Som		<u> </u>	VOLUME	FIEI	D DADAME	TEDE	<del></del>	
(GALS) (umhos/cm) (GS.U.) OTHER    192996   6940   Surge with Surge black for   5 minter     0954   33   The lett with 3" Submiguity   1054   23   Will Parked Selection     1106   Well Remote Selection     1110   85.D   10.10   Well Remote Only 3.5 feath   1111   26   659.D   80.1   11.90   69.5/cit   Vary funds.) - John Collish Brown   1111   Will Parked to Alexe dryness   1254   Surge with Surge blown   1254   Surge with Surged, from   1254   Surge with Surged, from   1255   Surge with Surged, from   1256   Surged to the Surged, from   1257   Surged to the Surged, from   1258   Surged to the Surged, from   1259   Surged to the Surged, from   1259   Surged to the Surged, from   1259   Surged to the Surged, from   1250   Surged to the Surged, from   1250   Surged to the Surged, from   1251   Surged to the Surged to the Surged, from   1251   Surged to the Surged to the Surged, from   1251   Surged to the Surged to t	DATE/T	IME					Turbis.tr	REMARKS
22   16   109	<b>·</b>					•	•	
0954   3" Someonic   1054   3" Someonic   1054   23   1170   11.90	<u> </u>	60.1-	T	ļ , , , , , , , , , , , , , , , , , , ,	- 'F	T	NTJ	
1005   1106   1170   85.5   7.98   350   115th from   1602   26.5   1770   88.5   7.98   350   115th from   1608   1708	125116 1	6460	<del> </del>	<del></del>	<del></del>	<del> </del>	<del> </del>	
10054   Q3	+	Mari	<del> </del>	<del></del>	<del> </del>	<del> </del>	<del> </del>	
0959 93    Unil Pumper to Mer dryneps (W +1 of Green)   1106	<del></del>	U137	<del> </del>	<del> </del>	+	<del> </del>	<del> </del>	
106	<del>                                     </del>	0954	23	<del> </del>	<del>                                     </del>		<del> </del>	
106	<del></del>	<u> </u>	<del> </del>	<del>                                     </del>	-		<u> </u>	
1109		1106	<del> </del>			<del> </del>	<del> </del>	
1112 26 6590 80.1 11.90 off-sick Very trob.) - den (cols) brown  1114  1254  1254  1254  1254  1255  1256  1257  1258  1			<del> </del>	GYL	85.5	10.10	655	
1114			26		+	7	+	Vor took ) - dark (c)) A brown
1254   Sura bell with Singe block   for 5 minutes Pune will with   3" (une - AND with Surged), from   Screen from - AND with Surged), from   Screen from - AND with Surged, from - AND w				1	1			bull Pumpes to near dryness
for 5 minutes Pump well with   3" (non - AND with Sorged), from   Sevent from   Seve								
Sevel fires to excellent level		-						
Sevel   f.nes to excellent level								
1602   26.5   1470   88.5   9.98   350   Shightly 4.6.0     1606   07.5   1600   8/.8   9.90   021   " " "     1608   08.0   1180   82.3   10.35   178   " "     = TOTAL VOLUME REMOVED (gal.)								Screen times to excellente Per
1602 26.5			<u> </u>					bull your is LO.1 gpm
, 1606 37.5 /0/D 8/.8 9.90 321 "" "  // 1608 38.0 1180 82.3 /0.35 178 " "  = TOTAL VOLUME REMOVED (gal.)		1600						Begin Pumping at 0.3 gla
V 1658 38.0 1180 82.3 10,35 178 " " "  = TOTAL VOLUME REMOVED (gal.)				1475	188.5		<del> </del>	Slightly to-6.0
TOTAL VOLUME REMOVED (gal.)				1110				
	_	1602	27.5	1010				<u> </u>
		1602 1606	27.5	0/0/ 0/811	P2.3	10,35	178	<u> </u>
		1602 1606	27.5	0/0/ 0/811	P2.3	10,35	178	<u> </u>
	EVELOPM	/6 0 2 160 b 1608 MENT M	97.5' 98.0	1180 = TOTAL \  Gruntfos Sylm	P2.3 OLUME RI	10,35' EMOVED	(gal.) Bick by	er injection
	EVELOPN Poll Peco	/6 0 2  60 6  608 MENT M	97.5 98.0 PETHOD:	1180 = TOTAL \ Grundfos Sylm Yillo 4 0.1	PR.3 VOLUME RI	Sune Sune	(gal.) Blick WH	or injection  Courth development -
ater intoduced in the Well was immediately removed. A Combination of Pumping and Surging	EVELOPN Icil Reco	1602 1608 1608 MENT M	97.5' 98.0 DETHOD: 'Cy Slow (A	1180 = TOTAL V Grundos Sylm Yillo L O.1	PR.3 VOLUME RI VE.J. PUMP SIMD - US. PEMOVA.	10,35 EMOVED  Surge  Surge  A Cimbi	(gal.)  Block Wat to helf	or injection  with development -  Purply an Surgay
weter introduced in the well was immediately removed. A Combination of Property and Sursing with a Surse block was used for well Development. Approximately 99 Jailles of Water	EVELOPA 1011 Peco ato into	1602 1608 1608 MENT M	97.5' 98.0  JETHOD:  (Cy Slow (&  the well we block wo us	Gruntos Salm Yill 2 0.1 inmediately  for bell I	PR.3 VOLUME RI SIM) - US remova. Development	Surge Surge Surge Surge A Cimbi	(gal.)  Block WH to helf astin of	or injection  with development -  Purply an Surgay
enter introduced in the Well Was immediately removed. A Combination of Pumping and Surging	EVELOPA 1011 Peco ato into	1602 1608 1608 MENT M	97.5' 98.0  JETHOD:  (Cy Slow (&  the well we block wo us	Gruntos Salm Yill 2 0.1 inmediately  for bell I	PR.3 VOLUME RI SIM) - US remova. Development	Surge Surge Surge Surge A Cimbi	(gal.)  Block WH to helf astin of	or injection  with development -  Purply an Surgay
water introduced in the Well Was immediately removed. A Combination of Pumping and Surging with a Surge block was used for well Development. Approximately 99 Jailies of Water	EVELOPA 1011 Peco ato into	1602 1608 1608 MENT M	97.5' 98.0  JETHOD:  (Cy Slow (&  the well we block wo us	Gruntos Salm Yill 2 0.1 inmediately  for bell I	PR.3 VOLUME RI SIM) - US remova. Development	Surge Surge Surge Surge A Cimbi	(gal.)  Block WH to helf astin of	or injection  with development -  Purply an Surgay
water introduced in the Well Was immediately removed. A Combination of Pumping and Surging with a Surge block was used for well Development. Approximately 99 Jailies of Water	EVELOPA 1011 Peco ato into	1602 1608 1608 MENT M	97.5' 98.0  JETHOD:  (Cy Slow (&  the well we block wo us	Gruntos Salm Yill 2 0.1 inmediately  for bell I	PR.3 VOLUME RI SIM) - US remova. Development	Surge Surge Surge Surge A Cimbi	(gal.)  Block WH to helf astin of	or injection  with development -  Purply an Surgay
with intology in the well was immediately removed. A Combination of Purpose and Surging with a Surge block was used for well Development. Approximatly 99 Jailles of Water pur comoved (excluding the water albed to and development)	EVELOPN Poll Reco who into	1602 1608 1608 MENT M	97.5' 98.0  JETHOD:  (Cy Slow (&  the well we block wo us	Gruntos Salm Yill 2 0.1 inmediately  for bell I	PR.3 VOLUME RI SIM) - US remova. Development	Surge Surge Surge Surge A Cimbi	(gal.)  Block WH to helf astin of	or injection  with development -  Purply an Surgay
wet intoduced in the well was immediately removed. A Combination of Property and Sursing with a Surse block was used for well Development. Approximately 99 Jailles of Water	EVELOPN Poll Reco who into	1602 1608 1608 MENT M	97.5' 98.0  JETHOD:  (Cy Slow (&  the well we block wo us	Gruntos Salm Yill 2 0.1 inmediately  for bell I	PR.3 VOLUME RI SIM) - US remova. Development	Surge Surge Surge Surge A Cimbi	(gal.)  Block WH to helf astin of	or injection  with development -  Purply an Surgay
et into Suc) in the Well Way immediately removed. A Combination of Purpose and Sursing with a Surse block the Uses for well Development. Approximately 99 Jailles of Weter all Icmoved (excluding the wester alles) to as development)	EVELOPN Poll Reco who into	1602 1608 1608 MENT M	97.5' 98.0  JETHOD:  (Cy Slow (&  the well we block wo us	Gruntos Salm Yill 2 0.1 inmediately  for bell I	PR.3 VOLUME RI SIM) - US remova. Development	Surge Surge Surge Surge A Cimbi	(gal.)  Block WH to helf astin of	or injection  with development -  Purply an Surgay



	_					
JOB NAME	SCP Cals	+43+	_	JOB NO.	94	13-6222 WELL NO. MW- 10
DEVELOPED BY	_ S. M.tch	eil		DATE OF	INSTALL.	SHEET 2 OF
STARTED DEVEL.	8/22 16 1	0940	_			. <u> </u>
	DATE	TIME	-	_		DATE TIME
W.L. BEFORE DEV	'EL. /	1		AFTER D	EVEL.	
	DEPTH C	DATE TIME	-			DEPTH DATE TIME
WELL DEPTH: BEF	ORE DEVEL.			AFTER D	EVEL.	WELL DIA. (In)
STANDING WATER	COLUMN (FT.)	•	-		IG WELL VO	
SCREEN LENGTH			-		G WATER LO	·
			_			·
	VOLUME	FIELD	D PARAME	TERS		
DATE/TIME	REMOVED	SPEC. COND.	TEMP.	pН	Turbis,ly	REMARKS
	(GALS)	(umhos/cm)	10/	(s.u.)	OTHER	
8/22/96 /1610	28.5	1490	83.9	10.77	1 142	Clouly
1612		1 7770	05,7	7 7	1 / 4	PUAD TAK 0.258 m
1613	29.0	1973	86.4	10,99	134	
1616	04.5	2120	88.0	11.09	132	
1622	30.5	CCFC	90.0	11,10	135	Cloudy
1625	31,0	2460	91.2	11.13	191	Cloudy
1629	3 <i>2</i> . ي		91.2	11.15	142	(/0034
/630						Stiles Pumping
<u> </u>		ļ	ļ		<b>}</b>	Total Dept. ( Mil. 42.0 69)
	<del></del>	<del> </del>	<u> </u>		<del> </del>	- [cmored 0.5 of Sediment
8/23/96 / 0745					<del> </del>	Total Durth of Well 42.0 '695 Deeth to make 19.2' 695
0814		<del> </del>				Surge Well Wife Surger Block for
0.17						5 marty
0824						Bus programe 0.258m
0825	0.2	2180	78.5	11.16	64	I IX.A FOMPING E O.S. JIM
6828	0,6	2270	76,9	1.37	164	Cloudy
0837	2.6	1250	78.4	11.12	618	Turb. ) - redlint - brewn
0848	4,6	V22,0	79.2	10.84	<i>1</i> 032	TUILID . 11 11-
		= TOTAL V	OLUME RI	EMOVED	(gal.)	
EVELOPMENT MI	ETHOD:					
	<u> </u>					
IOTES:						



		***	- DE VELOT	14117141	1	3	
JOB NA	ME	SCP (arb.	falt.	_	JOB NO.	943	3-6222 WELL NO. MW-10D
DEVELO	OPED BY	S.M.K	٧ <i>ا</i>		DATE OF	INSTALL.	SHEET 3 OF S
STARTE	ED DEVEL.	8/22/96 1	0944	-	COMPLE	TED DEVEL	/
		DATE	TIME	_			/ DATE TIME
W.I. BE	FORE DEV	/EI /	1			EVEL.	
	0112024	DEPTH (	DATE TIME	-	AL ILITO		DEPTH DATE TIME
MELL D			ATE TIME		A	ריבו	
		FORE DEVEL.		-			WELL DIA. (In)
STANDI	NG WATER	R COLUMN (FT.)	'	-	STANDIN	IG WELL VO	OLUMEgal.
SCREE	N LENGTH	•		_	DRILLING	WATER LO	OSSgal.
							· 
		VOLUME	FIELD	D PARAME	TERS	T 1.11	
DAT	E/TIME	REMOVED	SPEC. COND.	TEMP.	pН	Turbishy	REMARKS
		(GALS)	(umhos/cm)	Set	(s.u.)	OTHER	· ·
2/2.190	10838	1 / /	/630	80.2		795	Turbis- Cellish brown
<u> </u>	0907	8.6	1780	80.1	10.85		11 11
-+	0917	10.6	6991	80.7	10.99		<del>                                     </del>
	0438	11.6	280	83.6	11.01	144	Cloudy
	0940	77.8	<del>  300</del>	05.6	11.07	/ / / / /	Pum off. Surx will will
	0170	<del> </del>		<del>                                     </del>			Sus Block for 10 months
-+	101/2		<del></del>	<del> </del>	<u> </u>		Basin Rumbing Q 0.2 5Pm
	1043	14.8	2260	87.9	10.92	off-scry	1 25.4 10.41.43
	1018	12.8	1770	82.1	10.77		Turbis. Cossist down
	10:5	17.0	1960	81.5	10.70	960	7
	1104	18.8	1990	88.7	10.91	949	Turd. J - Collish brown
	1)13	20.5					Pumery rik 0.4 91m
	1114	21.0	1915	88.3	10.82	954	1
	1112	51.4	1480	88.3	10.89	659	Tuidid. reddit brown
	1117	22.0	1990	88.6	10.90		PUMP Shit off - Well new dryn
	1334						Beg. Rumping @ O.5 gpm
	1335	22.5	2225	99.7	10.73	670	Turbs - restish brown
	1340	55.5	1450	85.0	10.69	3/8	Slightly Turb.)
V	1343	26.5	1760	85.6	10.70	228	
		-	= TOTAL V	OLUME R	EMOVED	(gal.)	
		·· <del>·····</del>	<u> </u>				
EVELC	PMENT M	ETHOD:					
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	-						
		<u></u>	<del> </del>				
IOTES-							
OTES:			'n				



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JOB NAME	SCP Cali	tast		JOB NO.	943	-6222 WELL NO. Mb./0)
DEVELOPED BY	Smite	h.il	-	DATE OF	INSTALL.	SHEET 4 OF 5
STARTED DEVEL.	2/22/96 1	5941	<del>-</del>			
OTTAINED DEVEL.	DATE	 TIME	_	OOM! LL	TED DEVEL	. / DATE TIME
W.L. BEFORE DEV	/FL /	, ,				
	DEPTH D	ATE TIME	_	AL ILITO		/ / DEPTH DATE TIME
WELL DEPTH: BEF				AFTERD	EVEL.	WELL DIA. (In)
STANDING WATER		•	_		IG WELL VO	
SCREEN LENGTH			_			
SOUTE N LEWGIN	<del></del>		_	DHILLING	3 WATER LO	OSS gal.
	VOLUME	FIELI	D PARAME			
DATE/TIME		SPEC. COND.		рН	Turbisity	REMARKS
	(GALS)	(umhos/cm)		(s.u.)	ОТНЕН	
8/23/16 /1346	28.0	2040		88.01		Cloudy
1348	29 0	2330		10.96		11
1351	30.5	24/0	93.9	10.99		11
1355	32.5	2130	944	11.01	138	4
V 1400	35.0					Pum shil. OH. Weil near
			<u> </u>	ļ		genera
8/26/96 /0854			ļ	ļ		TOtal Deptail will 41.80' bs
1			ļ			Dorth to Water 8.30'615
2280			<del> </del>	-	<u> </u>	Sirse Well with Sugar ofoch
0144	_		<del> </del>			for 10 minutes
0945	0,4	/342	73	11.17	418	Bein funding P ay sim
0947	0.4	137.0	1.73	1. 11.18	710	Purping rike 0.3 cpm
0948	2,0	1250	73. 1	11.50	3-71	Very fuels. 102124 6:02
0952	3,2	1390	77 -	11.50	564	Turb; )
0157	4.4	MLD	80.6	11.33	1084	l,
1005	6.8	1580	82.4	11.3/	183	· · ·
1 1013	9.0	1580	83.0	11.53	3/0	Stuffly tob. ). (2) . It brown
V /027	13.0	1700	83.6	11.51	249	· .
		= TOTAL V	OLUME R	EMOVED	(gal.)	
DEVELOPMENT MI	ETHOD.					
DEVELO: MENT M	LITIOD.	· <del>- · · · · · · · · · · · · · · · · · ·</del>			····	
	<del></del>	<del></del>				
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NOTES:						
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			_	JOB NO.	943	6257	WELL NO.	MW-10-	
EVELOPED B	Y _ S.M.	itchell	_	DATE OF	INSTALL.		SHEET	OF_	
TARTED DEV	EL. 8/22/16	1 Ofty		COMPLE	TED DEVEL.	<i>1</i>			
	DATE	TIME					DATE TI	ME	
				AFTER C	EVEL.		1 1		
	DEPT	H DATE TIME	_			DEPTH	DATE TIME		
/ELL DEPTH:	BEFORE DEVE	1.		AFTER C	EVEL.		WELL DIA.	(in)	
		<del></del>					•		
	_	(٢١.)	_		-			9	
CREEN LENG	·		_	DHILLING	WATERLO		<del></del>		
	VOLUME	FIEI	D PARAME	TERS			···		
DATE/TIME					Tur6.J.14		REMARKS	3	
2 I I IIIL		1		•				-	
1-6-1-							· ·		
				<del></del>			7À		
			<del></del>	,	<del></del>				
		- 100	86. 7	11.64	154		1.10 1 11	(in descri	
		<del></del>	<del> </del>	<del> </del>	<del> </del>				
		1745	87,	GCLL	13.2			1.7 1.6W	
					<del>                                     </del>				
								<del></del>	
	-		<del></del>			11			
/522						li.			
		1570			63	H			
123.		1540	83.2	11.94	62	Clear			
1520		122.0	83.4	11.47	60			٠.	
1/3/	3 0. 0	1570	85.3	11.43	2.5	Cley			
123.	31.0	1270	86.4.	11.43	55	LIELI			
153	DEPTH DATE TIME  H: BEFORE DEVEL.  WATER COLUMN (FT.)  ME  WOLUME  REMOVED  (GALS)  (Umhos/cm)  ME  PIELD PARAMETERS  PARAMETERS  PARAMETERS  (Umhos/cm)  ME  PREMOVED  (GALS)  (Umhos/cm)  ME  PREMOVED  (GALS)  (Umhos/cm)  ME  PREMOVED  (GALS)  (Umhos/cm)  ME  PREMOVED  (GALS)  (Umhos/cm)  ME  PREMOVED  (S.U.)  OTHER  PREMOVED  PREMOVE								
			<b></b>						
				ļ					
			<u> </u>						
		= TOTAL \	VOLUME R	EMOVED	(gal.) 9	1. O			
•									
EVEL ODMEN	METHOD:								
LILLOFINEN	WEITIOD.								
	<del></del>								
	-								
			<del></del>						
OTES:		_						•	
OTES.		i,							



						D RECC	
		Scr Carlsto		_	JOB NO.	. 94	5-6-72 WELL NO. /W-10R
DEVELOPED	BY _	S. M.tc	est	_	DATE OF	INSTALL.	SHEET _/_OF_3
STARTED DE	VEL.	7/27/96 1	0905 TIME	_	COMPLE	TED DEVEL.	3-6272 WELL NO. MW-10 R SHEET 1 OF 3  B/28/76 1 /536  DATE TIME
W.L. BEFORE	E DEVE	L. 7.25 / 1/2	1/21/96/ 0845 ATE TIME	-	AFTER (	DEVEL. (	0.80 18 28/961 0731 DEPTH DATE TIME
			65.61				·
				-	AFIERL	JEVEL.	WELL DIA. (In) 2.0 Cas.,
			<u> 58:4 '</u>				LUME 38.0 gal.
SCREEN LEN	IGTH	· /o'		-	DRILLIN	G WATER LC	OSS <u>400</u> gal.
		VOLUME		D PARAME	TERS		
DATE/TIM	IE I	REMOVED (GALS)	SPEC. COND. (umhos/cm)	TEMP.	pH (s.u.)	Turkishy OTHER	REMARKS
867/96/09	05		<del></del>			T 713	Basa Pumpa, @ 1,0 spm
	07	2.0	490	67.7	8.90	off-suh	Very tirbio. (cas. in brown
<del>-   •</del>	-		7.75		1170	1011 1614	Pump shit-off du to
	<del> </del>						too much Silt
69	1/0						Pune on - luren a D.7912
01	915	5.5	470	71,1	7,18	04-56.4	Vertueb. 3- Call. 14 brama
09	929	15.0	510	73.4	9,00	339	vit u
	956	3 <i>4.0</i>	₹7 <b>3</b>	71.7	8,44	840	10 11
100	٥٥						Punping Cate Q 1.8 scm
112	9	194	620	72.7	7.61	305	Stratly toob, )
113	33					ļ	Proping rate @ 1.05Pm
	15	213	660	74,2	8.00	168	Cloudy
	35	963	7/0	74,1	8.08	751	Tursis-105114 brown
	522	283	680	74.1	8.07	85	Cloud
15.	47			ļ			PUMPING 14th @ 1.25/m
		····				ļ	Pure in rate increased to
			7-2				1.4 sin e 1302
	80	300	<u>680</u>	72.2	40.8	56	Clew
V [3	38	320	750	71.6	8.20	71	Cloudy
			= TOTAL V	OLUME RE	MOVED	(gal.)	} }

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<del></del>		DEVELOT		1 1 1 1 1 1	J IILUC	
JOB NAME DEVELOPED BY	SCP Curb	44.24		JOB NO.	9	143-6222 WELL NO. MW -/01
DEVELOPED BY	S. M:+	chel	-	DATE OF	INSTALL.	SHEET 2 OF 3
STARTED DEVEL	0/2/19/	marc	-	COMPLE	TED DEVEL	
STARTED DEVEL.	8/27   16 1	TIME	-	COMPLE	IED DEVEL	. / / DATE TIME
W.L. BEFORE DEV	EL. <u>/.25 /</u> .	8/27/96/ 0845	_	AFTER D	EVEL.	
		ATE TIME				DEPTH DATE TIME
WELL DEPTH: BEF			_	AFTER D	EVEL.	WELL DIA. (ln)
STANDING WATER	COLUMN (FT.)	•		STANDIN	IG WELL VO	LUME ga
SCREEN LENGTH			_	DRII LING	WATER LO	
			-			<u></u> -
	VOLUME	FIELU	D PARAME	TERS	<del></del>	
DATE/TIME	REMOVED	SPEC. COND.	TEMP.	pН	Turbis.ty	REMARKS
	(GALS)	(umhos/cm)	101		ОТНЕВ	
5/20/6 /12:51	325	/ 9	<del>/</del>			
8/27/96 / 1354		690	72.1	8.52		Clear
1400	3 <b>28</b>	7/0	73. 2	8.33	132	برلادها)
1560		730	73.7	.8.21	61	clev
1350	370	730	73.5	8.33	١٩	(lex
1600	380	720	72.2	8.41	19	
V 1601			<del> </del>			Pump Shit-off
8/28/96 10813		<del></del>	<del>                                     </del>			Doeth to with 7. Vo'
						Surged her for 5 minutes with
			<del> </del>		<del></del>	Grafs Par.
0820	·			- C . C		Besin Propert @ 12 5Pm
0821	1,2	580	65.2	9.19	912	Very turdis. ressish brenn
0901	13.5	630	(de,6	8.96	583	Slightly turbis
0911	<u> </u>	630	69.1	9.08	/08	Clavary
0921	37,0	<u>640                                    </u>	69.0	9,07	<u>5^3</u>	Clay
1017	130	690	70.0	8.53	13.2	Pune in rak 1.5 200 - Clear
1034	155	7° d	73.3	8.33	8.0	Clear
1104	180	730	73.2	8.05	9,0	(ky
11/0	185	<u> 7/o</u>	62.8	7.83	918	10weed Purp 5' from button
1130	205	730	73.3	8.18	118	1 Cloudy
		= TOTAL V	OLUME RI	EMOVED	(gal.)	
					•	
DEVELOPMENT ME	ETHOD:					
					<del></del>	<del></del>
	<u> </u>					
			<del></del>	····		<u> </u>
NOTES:		t.				
						•



JOB NAME DEVELOPED BY STARTED DEVEL. W.L. BEFORE DEV WELL DEPTH: BEF STANDING WATER SCREEN LENGTH	DATE EL. / DEPTH DEPTH DECOLUMN (FT.)	TIME / PATE TIME	- - -	AFTER DE	INSTALL. TED DEVEL.		OF <u>3</u>
DATE/TIME	VOLUME REMOVED (GALS)	FIELI SPEC. COND. (umhos/cm)	PARAME TEMP.	рΗ	TUCK: 3.HY	REMARKS	
8/28/96 / 1235		730	73.4	8.25		Cley	
1355						Well Surges W/ PUMP	
1402	3\$5	773	74.8	8.35	975	Toold, possish brow	
1418	375	760	74.5	7.84	23.2	Strandy furby	
1435	390	762	75.2	8.10		clew	
1415	400	750	75.0	8.26	27	Ckey	
1455	405	740	73 3	8.43	32	cley	
/5/1	410	770	73.8	8.23	15.9	(14	
1521	420	780	74.1	8.26		(104/	
/527	425	780	73.9	8.26	13	Clex	
JS30	<del></del>					Pump Shit off	· ·
	<u> </u>						
							:
		= TOTAL V	OLUME R	EMOVED	(gal.) 80	)5	
DEVELOPMENT ME	ETHOD:	į,					



, , , , , , , , , , , , , , , , , , ,	1.1220112
JOB NAME <u>Carktert - SCP</u>	JOB NO. 943-6222 WELL NO. MIN-11R
DEVELOPED BY Stuat M. tchil	DATE OF INSTALL. 2/1/16 SHEET 1 OF 3
STARTED DEVEL. 8/8/96 / 08/3	COMPLETED DEVEL. 8/8/96 _1/552_
DATE TIME	DATE TIME
W.L. BEFORE DEVEL. 5.69 18/1/96 1 0830	AFTER DEVEL. 6.0 18/8/16/1851
DEPTH DATE TIME	DEPTH DATE TIME
WELL DEPTH: BEFORE DEVEL. 57.0 bgs	AFTER DEVEL. 57,065, WELL DIA. (In) 3.5
STANDING WATER COLUMN (FT.) 51.32	STANDING WELL VOLUME 32.0 gal.
SCREEN LENGTH 9.0 feet (Olea Borcholi)	DRILLING WATER LOSS 500 gal.
<u> </u>	
VOLUME FIELD PARAM	ETERS

	VOLUME	FIELD	PARAME	TERS		
DATE/TIME	REMOVED	SPEC. COND.	TEMP.	pН	Tur6: J.17	REMARKS
,	(GALS)	(umhos/cm)	۲۵	(s.u.)	OTHER	
8/8/96/0843	Initial realing	1420	67.5	11.62	40.3	Besin Punens C ~ 2.14 glm
_" 0854	24	628	67.8	11.16	21,5	Water Jamela Clear
0857						Incress Pumping (ele to 2.75 PA
8904	47	553	67.7	10.93	20.0	bush same Clear
0917	82	598	68.4	10.90	8.0	
0920		·	Ĺ	Ĺ		Increm Purpos rak to 3.2
0929	119	OYO	67.7	10.76	7.8	water same Clay
0939	151	712	67.1	10.63	5.93	water Sample (les)
0949	183	751	67.1	<i>p</i> ).√3	5.4	(water Samoi clev
0952			ļ	<u> </u>	<u> </u>	Increw lumeras Cate to 4.0 gla
0959	221	791	67.2	10,27	11,70	Water Sumpe Clear
/009	261	850	66.7	/0.03	4,9	10
1019	301	917	663	9,84	4.8	
1029	341	989	66,8	9.72	4,7	U .
1034	381	1140	66.7.	9.54	3.7	ч
1019	4/21	1170	67.4	9.44	2.8	ıı ı
1059	461	/200	66,2	9.37	1,9	u
/100						Storal Pumling to Empty Getter tan
1138						Besin Pumping C 4.0 gPm
<b>V</b>		= TOTAL V	OLUME R	EMOVED	(gal.)	

DEVELOPMENT METHOD:	Grund for	Sub mersial	Pump -	Approximitely	1 2.5
		(cmove).	Dovelsement	Compales o	u pr
USEPA OVERIJA+ (TCA	- Kaisu),				
			<del></del> ,	<del></del>	
		·- <u>-</u>			
NOTES: Wall is open	Borchole"				



JOB NAME	Cabhit -	SCP	_	JOB NO.	94.	3-6222 WELL NO. MW-11R
DEVELOPED BY	Stunt Mil			DATE OF	INSTALL.	Philip SHEET 2 OF 3
		0473	-	COMPLE	TED DEVEL.	8/8/912 1 /552 DATE TIME
	DATE	TIME	_	•		DATE TIME
W.L. BEFORE DE	VEL. 5,68 / 1	8/8/961 0830		AFTER D	EVEL.	6.0 ( 18/8/961 1551
	DEPTH D	DATE TIME	-			DEPTH DATE TIME
WELL DEPTH: BE	FORE DEVEL.	57.0 695		AFTER D	EVEL. 9	7,065_ WELL DIA. (In) ろ.
STANDING WATE	ER COLUMN (FT.)	51.32		STANDIN	G WELL VOI	
		feet ( open borch	. u )	DRILLING	WATER LO	· · · · · · · · · · · · · · · · · ·
		tal ( of constitution	<u> , , , , , , , , , , , , , , , , , ,</u>			
		<del></del>		<u> </u>		
	VOLUME		PARAME			
DATE/TIME	REMOVED	SPEC. COND.	TEMP.	pΗ	Turbis. Ly	REMARKS
	(GALS)	(umhos/cm)	(O)	(s.u.)	OTHER	·
8/8/96 / 1139	501	1280	70.3	9.58	2.8	Water Samo Cler
1149	5-11	1250	68.0		1.8	•
1159	581	1260	67.4	9,33	2.3	<i>u</i>
1209	621	1290	68.4	9.30	2.1	<u>'</u>
1219	661	1310	67.5	9,25	1.9	
1234	721	137 7	68.2	9117	1.8	u u
1244	801	137 0	68.9	9,13	1.8	
1304	841	1390	68.2	9,10	1.6	tt .
1314	881	1/20	68.7	9,03	1.4	
1324	921	1410	68.4	8.94	1.0	<i>v</i>
1334	961	1430	69.4	8.96	0,9	
/33-/						- Stoped Pumping to Emply With +
1438						Bern Rumeins C = 4.0 gem
1440	968	1480	72.2.	9.12	1.6	Custer Same Cher
1450	1008	1/20	69.8	9.5	1,2	11
1500	1048	1400	69.9	8.48	1.2	· · · · · · · · · · · · · · · · · · ·
1210	1088	1450	71.0	8.96	1.0	<i>u</i>
1520	1128	1470	10.5	8.89	0,9	<i>''</i>
<del></del>		= TOTAL V				



	V V L L L	DLVLLOR	IVILIA	1 1 1 1 1 1 1 1	7 11200	7110		
JOB NAME	Captur -	Scp	_	JOB NO.	943	3-6222 WELL N	o. MW.11K	
DEVELOPED BY	_ Stuar P	ritche"		DATE OF INSTALL. 8/1/96 SHEET 3 OF 3  COMPLETED DEVEL. 8/8/96 1 /552  DATE TIME				
STARTED DEVEL.	8/8/94 1	17843	_	COMPLE	TED DEVEL.	8/8/96 1	1552	
		TIME	-			DATE	TIME	
W.L. BEFORE DEV	/EL. 5,68' /	2880 Luplak		AFTER D	EVEL.	6.01 188/96	1 1551	
	DEPTH D	ATE TIME	-			DEPTH DATE 7	IME	
WELL DEPTH: BEI	FORE DEVEL	57 1 hzs		AFTER D	FVFI 3	57.0 875 WELL D	1A. (In) 3 <	
STANDING WATER	R COLUMN (FT )	SI 22	-		IG WELL VO			
STANDING WATER SCREEN LENGTH	1 2	1 / 10	111					
SCHEEN LENGTH	1,0.40	of COle- Doc	791C)	DHILLING	WATER LO	oss <u>500</u>	⊃ gal.	
	VOLUME	FIFI I	PARAME	TERS				
DATE/TIME	REMOVED	SPEC. COND.	TEMP.		Turbis.ly	REMAI	RKS	
	(GALS)	(umhos/cm)	10 F		STHER'			
8 196 /1530	<del></del>	<u> </u>			NTJ 0.9	1. ) 5		
	1168	1460	70.5	8.93		Water Sanne (	lev	
11 /240	1200	1450	69.4	8.86	0.8	"/		
1552	1256	7130	b/	0.00	0.3		5 Durlipment	
1552	123 2		<del></del>	<del>†                                      </del>		Completed	Deter (F) (2)	
		·		<del>                                     </del>		W/March		
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			1	1	4 12 10			
L	<u> </u>	= TOTAL V	OLUME H	EWOVED	(gal.) 123	56		
•							*	
DEVELOPMENT M	ETHOD:							
5_1							· ·	
			_,	·· <del>····</del>		•	-	
							<del></del>	
NOTEO								
NOTES:		ľ					•	
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			-					7
AN BOL	ME	Calstrit.	Scl	_	JOB NO.	943	6222 WELL NO. MW-14D	
DEVELO	OPED BY	S. M. tchu	IM. Ebner		DATE OF	INSTALL	SHEET / OF 4	
		7/29/96		-	COMPLE	TED DEVEL	7/3,186 / 1054	
		DATE	TIME	-			DATE TIME	
W.L. BE	FORE DEV	/FL / 0 ' /	17/29/96/ 0920		AFTER C	EVEL.	1 1	
	0.1.2.02.		DATE TIME	-	711 12112		DEPTH DATE TIME	
WELL C	COTU, DC	FORE DEVEL.			AFTER C	ים/כו	WELL DIA. (In) 4,0	Ì
				-				l
STAND	NG WATE	R COLUMN (FT.		-	STANDIN	IG WELL VO		}
SCREE	N LENGTH	10 +	ect	_	DRILLING	3 WATER LO	OSS <u>O.O</u> gal.	ĺ
		VOLUME	FIELD	PARAME	TERS			İ
DAT	ЕЛІМЕ	REMOVED	SPEC. COND.	TEMP.	pH	Tudid.ly	REMARKS	1
		(GALS)	(umhos/cm)	65	(s.u.)	OTHER NT		]
=1 10	- /	· · · · · ·	<u> </u>	1	· · ·	N <sub>L</sub> 2		
7/29/90		2 :	0.2.0	7,7	12	( )	Bun Punen Q & 251m	1
	1000	2.0	2380	71.5	12.12	609	Clossy	
	/019	40					Pure rak decreves to A 1,0 gra	
	/02.	12	<del></del>				for 5 montes	
	1043		<del> </del>	<del>-</del>	<del> </del>	<del> </del>	Bun Puning of car of 22591	l
	1046	49	<del></del>			<del> </del>	Well funces Dry	n
<del>'</del>	1306		<del> </del>				Besa Punem C 10 sea	
	1500						@ 1309 Felice (une of the	!
			<del> </del>				0,25 Jpm - Note after 12	
$\neg$			_		, , ,	· · · · · · · · · · · · · · · · · · ·	he well only received 10 feet.	
	13/0	52	3/00	72.8	120	1097		
	1315	54				1037		
	1319	235	2910	71.8	12.20	/013		ĺ
	1322	56	3/19	71,2.	12,24	902	Cloudy - light Cellish brown	ĺ
	1326	57				683		
	1328	57.5					Stor Puncing - Well almist Dry	
_ _	1418		<u> </u>				Strac Well with Surar Bloin for 5	Prin
V	1458		ļ			L	Town Punting @ 4:0-25 319 1	1
			= TOTAL V	OLUME RI	EMOVED	(gal.)	Auk - After x 1 hr well only	1
				•			reloved & feet.	ł
			C	<i>( c .</i>				-
	PMENT M		Consinution				Vije Block	ĺ
1671	amen	+ removed	138 gallons (	- 6.0	vell v.	lumes)		
						<del></del>		l
				·				
						<del></del>		
			· · · · · · · · · · · · · · · · · · ·					
OTES:			p					
OTES:			p				·	



JOB NAME DEVELOPED B	Carbtest Y S. M.t.	- SP Chill (M. Elsner	_				_WELL NO. _SHEET	
STARTED DEV	EL. 7/21/96 DATE	1 /OOJ	-				DATE TIM	
			-	AFTER D	EVEL	DEPTH	/ / DATE TIME	<del></del>
WELL DEPTH:	BEFORE DEVE	L. 38.85		AFTER D	EVEL.		WELL DIA. (	(In) 4,0
STANDING WA	TER COLUMN (	FT.) 37.15	-	STANDIN	G WELL VO	LUME	24.60	ga
	TH		-		WATER LO		0.0	
			_					
	VOLUME		PARAME		<i>T</i>			
DATE/TIME	REMOVED (GALS)	SPEC. COND. (umhos/cm)	TEMP.	pH (s.u.)	TURNITY OTHER NTU		REMARKS	·
7/24/96/1429		2480	69.4		800			
1430		2510	69.2	12.14	924	Voy +	14.7. (0)7.7	brown
1441		2550	70.3	13.44	990	<u> </u>		
1440		2530	70,5	12.12	/ :	Clouly	· lira ress	1.14 - 61 cm
144			<del>                                     </del>		<u> </u>			
142		2580	71.1	12.50				
142		<del>-  </del>	<del> </del>		1050			
142		2620	71,3	12.25	880			
1500		2600	69.4	12.10		Slav		
162		<del></del>		-		Carres	Puncing. Well Cuell Cuita S-	WIMIT DY
102							nctu - Afr	
							aly (clia) 6	
/630		<del></del>					Puran e 1	
/ /65		1650	66.2.	12.04			7.55	2, , ,
163						Well 1	Went Dry	Nok
V						DEMA	to Bitin of	Well 39.30
								:
								·
		= TOTAL V	OLUME R	EMOVED	(gal.)			
PEVELOPMEN	METHOD:	Submers. LC	Pune/	Surge	Hock			-
			·····					
<del></del>	<del></del>	<del></del>						
OTES:								



	<del></del>	DLVLLOI				
JOB NAME		IscP		JOB NO.		MELL NO. WM-14D
DEVELOPED BY	L			DATE OF		SHEET 3 OF 4
STARTED DEVE	L. 1	<u> </u>				
• • • • • • • • • • • • • • • • • • • •	DATE	TIME	-	00 22	.,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	DATE TIME
. WI BEEODE D		1 .		VELED U	EVEL.	
W.C. BEFORE D	EVEL. /	ATE TIME	-	AFTERD	CVLL	/ / DEPTH DATE TIME
WELL DEPTH: B	EFORE DEVEL.		_	AFTER D	EVEL.	WELL DIA. (In)
STANDING WAT	ER COLUMN (FT.)		_	STANDIN	IG WELL VO	LUMEgal.
SCREEN LENGT	ዝ			DRILLING	WATER LO	OSS gal.
	-		_			·
	VOLUME	FIELI	D PARAME	TERS		
DATE/TIME	REMOVED	SPEC. COND.	TEMP.	pН	Turbisty	REMARKS
	(GALS)	(umhos/cm)	(8)	(s.u.)	OTHER	]
7/3/46 / 0900	<u> </u>		T- /-	T	NTS	D.T. w 7.14 feet
1 0917	<del></del>	1664	67.1	12.45	727	Start puring at L 1/2 gg m
0921	<del> </del>	7001	101.1	12:73	7 3 1	DIT.W 10.06 E & 1/2 180
0955	15.0		1	<del>                                     </del>		D.T. W 15 2.1 C 6 1/2 5 Pm
1001	73.0	225.0	69.5	12.60	44.0	D.T.W 17.11 'C L 1/2 38-
/881	<del>-</del>	223.0	1-61.7	1-(85	77.5	-Surge Wet - Pum oft
1015		2/00	69.0	12.57	44.3	Risters Rund & L'/Lgpm
1025		2,00	Ψ,			D.T.U 21.05
1030	1	2520	70.5	/2 66	117	
/032	21.0		1			D.T. W 21.60
1056	33	2910	71.0	12.84	93,1	Well Glows Down Stop Proper
1215						Since Well
1214						Resume Pumpins
1232	43.5					1
1263						D.T.W 38.51 - Well Recovery
W (353						D.T. W 34.75 ~ 0.151m (echaps
7/31/96 0955						D.T. W 6.0
1005	•			<u> </u>		Start Pumping @ n 0.253Pm
1034		1604	70.5	12.57	22.1	·
		= TOTAL V	OLUME R	EMOVED	(gal.)	
<del></del>	· · · · · · · · · · · · · · · · · · ·					
DEVELOPMENT	METHOD:		_ <del></del>			·
	<del></del>					
				<del></del>		<u> </u>
		p	-			
NOTES:						
						•



JOR MAWE	Carlstart		_	JOB NO			WELL N	o. Mu	ayı.
DEVELOPED BY			_	DATE O	F INSTALL.				OF 4
STARTED DEVEL		,	_		ETED DEVEL		-		
		TIME	_				DATE	TIME	
W.L. BEFORE DE	EVEL.	<u> </u>		AFTER (	DEVEL.		1	1	
	DEPTH I	DATE TIME	_				DATE T		
WELL DEPTH: BI				AFTER	DEVEL.		WELL D	IA. (In)	
		)			NG WELL VO		-	` '	gal.
SCREEN LENGTI			_		G WATER LO		•	···	gal.
OOTICEN ECNOTI			_	Dittelle	a which co	,			yaı.
·	VOLUME	FIEL	D PARAMI	ETERS		1		<del></del>	
DATE/TIME	REMOVED	SPEC. COND.			Turbialty	1	REMAR	RKS	
	(GALS)	(umhos/cm)		•	OTHER NTJ				1
7/3,196 /1054	8.0		) <u>-</u>	1	V7.V	750	23,9		
1110	16:0	2120	72 8	12.12	20 2	10,1.00		<del> </del>	
[HH	18.0		1/2	1		D.7. W	34.5-	almost Da	·y
1120	21.0		1				38.5		
						Well F	Recovering		
1,7 34							_	)	
1337		2240	77.8	5.89	17.4	D.T W	28.50 5	fut Pump.	ns c 0.
1330	23.5	1350	74.5	578	10 21	1	<del></del>		
132-		<u> </u>	ļ			D.7 W	32.1	·	
1335		1801	72.2	5.21	4.91	ļ			
1357	25.0	1778	72.8	2.8v	5.02	1			
1343	36.0	9 371	74.1	5.90	5.36			Mh as Pa	
	<del>-</del>	<del> </del>	<u> </u>			8001:3	<u>4r</u>	<del></del>	
	<del> </del>	<del> </del>	<del> </del>	1					
			<u> </u>	<del> </del>	1	1			
	<del> </del>								
			<u> </u>		1	1		:	
							•	•	
		= TOTAL V	OLUME F	EMOVED	(gal.)	138			



JOB NAME () DEVELOPED BY 1/1 STARTED DEVEL. 7/1	ar15tad	<u>+</u>	-	JOB NO.	943.	6222 WELL NO. MW-14 R
STARTED DEVEL 37	62121	<u></u>	-	COMPLE	TED DEVEL	7/2/196/ 1/3
STARTED DEVEL.	2)/46: 1 DATE T	IMF	-	COMPLE	TEO DEVEL.	7/23/97 SHEET [ OF ] 7/23/96/1 /653 DATE TIME
W.L. BEFORE DEVEL	1761	7/221 1435	)		EVEL.	1 1
W.L. BEFORE DEVEL.	DEPTH DA	TE TIME	<u>-</u>	AI ILIIO	_,	DEPTH DATE TIME
WELL DEPTH: BEFOR	RE DEVEL.	640'		AFTER D	EVEL.	WELL DIA. (In) 4
WELL DEPTH: BEFOR STANDING WATER CO SCREEN LENGTH	OLUMN (FT )	1174	•	STANDIN	IG WELL VOI	UME 40.3 gal
SCREENLENGTH		01.		DRILLING	WATER LO	SS () gal
CONCENTERIOR		0		, D1	2 *************************************	gu
•						
V	OLUME	FIELD	PARAME		Turbidity	
	EMOVED	SPEC. COND.			NTU OTHER	REMARKS
	(GALS)	(umhos/cm)	(C)	(s.u.)	OTHER	
7-23/1520 1	00	1011	67.7	8.73	7.11	
7-23/1551	60	1078	66.2	10.23	8.96	
7-23/1622 )	270	1083	66.8	7.56	7,4 <u>7</u>	
7-12/1693	290	1979	66.0		4.55	tank full
7 7 107	2 (0	1105	001)	2.0)	1 -1.5	1011
						·
			<u> </u>	ļ		
<del></del>		· · · · · · · · · · · · · · · · · · ·		<del> </del>		<del></del>
	·					
				ļ		
			<u> </u>	<del> </del>		
				-		4
		= TOTAL V	OLUME B	FMOVED	(gal.) $0.9$	10
<u> </u>	l	- TOTAL V	<u>OCOME 11</u>	LINOTED	(guil)	, w
			- 0			
DEVELOPMENT METH	IOD:	<u>Submersible</u>	2	PUMI	<u> </u>	<u> </u>
pumped x g	Ogal a	- 4 gpm	a. C	- /4	500 (	<u></u>
Then Flow	rate move	10 = 1.5 gr	70 Y	<u> </u>	Jugar	
	101 - 11101	21398	<del></del>			
NOTES:		P				
110160.			•			•
						:





					DRECK		
	SCP Calltal S. M. tchi		_	JOB NO.	CINCTALL	143-6222 WELL NO. MW-15D SHEET / OF 7	
OTABLED DEVE	S. MITCH		-	DATEO	TED DELE	- SILE! / OF /	-
STARTED DEVEL	8/19/9 b /	1054	_	COMPLE	TED DEVEL	8/21/96 / /653 DATE TIME	ł
	DATE	TIME				DATE TIME	
W.L. BEFORE DE	DEPTH D	8/196 1034 ATE TIME	_	AFTER C	EVEL.	9.50 18/22/94 0936 DEPTH DATE TIME	
WELL DEPTH: BI	EFORE DEVEL.	49.9' 695				52. 2' WELL DIA. (In) 4.0	
		44:10				DLUME 29.0 gal.	
	H 2 fe		_			OSS O gal.	
			_				
	VOLUME		D PARAME		<u> </u>		
DATE/TIME	REMOVED (GALS)	SPEC. COND. (umhos/cm)	TEMP.	•	OZHEB Javpiny	REMARKS	
8/11/96/1054						Surse Well With Surse Block	
11					<u> </u>	for 5 minutes	
1140		<u></u>	<u> </u>	<u> </u>		Bis - Purling @ 0.6 gen	
1142	1,2	7330	90.1	12.39	off-scile	Yery L.b. ) - Jan (cd) sh brown	
146	6.0	226.0	80.1	12,35	off-suh		
1150			<u> </u>	<u> </u>		About Pumping 14 to 0.3 s/m	
1151	6,3	23.42	77.1	12.25	316	wet same cloudy	
1154				<u> </u>		Pumping rate 0.5' spm	
1200	10.0	5230	75.1	12.54	645	St.544, L.6.J.	1
P07	12.0	<u> </u>	ļ	ļ		Pur Cut. off	
1226	14,0	2170	78.3	12.51	150	Besin Runging @ 0.8 28m	1
1524	20.4	3173	78.7	12.56	79	Stightly Cloudy	
1540	27.0		<del> </del>	<del> </del> -		Pune Cut. off - Pribama with	51-25 F
	<del> </del>		ļ		ļ	Punc	
¥ 14/0	<del> </del>		<del> </del> -	<del>                                     </del>		Pune not opensu- Depth of	NIGII
9/ b. 100	<del>- </del>	<del> </del>	<del> </del>	<del> </del>		19.9' b,s	
8/20/96/0830	<del></del>	<del></del>	<del> </del> -		<del> </del>	Total Dith of Well - 49.50 16.75 -	
10854	<del></del>		<del> </del>	ļ		Death to with 12.601695	İ
70021						Surse well with surse block for	1
<del></del>	<u>.1</u>	= TOTAL V	OLUME R	EMOVED	(gal.)	2 / 111140	
	socket + conte soll. A Comb with a Surge E	r injection used	to the	o / Surge move at Cu.th a Luell	Proximikly 2' Gru Druilspoon	Ducket   Under injection / Bailer  Distant of Sediment from  who somes be Punp  to Asproximately 222	



IOB NAN	ΛE	SCP Carl	1477	_	JOB NO.	. 94	13-6212 WELL NO. MW-13
DEVELO	PED BY	S. M.tch	ve i l	_	DATE O	F INSTALL.	SHEET 2 OF
TARTE	D DEVEL.	8/19/96	1054	_			
		DATE	TIME	-			DATE TIME
N.L. BEF	ORE DEV	EL.	1 1		AFTER D	DEVEL.	1 1
		DEPTH 1	DATE TIME	-			/ / DEPTH DATE TIME
NELL DE	EPTH: BEF	ORE DEVEL.			AFTER D	DEVEL.	WELL DIA. (In)
		R COLUMN (FT.		_		NG WELL VO	
	LENGTH		/ <del></del>	_			
OUCEN	LENGTH	-		_	DHILLIN	G WATER LO	OSS
		VOLUME	FIELI	D PARAME	TERS	<del> </del>	1
DATE	TIME	REMOVED	SPEC. COND.	TEMP.		Turbisity	REMARKS
		(GALS)	(umhos/cm)		(s.u.)	OTHER NTU	
8/20196	10912		+	<del>- /-</del>	1	NTU	By. Runging C O.S GPM
<u>ت رین را</u> ۱	0913	0,5	3240	71.1	12.10	04-5cm	Vryfulis. Jah rosin brens
	012=	71.0	3540	70.4	12.10	off-sah	Sursay well whice pumping
_	<u> </u>	<u> </u>		1	1		- Yen turbis. Durch radish brow
	0922			1			Pumping rak adjustes to 0.39
	0921	6,0	36 10	70.4	12.75	04-56,6	
	0932	80	3420	72.5	12.65	1069	Turbid - ressist brown
	0946						Surgery well call pumping
	0947	12.5	2830	68.7	12.20	1120	
	0155	14.0					Stor Punning
	1066			ļ	ļ	<u> </u>	Susc Well Wift Durse blown
			<del> </del>	<u> </u>		ļ	for - 8 minutes
	/७/১					ļ	Bish Pumins C 0,5 DPM
- -	1012	15.0	3070	78.3	11/19	/0/2	Tu-6,3
	1015	16.5	3649	62,5	10.00	off sale	Voy tobis - son rewish brown
		.0 _		100	0.50	100	- Adjust flow pate to 0.6 spa
$\dashv$	/025	19,5	2820	\$8.7	9.59	289	Turbis
-	1025	23,0	2690	~~~	9 .	454	Flow rets 0.5 51m
	7 423	43,0					Tubis. Flor ret 0.3 spin
			= TOTAL V	OLUME R	FWOVED	(gai.)	
EVELOF	MENT MI	ETHOD:					
							<del> </del>
				•			
OT==			_				
OTES:			P				•



JOB NAME	SCP Cals	fast		JOB NO.	. 94	13-6222 WELL NO. MW-15D	
DEVELOPED BY	S. Mitch	ıl TIME		DATE O	FINSTALL.	SHEET 3OF 7	
STARTED DEVEL.	1		-				
	DATE	TIME	_			. / DATE TIME	
W.L. BEFORE DEV				AFTER D	DEVEL.	1 _ 1	
	DEPTH C	ATE TIME	-			/ / DEPTH DATE TIME	
WELL DEPTH: BEI					DEVEL.		
STANDING WATER		•	-				
			_				
SCREEN LENGTH		<del></del>	-	DRILLIN	G WATER LO	OSSgal.	
	VOLUME	FIEL I	PARAME	TERS	<del></del>		
DATE/TIME	REMOVED	SPEC. COND.	TEMP.	pH	TUNION	REMARKS	
	(GALS)	(umhos/cm)	SOY	•	OTHER		
8/20/96 //035	26,0	3560	<del></del>				
8/20/16 //035	∠ €,∪	2962	51,0	8.35	10tf-Sur	Sand Very List (Muly)	
<del>-  </del>	<del> </del> -	<del> </del>	<del> </del>		<del> </del>	- Flow (at 0.5 gpm	
/48 7	27.5				<del> </del> -	Store Pumping - flus tos tang	
						for Pung. Use 3" but to	
						Comun Desiment	
1252	42.0					· (comme) 15 galling with back	
						Total Depth of well Now 50.5' bys	
							fluid
					ļ	Well With Potage water	
14/3				<del></del>	<del> </del>		الد
1504				<del></del>	<del> </del>	Combination of flucking + Pumping	いない
730-7					<del> </del>	Stored Purping. Triedis - 50 sally of Caproximally GO gallay - No Water 185	
			<del></del>			1 1 1	TWING
_	50.0	<del> </del>				8 Jelli-7	(7.,00
1577					1	Total Death , & well 50.8163;	
						·	
						· ·	
		= TOTAL V	OLUME RE	MOVED	(gal.)		
EVELOPMENT M	ETHOD:						
PACEOL MICIAL W	LINOU.		<del></del>				
	<del> </del>						
						L L	
IOTES:		P					



OB NAME	SCP Clarkt	.) <del></del>		JOB NO.	943-62	22 WELL NO. Mω-/5D
		11		DATE OF	INSTALL	SHEET 4 OF
TARTER DEVEL	<u> 3. P.Hele</u>	· · · · · · · · · · · · · · · · · · ·	-			
TARTED DEVEL	DATE	TIME	-	COMPLE	TED DEVEL	DATE TIME
				. —		
/.L. BEFORE DE	/EL/	/ DATE TIME	_	AFTERD	EVEL.	1 1
	DEPTH L	DATE TIME				DEPTH DATE TIME
/ELL DEPTH: BE	FORE DEVEL.		_	AFTER D	EVEL.	WELL DIA. (In)
TANDING WATE	R COLUMN (FT.)	•		STANDIN	IG WELL VO	LUME g
CREEN LENGTH			_	DBILLING	3 WATER LO	OSS g
			-			
· · · · · · · · · · · · · · · · · · ·	VOLUME	FIELD	PARAME			
DATE/TIME		SPEC. COND.			Turbis.ty	REMARKS
1	(GALS)	(umhos/cm)	(e)	(s.u.)	OTHER THER	
3/1/96 / 0835			<del></del>	T	T	Total Delft . ( Well 50.7' 655 -
1	<u> </u>		<del> </del>		· · · · · · · · · · · · · · · · · · ·	Dept + wit 9.45' 695
0900	<u> </u>	<del></del>	-			Use Sand burket to common
1			1			SW, next
0932	15					Total Deptr. 1 win 52.2'-all
						Sediming her been Removed
040	33					Total 3" Superish - Surge well
T						to remin drilling fluid - Rund
						18 galling . Pur well to New
						digners
1020	41					Such well with funt. fund
				,		P. O galler
1125						Sunc Can with Sun blow for
						5 minutes . Begin Purply with
	<u> </u>		·	ļ		brundfor 6 014 514
1134	42.0	2850	58.3	7.84	391	Clasy
/137	43.5	2360	60,1	7.64	261	Cloudy
1147	47.5	2810	58.3	7.85	127	Shoutly Cloudy
V 1157	52.5	2138	54.5	8.25	90	Clear
		= TOTAL V	OLUME R	EMOVED	(gal.)	
EVELOPMENT M	ETHOD:					
<del></del>					<del></del>	<del></del>
<del></del>	<del></del>				<del></del>	
	<del></del>					
	•					
·						
OTES:		<u>*</u>				
OTES:		:				



OB NA	AME	SCP Carl	strat.	_			3-6272 WELL NO. Mb-152
DEVEL	OPED BY	S. Mitch	e (	_	DATE O	INSTALL.	SHEET SOF
TART	ED DEVEL.			_			
	•	DATE	TIME	-			/ DATE TIME
			<u></u>		AFTER (	DEVEL.	
.,_,		DEPTH I	DATE TIME	-			DEPTH DATE TIME
VELLE	DEPTH: REF	ORE DEVEL.			AETER I		WELL DIA. (In)
				-			
		COLUMN (FT.	)	-		NG WELL VC	···································
CHEE	N LENGTH			-	DRILLIN	G WATER LO	OSS
				·			
		VOLUME	FIELD	D PARAME	TERS	_	
DAT	ЕЛІМЕ	REMOVED	SPEC. COND.	TEMP.	pН	Turbis.ly	REMARKS
		(GALS)	(umhos/cm)	(G)	<b>(</b> s.u.)	STHER	
8/2, 4	6/1159		<del> </del>	<del>                                     </del>	<del></del>	T ~ 10	Surge Well with surge blake
1	6 1 1131	• • • • • • • • • • • • • • • • • • • •		<u> </u>		<del>                                     </del>	while furting
$\neg \vdash$	1207	57.3	2820	63.8	7,13	175	
	1317	<u> </u>	2920	68.7	7,12	137	Slightly Cloudy.
	1242	67.0	3160	68.4	7,51	31	Clex
	1252	71.0	3410	70.1	7,50	21	Clay
	1302	75.0	3200	71.9	7,28	21	Clear
	1306	76.5					Surse her hit Surs. Bluch
							while punding.
	1312	79.0	3410	72.9	7.53	721	(lov)y
	1322	<u>83 o</u>	3480	74.2	7.52	35	Streety Cloudy
	1332	87.5	3390	74,2	7.49	32	Clex
- -	1342	910	3600	72.5	7.51	13.4	(14
-	<u>Bs</u> ∠	25.0	32.00	70.1	7.44	9.14	Cley
_	1402	99.0	3600	71.8.	7,44	7.21	Clev
	1400		ļ	ļ	<b> </b>	<del> </del>	Surge Well With Surge block
+-			0		<del></del>	1495	Cilile Pumping
<del>\/</del>	1412	/03.0	3350	72.0	7.17_	1087	Punting (sk 0.6 18m.
	1416	104.5			L	<del></del>	1 4 min (ch 0.6 31m
			= TOTAL V	OLUME R	EMOVED	(gal.)	
EVELO	DPMENT ME	THOD:					
		•					
						_ <del></del>	
OTES:			į				
UIES.							· · · · · · · · · · · · · · · · · · ·



DATE OF INSTALL.   SHEET & OF	DEVELOPED BY   S / S   CON     STARTED DEVEL.	TE OF INSTALL.  MPLETED DEVEL.  MPLETED DEVEL.  DATE TIME  J  DEPTH DATE TIME  WELL DIA. (In)  MANDING WELL VOLUME  GRANDING WATER LOSS  GRANDING WATER LOSS  REMARKS  OH Tork. Hy  Port Sk-1-off  Dua Porton Q 0.4 5th  (24 21.4 Clus)  Y3 12.9 Clus  Y3 12.9 Clus  39 7.80 Cles
DATE OF INSTALL.   SHEET   OF	DEVELOPED BY S A HOLD STARTED DEVEL.	TE OF INSTALL.  MPLETED DEVEL.  MPLETED DEVEL.  DATE TIME  J  DEPTH DATE TIME  WELL DIA. (In)  MANDING WELL VOLUME  GRANDING WATER LOSS  GRANDING WATER LOSS  REMARKS  OH Tork. Hy  Port Sk-1-off  Dua Porton Q 0.4 5th  (24 21.4 Clus)  Y3 12.9 Clus  Y3 12.9 Clus  39 7.80 Cles
TARTED DEVEL.	COM-   DATE   TIME     W.L. BEFORE DEVEL.	MPLETED DEVEL.  DATE TIME  J DEPTH DATE TIME  DEPTH DATE TIME  WELL DIA. (In)  ANDING WELL VOLUME  GRANDING WATER LOSS  GRANDING WATER
AFTER DEVEL.     DEPTH DATE TIME	W.L. BEFORE DEVEL.	DEPTH DATE TIME  DEPTH DATE TIME  WELL DIA. (In)  ANDING WELL VOLUME  GRANDING WATER LOSS  GR
DEPTH DATE TIME	DEPTH DATE TIME  WELL DEPTH: BEFORE DEVEL.  STANDING WATER COLUMN (FT.)  SCREEN LENGTH  DATE/TIME REMOVED (GALS)  (GALS)  (Umhos/cm)  (S. 25. 25. 25. 25. 25. 25. 25. 25. 25. 25	DEPTH DATE TIME WELL DIA. (In)  ANDING WELL VOLUME GENERAL SERVICES  REMARKS S.U.) OTHER ATT  POW SA-1-Off DUA COMP. AS POW. (1 US) (2 22.4 CLUX (3 12.9 CLUX (3 12.9 CLUX (3 12.9 CLUX (3 12.9 CLUX (3 12.9 CLUX (4 C
DEPTH DATE TIME	DEPTH DATE TIME  WELL DEPTH: BEFORE DEVEL.  STANDING WATER COLUMN (FT.)  SCREEN LENGTH  DATE/TIME REMOVED (GALS)  (GALS)  (Umhos/cm)  (S. 25. 25. 25. 25. 25. 25. 25. 25. 25. 25	DEPTH DATE TIME WELL DIA. (In)  ANDING WELL VOLUME GENERAL SERVICES  REMARKS S.U.) OTHER ATT  POW SA-1-Off DUA COMP. AS POW. (1 US) (2 22.4 CLUX (3 12.9 CLUX (3 12.9 CLUX (3 12.9 CLUX (3 12.9 CLUX (3 12.9 CLUX (4 C
TANDING WATER COLUMN (FT.)   STANDING WELL VOLUME   CREEN LENGTH   DRILLING WATER LOSS   CREEN LENGTH   REMOVED   SPEC. COND. TEMP. pH   Turk	STANDING WATER COLUMN (FT.)   STANDING WATER COLUMN (FT.)   STANDING WATER COLUMN (FT.)   STANDING WATER COLUMN (FT.)   STANDING WATER COLUMN (FT.)   STANDING WATER COLUMN (FT.)   SPEC. COND.   TEMP.   P.	ANDING WELL VOLUME  ga  ILLING WATER LOSS   GS  OH  Turb. Hy  REMARKS  S.U.) OTHER  Pure shill-off  Dyna Pure ny Q 0.4 sen  (24 31.4 Cluby  (2 32.4 Cluby  (3 12.9 Club  39 9.80 Clear
TANDING WATER COLUMN (FT.)   STANDING WELL VOLUME   CREEN LENGTH   DRILLING WATER LOSS   CREEN LENGTH   REMOVED   SPEC. COND. TEMP. pH   Turk	STANDING WATER COLUMN (FT.)   STA	ANDING WELL VOLUME  ga  ILLING WATER LOSS   GS  OH  Turb. Hy  REMARKS  S.U.) OTHER  Pure shill-off  Dyna Pure ny Q 0.4 sen  (24 31.4 Cluby  (2 32.4 Cluby  (3 12.9 Club  39 9.80 Clear
DRILLING WATER LOSS   CONTINUE   PIELD PARAMETERS   SPEC. COND.   TEMP.   pH   Turkly   REMARKS	DRILE   DRIL	REMARKS  OTHER  POM Shot-off  Dun Pompins Q O. 4 5Pm  (24 21.4 Closs)  (2 22.4 Closs  73 12.9 Closs  39 9.80 Closs
DATE/TIME REMOVED (GALS)  (GALS)  (Umhos/cm)  (SPL)   1/16   1/12   1/17	DATE/TIME REMOVED (GALS) SPEC. COND. TEMP. p (GALS) (umhos/cm) (c) (s.  8/11/16   14/2 \( \)	DH Turbuly REMARKS  S.U.) OTHER  POM Shil-off  Thum Pomping & 0.4 5Pm  (2) Dhy Cloudy  (2) Day Cloudy  (3) 129 Cloud  (4) 129 Cloud  (5) 129 Cloud  (6) 129 Cloud  (7) 129 Cloud  (7) 129 Cloud  (8) 129 Cloud
DATE/TIME REMOVED (GALS)  (GALS)  (Umhos/cm)  (SPL)   1/16   1/12   1/17	DATE/TIME REMOVED (GALS) SPEC. COND. TEMP. p (GALS) (umhos/cm) (c) (s.  8/11/16   14/2 \( \)	DH Turbuly REMARKS  S.U.) OTHER  POM Shil-off  Thum Pomping & 0.4 5Pm  (2) Dhy Cloudy  (2) Day Cloudy  (3) 129 Cloud  (4) 129 Cloud  (5) 129 Cloud  (6) 129 Cloud  (7) 129 Cloud  (7) 129 Cloud  (8) 129 Cloud
DATE/TIME REMOVED (GALS)  (GALS)  (Umhos/cm)  (SPL)   1/16   1/12   1/17	DATE/TIME REMOVED (GALS) SPEC. COND. TEMP. p (GALS) (umhos/cm) (c) (s.  8/11/76   14/2 \( \)	DH Turbuly REMARKS  S.U.) OTHER  POM Shil-off  Thum Pomping & 0.4 5Pm  (2) Dhy Cloudy  (2) Day Cloudy  (3) 129 Cloud  (4) 129 Cloud  (5) 129 Cloud  (6) 129 Cloud  (7) 129 Cloud  (7) 129 Cloud  (8) 129 Cloud
(GALS) (umhos/cm) (G.u.) OTHER NTS    1/16   1/12	(GALS) (umhos/cm) (S. 8/11/16   1425   1530   1530   1530   1530   1540	S.U.) OTHER  POM Shot-off  Thus Pompins Q 0.4 5Pm  121 21.4 (1.4)  12 22.4 (1.4)  13 129 (44)  39 9.80 (1err
	8/11/16 1423 1533 1533 1533 1603 114 1603 118 1380 1603 118 1380 1600 1	Pum sh-1-off  Dun Pumping Q 0.4 sen  121 21.4 Cloudy  12 22.4 Cloud  13 129 Cuc  39 980 Cloud
1530   106.0   1110   51.7   5.21   21.4   Clossy   1573   170   3470   57.4   752   22.4   Clossy   1583   114   3480   553   7.43   12.5   Clossy   1603   118   3590   59.7   7.29   9.80   Clear   1610   120.6   3580   Gc.1   7.41   G.0   Clear   Clossy   Gc.1   7.42   Gc.1   Clossy   Gc.1   7.42   Gc.1   Gc	1530	Dun Pumping Q 0.4 5Pm 124 21.4 Clary 12 22.4 Clar 13 12.9 Clar 39 9.80 Clar
1533   106.0   -16/0   51.2   51.2   51.4   Clary     1543   110   3470   59.4   7.62   52.4   Clary     1553   114   3480   59.7   7.33   12.9   Clary     1603   118   3590   59.7   7.39   9.80   Clary     1600   120.6   3380   60.1   7.41   6.0   Clary     1611	1533   106.0   - 6/0   56.7   5.7	121 21.4 Cluby (2 22.4 Club 13 12.9 Club 39 9.80 Club
1543   110   3470   59.4   7.62   32.4   Clex     1553   114   3480   59.7   7.39   189   Clex     1603   118   3590   59.7   7.39   180   Clex     1610   120.6   3380   Go.1   7.41   G.0   Clex     1611   Punctat in regulate 0.6 1/6     1612   Since letter in the same black on the last of the same black on the last of the same black of the same black of the same black of the same black of the same black of the last of t	1543   110   3470   59.4   7.5   1553   114   3480   59.8   7.5   1603   118   3590   59.7   7.2   1610   120.5   3380   60.1   7.4   1611   1612   125.0   3380   60.0   7.5   1627   131.0   3360   60.0   7.5   1627   131.0   3360   60.0   7.5   1627   131.0   3360   60.0   7.5   1627   131.0   3360   60.0   7.5	12 32.4 Clex 43 12.9 Clex 39 9.80 Clex
1603	1603 118 3590 59.7 7.2 1610 120.5 3380 60.0 7.4 1611 125.0 3380 60.0 7.4 1627 131.0 3360 60.0 7.5	39 9.80 Clear
1603	1610 120.8 3380 601 7.4  1611  1612  1617 125.0 3380 60.0 7.4  1627 131.0 3360 60.0 7.5	39 9.80 Clear
1612	1612 1612 1617 125.0 3380 60.0 7.4 1627 131.0 3360 60.0 7.4	
1612	1612 1617 125.0 3380 60.0 74 1627 131.0 3360 60.0 77	41 6.0 Cleu
1617	1617 125.0 3380 60.0 7.4 1627 131.0 3360 60.0 7.4	Punitat in raid to 0.6 11th
1617	1617 125.0 3380 60.0 7.4 1627 131.0 3360 60.0 7.4	Susc aux with Suge Hown which
1627	1627 131.0 3360 60.3 7.	Pumping well for s' minter
1631   133.5   3350   59.9   7.78   23   Shiphy Cloudy   1636   136.0   3380   60.1   7.50   9.5   Clay   1641   135.0   3360   60.1   7.51   16.9   1614   142.0   3350   51.2   7.78   6.28   Clay   1647   143   -		
1636   136,0   3380   60.1   7.50   9.5   Clev     1641   131.0   3360   60.1   7.52   16.9     1642   142.0   3350   51.2   7.17   628   Clev     1647   143     6.12   Clev     1649   143.5     60.05   Clev     1650   141.0     0.77   Clev		
1641   135.7   3360   6c.1   7.52   16.9   1640   142.0   3350   55.2   7.17   628   C CV   1647   143.5     60.12   C CV   1650   741.0     0.77   C CV   = TOTAL VOLUME REMOVED (gal.)		18 23 Slishly Cloudy
161L   142.0   3350   51.2   7.18   628   C CV     161P   143     6.12   C CV     1619   143.5     6.05   C CV     1650   141.0     0.77   C CV     TOTAL VOLUME REMOVED (gal.)		
161P		
1649 143.5" 60.05 (CCV )   1650 144.0 0.77 (CCV )   TOTAL VOLUME REMOVED (gal.)		
V 1650 141.0 — — 0.77 Clay  = TOTAL VOLUME REMOVED (gal.)	1017 1 1/3	
TOTAL VOLUME REMOVED (gal.)		
	■ TOTAL VOLUME HEMO	OVED (gai.)
	V 1650 141.0	- 0.77 Clay
	NOTES:	
OTES:		



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JOB NAME	Scl (al	falt		JOB NO.	943	3-6272 WELL NO.	NIW-15D
DEVELOPED BY	S.M. tch		_	DATE OF	INSTALL.	SHEET	7 OF 7
STARTED DEVEL.	. /		_			. 8/21/96 / 165	
	DATE	TIME	_			DATE TIM	ΙE
W.L. BEFORE DEV	VEL. /	1		AFTER D	EVEL.	9.50 18/12/961	J936
W.L. BEFORE DEV	DEPTH D	DATE TIME	-			DEPTH DATE TIME	
WELL DEPTH: BE	FORE DEVEL.			AFTER D	EVEL. S	52,2 WELL DIA. (1	n) 4,0
STANDING WATE	R COLUMN (FT.)		<b>-</b>		IG WELL VO		gal.
SCREEN LENGTH			-	DBILLING	3 WATER LO	oss	gal.
			-	DI WEEK I			
						•	
		· · · · · · · · · · · · · · · · · · ·				<del>,</del>	
	VOLUME	FIELD	D PARAME	TERS			[
DATE/TIME	REMOVED	SPEC. COND.		•	Turbis,ty	REMARKS	
	(GALS)	(umhos/cm)	10/	' (s.u.)	OTHER		
8 x 196 / 1651	144.5	_	T -	_	3.74	Clev	
1652	145.0				3.52	Cleur	
1653						Pum-Sh-1.04 De	velolment
						Completed	
<u> </u>			<u> </u>	ļ			
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<del></del>	ļ		J	<u> </u>	00		
	<u> </u>	= TOTAL V	OLUME R	EMOVED	(gal.) $6/6$	12.Ø	
DEVELOPMENT M	IETHOD:	•		ì			
T .	!					÷ .	·
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10:		<del> </del>		<u>-</u>			
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	····			,-			
NOTES:							
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	. 81,196 /		- - -	DATE OF	INSTALL.	6222 WELL NO. MN-16 D  SHEET / OF 3  8/1/16 / 1/428  DATE TIME  8.13 / 13/1/16/1/28  DEPTH DATE TIME
VELL DEPTH: BE	FORE DEVEL.	35,10	_	AFTER D	EVEL.	35,10 WELL DIA. (In) 4,0
STANDING WATE		29.23	_	STANDIN	IG WELL VO	LUME 19.0 gal.
CREEN LENGTH	1 <u>5,0</u>		-	DRILLING	3 WATER LO	gal.
	VOLUME	FIELL	D PARAME	TERS		
DATE/TIME	REMOVED (GALS)	SPEC. COND. (umhos/cm)	TEMP.	pH (s.u.)	Turk: J.Ay OTHER	REMARKS
3/1/96 0948	_	4650	69,0	11.65	off-scale	Julial Reading: Rume rate 110 5 P.
1 0956	7.0	4550	65.3	6.42	282	Web Same Slighty tubis. Colons 1
1002	13.0	2880	65.4	6.46	949	Webs Jart very folds . Tellish brew .
1008	19.0	1990	66.6	6.42	657	WALL SCAPE TURES - FEDDING DERONS
1015	26.0	1730	66,8	6.43	758	1¢
1017	28.0		ļ		<u> </u>	- Stop Purping - Surse Well
			<u> </u>		ļ	all surse block for 5' minter
1030	<u> </u>					Begin Pumlins P 1:0 51m
/031	29,0	2170	70.3	6.44	895	Ver tubio- (cs) so brown
/036	34,5	3/30	67.3	6.43	off-sch	11
1041	39.0	2280	6512	6.19	1010	
1046	44,0	1980	65	6.28	500	Tudes - respect 6 roug
1051	49,0	1890	65.5	6.33	190	Shirth toil
1100	54.0	1820	62.8	6.28	-01	Clea
1100	28.0				<del> </del>	Cuts Surge blow for 5 min e
1133	58.0	2560	73.5	6.56	475	Besin Pumpins @ 1,0 91m
1138	63.0	2920	67.7	15,75	off. Kill	Very turb. 1 - (c) 2:31 61000
1145	68, 0	2360	67.1	6,28	10/0	114 1010 2 - 1000 27 01 000
<del></del>	1	- TOTAL V				
DEVELOPMENT N Surges We	11 a fotal	Submesible of 3 times	Pume /	Surge I	Block	19 Minsky - Burpes a
VOKIA OVUS	~ 205 gell :1h1 (ICE Ka		Mck Agt	ν~() <u>-</u>	SOCULI OF TO	T COMPACE TO FO
				•		



IOD MAA						) RECC			
JOD MAIN	ИE	Carlstast -	scl		JOB NO.	943	-6222	WELL NO.	Mln.1ki
		Stock		-				_	
OTADTE	י בסטו	3/10/1	# S. 67	-	DATEO	יייטואבב.	2/10	_0/1221	<u> </u>
SIARIE	D DEVEL.	8/1/96 /	O SYT	-	COMPLE	TEU DEVEL.	- 81118	_SHEET 	(F
MI DEC	-005 00	ירו יכשהי י	2/15/ 1 45/2		4 ETED D		% in '	101 161 1	lm
W.L. BEr	ORE DE	VEL. 5,87' /	8/1/6 / 0//3	_	AFTERD	EVEL.	0,13 DEBTH	18/, )4/ 1 /	458
		FORE DEVEL.							
				-				_WELL DIA. (	
			29,23	_	STANDIN	G WELL VO		19.0	
SCREEN	LENGTH	_ 5.0		-	DRILLING	WATER LO	SS	0.0	9
		VOLUME	FIELD	D PARAME	TERS				
DATE	TIME	REMOVED	SPEC. COND.	TEMP.	pН	Turb. J.ly		REMARKS	
	,	(GALS)	(umhos/cm)	10 I	(s.u.)	OTHER			
8/196	1148	73.8	1960	66.3	6.39	681	Tub.	, red) as 6	(d.) 0
1	1153	78.0	1840	64.0	6,8	242	Sligati	1 turb.)	
	1158	83,0	18-10	66.5	6.48	13	11		
	1205	১.৪৪	1830	66.3	6,49	73	Class	·	
	1208	93,0	1830	65.7	6,50	61	4		
	1213	98.0	1770	65,6	6,50	48	"/		
┼	1218	/03	1830	66,1	6.51	33			
	12.23	108	1700	66.0	6.49	26	'/		
	1224	109		ļ	-		240107	Jumpin -S	idese hell
+-	1720	<del> </del>	<del> </del>	<del> </del>	<del> </del>			JOSE Block for	
<del></del>	1233 1235	111	1820_	71.1	6.50	58		fumero p 1	. 0 5 (m
<del></del>	1240	116	2100	67.3	6.50	561	CKEN TO	18.2 · (c)3.64	h - 4
$\dashv$	1245	121	1850	67.8	6.51	98 D	10 10	1	· Wro u.a.
$\neg$	1250	126	1720	67.7	6.49	289		relial bo	44
	1255	131	1710	68.6	6,43	113	11	1275.01.01.	-7.71
	1300	136	1780	68.4	6.41	62			
1	1305	141	1990	69.9	6.3-1	46			
	1310	146	1880	70.9	6.31	56	<u> </u>		•
V		1	= TOTAL V	OLUMED	EMOVED	(aal \			



	V V L L L	. DEVELOP	IVI		DILLOC	<u> </u>		
		SCP		JOB NO.	94.	3-6222	_WELL NO.	M6.16D
DEVELOPED BY	Strang	Mitchell		DATE OF	INSTALL.	_	SHEET 3	<u>_</u> OF <i>3</i>
STARTED DEVEL.	81,196 1	0940	-	COMPLE	TED DEVEL.	2118	 L 1 1428	
	DATE	OTYP TIME	-			<u></u>	DATE TIME	<del></del>
W.L. BEFORE DEV	DEDTH D	SINKI OTO	-	AFIERD	EVEL.	DEDTH	18/,/961 ) 178 DATE TIME	7
		35.10'					_WELL DIA. (in)	
STANDING WATER	R COLUMN (FT.)	29,23		STANDIN	IG WELL VO	LUME	19.0	gal.
SCREEN LENGTH	์ ร.ล		-	DRILLING	WATER LO	SS	0,0	oal.
			•					
	VOLUME	1	PARAM	ETERS				
DATE/TIME	REMOVED	SPEC. COND.	TEMP.		Tubis.ly		REMARKS	į
	(GALS)	(umhos/cm)	105	(s.u.)	STHER	1		ŀ
8/196 / 1315	151	1920	71.8		43	l — —		
1320	156	1860	70,9	6.3	37	ļ	<del>-</del>	
	157	1000		1-0.5		Show	Pumpins - Surge	(11)
19:11	1 1 1 1	<del> </del>		†		14.33 S	urs. block for	Zoucidu
1340	· · · · · · · · · · · · · · · · · · ·	·		†			Purping @ 1.0	
1312	159	2010	₹Ø.3	6.40	236	130.5	<u> </u>	<del>-//</del>
1347	164	2140	71.0	6.37	920	Very 1	6 دردلی - د.مار	(4), 0
1352	169	1830	706	6.35	361	1 7 7	910.2 - 1 - 0 213 1 0	7800
1357	174	1790	69.9	6.30	13-/	الدوناك	y 4,6.3 .	-
1402	179	1780	70.5	6.28	95	311771	7 19:0:0	
1407	184	1860	71,0	6,25	62			
1412	189	1500	70.6	6.31	40_			
1421	198	1760	70.3		33			
1426	203	17/0	70.6	6.34	38			
1/28	205			1000		Turas	Pum off	
1,								
			<del></del>					,
-V				1				-
		= TOTAL V	OLUMER	EMOVED	(0al) 204	<u> </u>		
<del></del>	L	101/LL V	OLO.III.		(941.) (4 02		<del></del>	
			-					
DEVELOPMENT M	ETHOD:							
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						- <u>-</u> -		
NOTES:		Ţ,						
						:		
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	VVELI	DEVELOR	IVICIVI	LIEL	ח חבטנ	
JOB NAME	Ca/14.21 - So	<u></u>		JOB NO.	91	13-6222 WELL NO. MW 17D
		S. Mitcher		DATE OF		
STARTED DEVEL	71, 16,	120	-	COMPLE	TED DEVEL	SHEETOF
SIARIED DEVEL	- //16 (9 6/	LIV TIME	-	COMPLE	TEU DEVEL	- 8 19196 / /328 DATE TIME
				. ====== ==	· - · · - ·	11 mg 1 mg/s
V.L. BEFORE DE	VEL. 2.15 /	7/16/96/ 1056 DATE TIME	-	AFIERL	EVEL.	11,72 18 1961 /128 DEPTH DATE TIME
	FORE DEVEL.		_			54.81 WELL DIA. (In) 4,0
STANDING WATE	R COLUMN (FT.)	) <u>52.5</u>	_	STANDIN	NG WELL VO	LUME <u>35</u> gal.
CREEN LENGTH	1 /01	feet		DRILLING	G WATER LO	OSS O gal.
	VOLUME	FIELI	D PARAME	TERS		
DATE/TIME	REMOVED	SPEC. COND.	TEMP.	ρH	Tubishy	REMARKS
	(GALS)	(umhos/cm)	10)	(s.u.)	OTHER	Que 2.4 2.4 4.
7/149 1251	35	1425	165	6.05	700	Punting Rak 2 2.0 5/m  Punked Sty P 505-1-1300
 	1 22	1-11-	" -	1 20,7	1-	10 we fin (Ak , Ce)im Q
	<del></del>		<del> </del>	†	<del> </del>	1301
1340	70	1290	65	6.23	83.6	Purse lak & 0.8 3812
1413	105	30,0	70.3	5.77	314	Pur (sh = 12 3Pm
Sc. tch	DH net		1 - 3 -			
1447	140	28.43	66.7	6.52	54.3	Punc (A 2 1.3 5Pm
1450						Stop Punery - Surse win
						Cuth Surge block for, 2
						10 Minutes
1511			<u>                                     </u>	<u> </u>	ļ	Rejume Pumping
	<u> </u>		<u> </u>	ļ	ļ	Pum landry a 1523 Costante 15
	4	·	ļ	ļ		Pune fan des @ 1527
1	<del> </del>		<del>  </del>			(white 1330 (miss Pane 6")
1543	175	2850	66.6	7.09	183.2	
8/1/96 1515	<del> </del>		<del> </del>	ļ	ļ	Such well for 6 minutes
172-	<del> </del>	<del> </del>	<del> </del>		<del> </del>	With Suize Block
/533	1 , -	2870	72 .	14.29	of(-5/44	Burn Pumerns well CIA 1.058m
1534	/.0	<del></del>	73.4		·	
	1	= TOTAL V	OLUME R	<b>EMOVED</b>	(gai.)	
			ı			•
EVELOPMENT N	METHOD:	Submesish 6	ounce 1:	الارود آ	Block	
	3 1/1100	may (3 1	3 (Well	Volvas		Ispment Conclube as per
	Lt (ICK Ka:			_ ,		
						<del></del>
OTES:		į.				
						. 1
					:	•



			DEVELOP	INITIAL	LIELI	D NEGC	<u> </u>		
JOB NAME Carlyful / SCP					JOB NO. 945-6222 WELL NO. MW. 172				
DEVELOPED BY M. Elsay S. M. Ichel				DATE OF INSTALL. SHEET 2 OF 4					
STARTED DEVEL. 7/16/96 1 /2/8 DATE TIME				-					
		DATE	TIME	-			. / DATE TIME		
		/EL/			AFTER D	EVEL.	1 1		
		DEPTH C	ATE TIME	-	,_,,		DEPTH DATE TIME		
WELLE	PEDTH: BEI				AFTER D	EVEI	WELL DIA. (In)		
WELL DEPTH: BEFORE DEVEL.  STANDING WATER COLUMN (FT.)			-						
				-		IG WELL VO			
SCHEE	N LENGTH			-	DRILLING	3 WATER LO	OSS gal.		
	•								
-		VOLUME	FIELD	PARAME	TERS				
DAT	E/TIME	REMOVED	SPEC. COND.	TEMP.	pН	TU, 6W. 4	REMARKS		
		(GALS)	(umhos/cm)	10 }=	(s.u.)	OTHER			
81.156	1538	5,0	2850	76.8	b.28	04.5614			
1	. 1341	8.0	3/00	79.0	6.21	306	Very tulis . redsish brown		
	1547	14.0	3180	790	6.2	1027	1		
	1553						Pumping (Ak 2 0.7 5/m		
	1554	21,0	318.0	80.0	6.25	1063			
	1600	25.0	3480	80.	6.27	720	·		
	1605	29.0	3293	81.5	6.37	68 0			
	1610	33. 0	3270	79.8	6,42	256	Tordis (cs) 14 brown		
	1620	37. o	2840	78.5	6.18	479	·		
+	1625	41.0	2740	77. ?	6,25	420			
	1627	42.0					Pune Shil-Off - Junge wen		
	<del></del>					(1)	Will Surge Block for 5 Marty		
_	1638	43.0	340	84.7	6,29	628	Cesum Pumpin e 2 0.5 3 Cm		
_	1643	4/3.5	21/0	79.4	6.24	offsich	very tuib ) . result brown		
+	1648	46.0	2810	78.7	626	172 907	Very trail - Cellish brown		
	1653	48.5	2840	78.5	6.21		FACRER IVARIA PARE to & 0-891A		
<del></del>	1658	52.0	2863	79.0	621	886			
<del>-  /</del>	1703 1706	56,0 58.5	2970	77.3	6.27	823	<del>                                     </del>		
	1706	21.5					L		
		1	= TOTAL V	OLUME H	EWOVED	(gai.)			
DEVELO	OPMENT M	ETHOD:				_			
					<del></del>				
				· · · · · · · · · · · · · · · · · · ·	<del></del>				
IOTEO.	•		ŗ						
NOTES:							•		
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	VVL	DEVELO	IVILIAI	1 11	JILOC	J110
JOB NAME	Carblast.	SCP	_	JOB NO.	943	6222 WELL NO. MW-17D
DEVELOPED BY			_			SHEET 3_OF_ <u>//</u>
STARTED DEVEL	7/4/90 1	1218	-			
STARTED DEVEL.	7//6//6 DATE	<u>/=/0</u>	-	OOMII CL	TED DEVEL	DATE TIME
				4 CTCD 0		
W.L. BEFORE DEV	'EL/	ATE TIME	-	AFTER D	EVEL.	/ / DEPTH DATE TIME
WELL DEPTH: BEF						WELL DIA. (In)
STANDING WATER	R COLUMN (FT.)		_	STANDIN	G WELL VO	DLUMEgal.
SCREEN LENGTH				DRILLING	WATER LO	OSS gal.
1	VOLUME	FIELD	PARAME	TERS	<u> </u>	
DATE/TIME	REMOVED	SPEC. COND.	TEMP.		Tub: J.ly	REMARKS
1	(GALS)	(umhos/cm)	10 I	(s.u.)	OTHER	1
8/196/1710		·		,	685	<del>                                     </del>
, , , , , , , , , , , , , , , , , , , ,	62.0	2930 298 <b>0</b>	76.9			
1714	65.0 68.0			6,26		Cloudy
1719		2810	75.8	6.26		C10037
	71.0 74.5	27.40	75.8	6.23	<u>4/13</u> 370	
1727	79,0	2800	75.4	6,24	260	Pune Shut off.
18 9 96 /011	77,0	2000	73.9	0,25	260	Suge wer all suge Block for
1013116/201				-		5 Minutes
1020						Begin Punting C. 1.0 gcm
/025	5.0	28/0	70.2	7.57	365	Cloudy
/03 L	<i>J.</i> O	2070	75.2	_/->./		Adjust Flouren to 0.9510
1035	15,0	2840	69,1	7.77	217	C/0434
1040	19,5	2850	71.0	7.30	126	(10224
1045	23.5	2970	71.5	7.32	128	Closdy
1054	27.5	3)90	73.5	7.29	80	Closdy
1105	36.0	3348	70.1	7.32	108	11
1115	45.0	3017	70.3		77	Slighty (las)7
, 1125	54.0	3010	70.3	6.21	82	:
1155	63.0	3090	70,3	7.12	43	Clear
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# APPENDIX D

Hydrogeologic Testing Procedures, Data, and Results

#### **Hydrologic Testing**

Introduction

Hydrogeologic testing was conducted in accordance with the Final Work Plan Amendment (Work Plan; Golder Associates, 1995) for the 216 Paterson Plank Road Site (Site) in Carlstadt, NJ. Hydrogeologic Testing was performed in all of the wells installed during the Off-Property Investigation (Investigation). Slug tests were performed in wells MW-10D, MW-10R and MW-14D through MW-18D, and packer tests were performed in wells MW-8R, MW-11R and MW-14R. The testing program was performed to provide information regarding the hydraulic conductivity of the till and the bedrock in the vicinity of the site.

This section describes the equipment used, testing procedures, data collection methods, and data analysis procedures. Results and interpretations of the data are contained in Section 4.2 of the report text.

#### **Packer Testing**

Packer Testing Set-up

The packer testing in MW-8R was completed using a double packer assembly with three pressure transducers to monitor hydraulic head conditions above (T1), below (T3) and within each test section (T2). The packer assembly consists of a pair of inflatable rubber cylinders separated by a section of perforated steel pipe. The packer testing in bedrock wells MW-11R and MW-14R were completed using a single packer assembly (the same assembly as described above minus the bottom packer). When the packers are inflated, a test zone within the corehole is isolated hydraulically from the rest of the corehole. Water is then allowed to flow from or into the test zone via the perforated pipe, and under controlled conditions. This is referred to as the "flow" portion of the test. The packer tool was equipped with a downhole shut-in valve to allow an instantaneous change of pressure within the test zone.

The hydraulic heads in the test section, above the top packer and below the bottom packer were monitored using pressure transducers. The pressure transducers were connected to a datalogger which recorded the head values. The heads were recorded every three seconds during early stages of the test when the head in the test zone was changing rapidly. The recording interval was gradually increased to a maximum of thirty minutes.

The length of the test interval ranged from 9.6 feet to 16.0 feet for testing in MW-8R and 10.0 feet for testing in MW-11R and MW-14R.

Borehole Drill Stem Packer Testing Procedures

The general packer testing procedure was conducted as follows:

- Lower the packer assembly to the required depth;
- Start recording the pressure transducer values with the datalogger;
- Inflate the packers using compressed nitrogen;
- Measure the stable water level inside the drill rod (i.e., the potentiometric level of the test zone) and close the shut-in valve;
- Pump water out of the drill rods in preparation for a rising head test;
- Open the shut-in valve allowing water in the aquifer to enter the test section and the drill rods;
- Monitor the change in hydraulic head with time ("flow" testing);
- Close the downhole shut-in valve to initiate the "shut-in recovery" testing;
- When the pressures in the transducers have stabilized to their pre-testing values, stop the datalogger;
- Open the downhole shut-in valve and deflate the packers; and,
- Download the data from the datalogger to a portable computer and insert the data into an Excel spreadsheet for analysis.

#### Packer Testing Analysis Methods

The data obtained from the flow portion of the packer tests were analyzed using the Hvorslev (1951) method (U.S. Department of the Navy, 1982). Hvorslev developed a method for the determination of horizontal hydraulic conductivity using measured values of head difference (y) versus time (t). The methodology of data analysis requires the plotting of head ratio (percentage of head yet to recover,  $y/y_o$ ) on the vertical scale of semi-log paper versus time (t) on the linear horizontal scale. The steps required for the analysis are summarized below. A more detailed description of the analysis method is contained in Hvorslev, 1951.

#### Step 1:

Plot  $y/y_o$  (logarithmic) versus t in a semilogarithmic format. Note:  $y_o$  is the initial head difference and is equal to  $h_o - h$ .

#### Step 2:

Because y, and t are the only variables in the equations, the plot must show a straight line (this is usually between 50 percent and 90 percent recovery). In other words, the straight line portion is the valid part of the readings, and the curved part of the plot may be due to wellbore storage, skin or boundary effects which are not accounted for.

#### Step 3:

Select two points on the straight line portion of the curve and record their coordinates  $(t_1, y_{i1})$  and  $(t_2, y_{i2})$ . Record the other test specific parameters (i.e. well coring radius, test section length, etc.).

#### Step 4:

Use the equation below to calculate the horizontal hydraulic conductivity (K):

$$K = \frac{r_c^2}{2L} \ln \frac{L_e}{R_e} \left[ \frac{\ln \left( \frac{h_1}{h_2} \right)}{\left( t_2 - t_1 \right)} \right] 30.48$$

where:

K = hydraulic conductivity [cm/s]

 $r_c = \text{casing radius [feet]}$ 

 $R_c$  = equivalent radius [feet]

 $L_c = \text{length of screened interval [feet]}$ 

t = time [seconds]

 $h_t = \text{hydraulic head at time t [feet]}$ 

#### Slug Testing

Rising head slug tests were performed on the wells screened in the till and bedrock monitoring well MW-10R. As discussed in Section 3.2 of the report, due to poor quality of bedrock encountered in MW-10R (low rock quality designation (RQD)), the installation of 2"-stainless steel well screen and riser was necessary precluding the use of packer testing at this location. The slug of water for

all tests was removed using a Grundfos RediFlow 2 centrifugal pump. Water removed from the wells was contained in 55-gallon drums and transported to the on-Site 10,000 gallon holding tank for subsequent off-Site disposal.

The water elevations in the wells were measured using an In-Situ SP2000 TROLL transducer/datalogger. The datalogger was programmed to record the water levels in a "logarithmic" method in which the time interval between measurements was very small (0.2 seconds) at the beginning of the test and gradually increased to a maximum time interval of 30 seconds after 5 minutes of recording. Using this recording scheme, sufficient early time data was recorded to capture rapid changes in water levels without collecting excessive late-time data.

The general procedure for slug testing was as follows:

- Measure the static water level was using and electronic water level indicator prior to inserting the datalogger/transducer into the well;
- Place the datalogger/transducer in the well;
- Input the initial static water level into the datalogger/transducer as a reference elevation;
- Insert the pump into the well and turn it on.
- When the pump runs dry, shut the valve at the outlet of the pump, start the datalogger, and shut off the pump;
- When the water level in the well reached the level at the beginning of the test, stop the datalogger; and,
- Download the data from the datalogger using a portable computer and insert the data into an Excel spreadsheet for analysis.

The slug tests were analyzed using the modified Hvorslev (1951) method (U.S. Department of Navy, 1982). Results and interpretations of the data are contained in Section 4.2. A brief description of the analysis method was included in the previous section.

#### REFERENCES

Hvorslev, M.J., 1951, "Time Lag and Soil Permeability in Groundwater Observations", Bulletin 36, U.S. Army Corps of Engineers, Waterways Experiment Station, Vicksburg, Mississippi.

U.S. Department of the Navy, 1982, "Soil Mechanics, Design Manual 7.1," Department of the Navy, Naval Facilities and Engineering Command, Alexandria, Virginia.

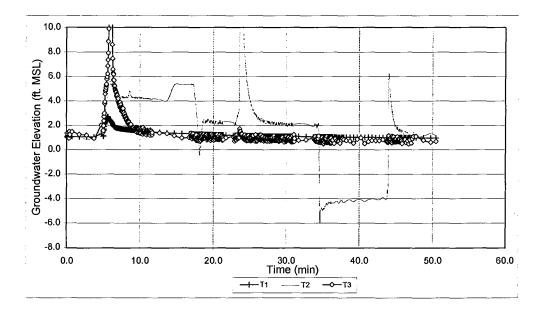
#### WELL MW-8R TEST 1 ARITHMETIC PLOT

#### TEST PARAMETERS

TOP OF INTERVAL	109.72 Ft. BGS
BOTTOM OF INTERVAL	119.32 Ft. BGS
LENGTH OF TEST INTERVAL	9.60 Ft.

INITIAL HYDRAULIC HEAD (H <sub>i</sub> )	1.90 Ft. MSL
HYDRAULIC HEAD AT BEGINNING OF SLUG TEST (Hos)	-5.95 Ft. MSL
MAXIMUM HYDRAULIC HEAD DIFFERENCE (H <sub>i</sub> - H <sub>os</sub> )	7.85 Ft.
HYDRAULIC HEAD AT BEGINNING OF RECOVERY TEST (Hor)	-2.60 Ft. MSL
HYDRAULIC HEAD DIFFERENCE (Hos - Hor)	3.34 Ft.

TEST ELAPSED TIME TO BEGINNING OF SLUG TEST (t; T = 0)	34.63 min.
TEST ELAPSED TIME TO BEGINNING OF RECOVERY TEST (t; T' = 0)	43.93 min.



Project Name: 216 Paterson Plank Road Site, New Jersey

Project No.: 943-6222 Test Date: 7/11/96 Analysis By: Checked By: DSL

Analysis Date:

#### WELL MW-8R TEST 1 **HVORSLEV FLOW PERIOD ANALYSIS**

$$K = \frac{r_c^2}{2L_o} ln \frac{L_o}{R_o} \left[ \frac{ln \left( \frac{h_t}{h_2} \right)}{(t_2 - t_t)} \right] 30.48$$

where:

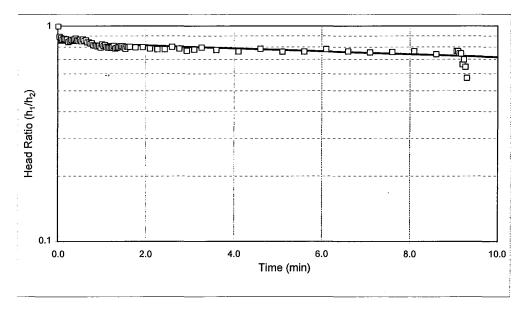
 $r_c$  = casing radius (feet);

 $R_e$  = equivalent radius (feet);

 $L_e$  = length of screened interval (feet);

t = time (seconds); and, $h_t$  = head at time t (feet).

INPUT PARAI	METERS	RESULTS
$r_c =$	0.08	
R <sub>e</sub> =	0.16	
L <sub>e</sub> =	10.00	K= 1.14E-05 cm/sec
$t_1 =$	0.00	K= 3.22E-02 ft/day
t <sub>2</sub> =	10.00	
$h_1/h_0 =$	0.84	
$h_2/h_0 =$	0.72	



Project Name: 216 Paterson Plank Road Site, New Jersey

Project No.: 943-6222

Test Date: 7/11/96

Analysis By:

DSL Checked By:

Analysis Date:

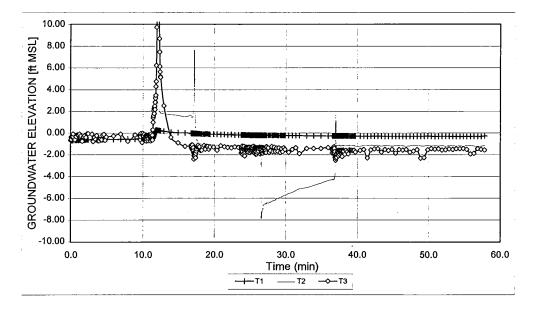
#### WELL MW-8R TEST 2 ARITHMETIC PLOT

#### TEST PARAMETERS

TOP OF INTERVAL	99.32 Ft. BGS
BOTTOM OF INTERVAL	109.32 Ft. BGS
LENGTH OF TEST INTERVAL	10.00 Ft.

INITIAL HYDRAULIC HEAD (H;)	-1.26 Ft. MSL
HYDRAULIC HEAD AT BEGINNING OF SLUG TEST (Hos)	-7.86 Ft. MSL
MAXIMUM HYDRAULIC HEAD DIFFERENCE (H <sub>i</sub> - H <sub>os</sub> )	6.60 Ft.
HYDRAULIC HEAD AT BEGINNING OF RECOVERY TEST (Hor)	-3.85 Ft. MSL
HYDRAULIC HEAD DIFFERENCE (Hos - Hor)	4.01 Ft.

26.60 min. TEST ELAPSED TIME TO BEGINNING OF SLUG TEST (t; T = 0) TEST ELAPSED TIME TO BEGINNING OF RECOVERY TEST (t; T' = 0) 36.87 min.



Project Name: 216 Paterson Plank Road Site, New Jersey

Project No.: 943-6222 Test Date: 7/20/96

Analysis Date:

DSL

Analysis By: Checked By:

## WELL MW-8R TEST 2 HVORSLEV FLOW PERIOD ANALYSIS

$$K = \frac{r_c^2}{2L_o} \ln \frac{L_o}{R_o} \left[ \frac{\ln \left( \frac{h_t}{h_2} \right)}{\left( t_2 - t_1 \right)} \right] 30.48$$

where:

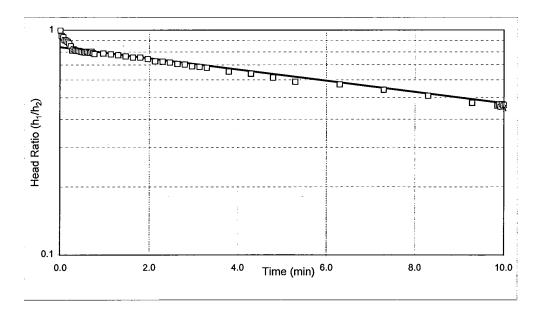
 $r_c$  = casing radius (feet);

 $R_e$  = equivalent radius (feet);

 $L_e$  = length of screened interval (feet);

t = time (seconds); and,  $h_t = \text{head at time } t \text{ (feet)}$ .

INPUT PARAI	METERS	RESULTS
r <sub>c</sub> =	0.08	
R <sub>e</sub> =	0.16	
L <sub>e</sub> =	10.00	K= 4.11E-05 cm/sec
t <sub>1</sub> =	0.00	K= 1.17E-01 ft/day
t <sub>2</sub> =	10.00	
$h_1/h_0 =$	0.84	
$h_2/h_0 =$	0.47	



Project Name: 216 Paterson Plank Road Site, New Jersey

Project No.: 943-6222

Test Date: 7/20/96

Analysis By:

DSL FG

Checked By: Analysis Date:

1/14/97

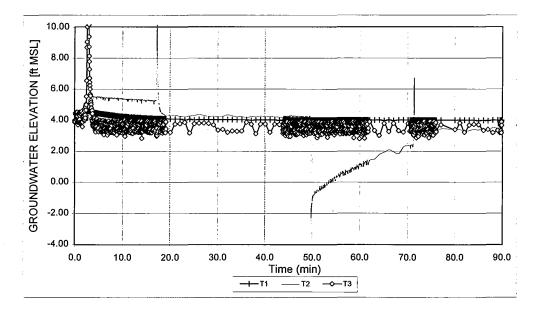
#### WELL MW-8R TEST 3 ARITHMETIC PLOT

#### **TEST PARAMETERS**

TOP OF INTERVAL	89.22 Ft. BGS
BOTTOM OF INTERVAL	98.82 Ft. BGS
LENGTH OF TEST INTERVAL	9.60 Ft.

	1
INITIAL HYDRAULIC HEAD (H <sub>i</sub> )	4.21 Ft. MSL
HYDRAULIC HEAD AT BEGINNING OF SLUG TEST (Hos)	-2.49 Ft. MSL
MAXIMUM HYDRAULIC HEAD DIFFERENCE (H; - Hos)	6.70 Ft.
HYDRAULIC HEAD AT BEGINNING OF RECOVERY TEST (Hor)	2.87 Ft. MSL
HYDRAULIC HEAD DIFFERENCE (Hos - Hor)	5.36 Ft.

TEST ELAPSED TIME TO BEGINNING OF SLUG TEST (t; T = 0)	49.77 min.
TEST ELAPSED TIME TO BEGINNING OF RECOVERY TEST (t; T' = 0)	71.30 min.



Project Name: 216 Paterson Plank Road Site, New Jersey

Project No.: 943-6222 Test Date: 7/11/96

Analysis By:

DSL Checked By: FG

Analysis Date:

1/14/97

## WELL MW-8R TEST 3 **HVORSLEV FLOW PERIOD ANALYSIS**

$$K = \frac{r_o^2}{2L_o} \ln \frac{L_o}{R_o} \left[ \frac{\ln \left( \frac{h_t}{h_2} \right)}{(t_2 - t_1)} \right] 30.48$$

where:

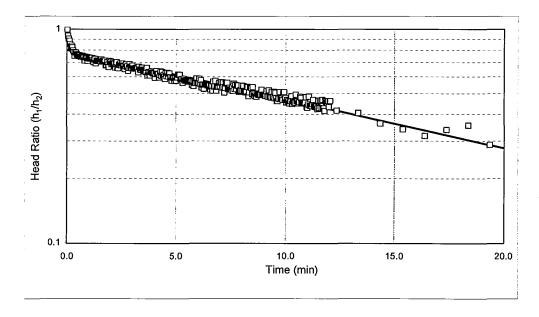
 $r_c$  = casing radius (feet);

 $R_e$  = equivalent radius (feet);

 $L_e$  = length of screened interval (feet);

t = time (seconds); and, $h_t$  = head at time t (feet).

INPUT PARA	METERS	RESULTS
r <sub>c</sub> =	0.08	
R <sub>e</sub> =	0.16	
L <sub>e</sub> =	10.00	K= 3.78E-05 cm/sec
$t_1 =$	0.00	K= 1.07E-01 ft/day
$t_2 =$	20.00	
$h_1/h_0 =$	0.80	
$h_2/h_0 =$	0.28	



Project Name: 216 Paterson Plank Road Site, New Jersey

Project No.: 943-6222

Test Date: 7/11/96

Analysis By:

DSL

Checked By: Analysis Date:

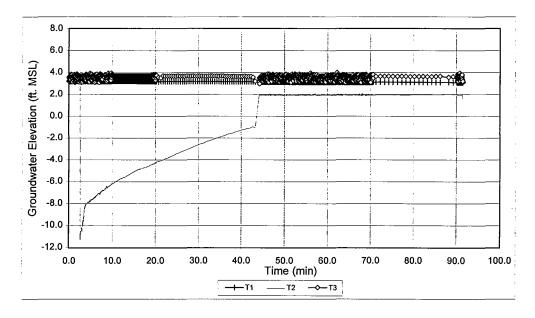
#### WELL MW-8R TEST 4 ARITHMETIC PLOT

#### **TEST PARAMETERS**

TOP OF INTERVAL	104.00 Ft. BGS
BOTTOM OF INTERVAL	113.60 Ft. BGS
LENGTH OF TEST INTERVAL	9.60 Ft.

INITIAL HYDRAULIC HEAD (H;)	3.21 Ft. MSL
HYDRAULIC HEAD AT BEGINNING OF SLUG TEST (Hos)	-11.30 Ft. MSL
MAXIMUM HYDRAULIC HEAD DIFFERENCE (H <sub>i</sub> - H <sub>os</sub> )	14.51 Ft.
HYDRAULIC HEAD AT BEGINNING OF RECOVERY TEST (Hor)	-1.01 Ft. MSL
HYDRAULIC HEAD DIFFERENCE (Hos - Hor)	10.29 Ft.

TEST ELAPSED TIME TO BEGINNING OF SLUG TEST (t; T = 0) 2.60 min.
TEST ELAPSED TIME TO BEGINNING OF RECOVERY TEST (t; T' = 0) 43.27 min.



Project Name: 216 Paterson Plank Road Site, New Jersey

Project No.: 943-6222 Test Date: 7/11/96 Analysis By:

DSL

Checked By: Analysis Date: FG 1/17/97

# WELL MW-8R TEST 4 HVORSLEV FLOW PERIOD ANALYSIS

$$K = \frac{r_c^2}{2L_o} \ln \frac{L_o}{R_o} \left[ \frac{\ln \left(\frac{h_1}{h_2}\right)}{(t_2 - t_1)} \right] 30.48$$

where:

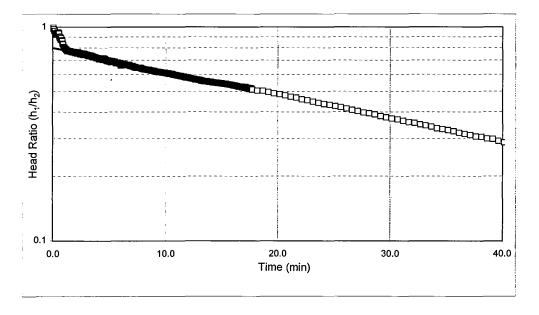
 $r_c$  = casing radius (feet);

 $R_e = \text{equivalent radius (feet)};$ 

 $L_e$  = length of screened interval (feet);

t = time (seconds); and,  $h_t = \text{head at time } t \text{ (feet)}$ .

INPUT PARA	METERS	RESULTS
r <sub>c</sub> =	0.08	
R <sub>e</sub> =	0.16	
L <sub>e</sub> =	10.00	K= 1.79E-05 cm/sec
$t_1 =$	0.00	K= 5.06E-02 ft/day
t <sub>2</sub> =	40.00	-
$h_1/h_0 =$	0.80	
$h_2/h_0 =$	0.29	



Project Name: 216 Paterson Plank Road Site, New Jersey

Project No.: 943-6222

Test Date: 7/11/96

Analysis By:

DSL FG

Checked By: Analysis Date:

1/17/97

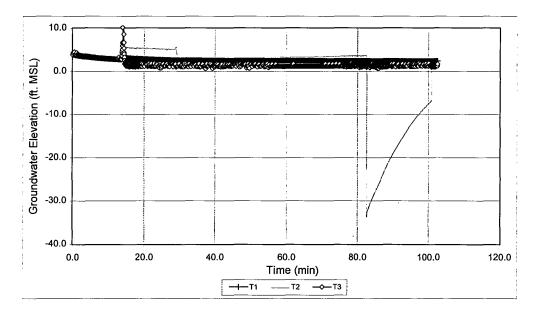
#### WELL MW-8R TEST 5 ARITHMETIC PLOT

#### **TEST PARAMETERS**

•	
TOP OF INTERVAL	114.00 Ft. BGS
BOTTOM OF INTERVAL	130.00 Ft. BGS
LENGTH OF TEST INTERVAL	16.00 Ft.

INITIAL HYDRAULIC HEAD (H <sub>i</sub> )	3.44 Ft. MSL
HYDRAULIC HEAD AT BEGINNING OF SLUG TEST (Hos)	-33.98 Ft. MSL
MAXIMUM HYDRAULIC HEAD DIFFERENCE (H <sub>i</sub> - H <sub>os</sub> )	37.42 Ft.
HYDRAULIC HEAD AT BEGINNING OF RECOVERY TEST (Hor)	9.95 Ft. MSL
HYDRAULIC HEAD DIFFERENCE (Hos - Hor)	43.93 Ft.

TEST ELAPSED TIME TO BEGINNING OF SLUG TEST (t; T = 0) 82.60 min.
TEST ELAPSED TIME TO BEGINNING OF RECOVERY TEST (t; T' = 0) 100.90 min.



Project Name: 216 Paterson Plank Road Site, New Jersey

Project No.: 943-6222 Test Date: 7/11/96 Analysis By: Checked By: Analysis Date:

DSL FG 1/17/97

#### WELL MW-8R TEST 5 **HVORSLEV FLOW PERIOD ANALYSIS**

$$K = \frac{r_{\circ}^{2}}{2L_{\circ}} \ln \frac{L_{\circ}}{R_{\circ}} \left[ \frac{\ln \left( \frac{h_{1}}{h_{2}} \right)}{(t_{2} - t_{1})} \right] 30.48$$

where:

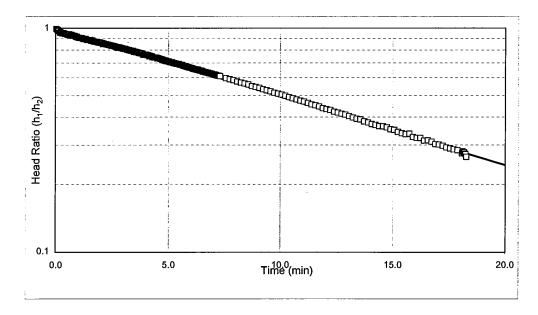
 $r_c$  = casing radius (feet);

 $R_e$  = equivalent radius (feet);

 $L_e$  = length of screened interval (feet);

t = time (seconds); and, $h_t$  = head at time t (feet).

INPUT PARAI	METERS	RESULTS
$r_c =$	0.08	
R <sub>e</sub> =	0.16	
L <sub>e</sub> =	10.00	K= 5.03E-05 cm/sec
$t_1 =$	0.00	K= 1.43E-01 ft/day
$t_2 =$	20.00	
$h_1/h_0 =$	1.00	
$h_2/h_0 =$	0.24	



**Golder Associates** 

Project Name: 216 Paterson Plank Road Site, New Jersey

Project No.: 943-6222

Test Date: 7/11/96

Analysis By:

Checked By:

FG 1/17/97 Analysis Date:

DSL

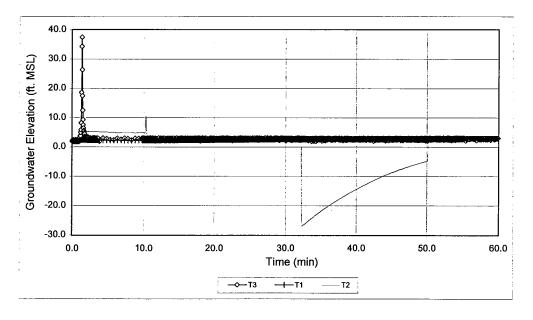
#### WELL MW-8R TEST 6 ARITHMETIC PLOT

#### **TEST PARAMETERS**

TOP OF INTERVAL	89.50 Ft. BGS
BOTTOM OF INTERVAL	99.10 Ft. BGS
LENGTH OF TEST INTERVAL	9.60 Ft.

INITIAL HYDRAULIC HEAD (H <sub>i</sub> )	2.67 Ft. MSL
HYDRAULIC HEAD AT BEGINNING OF SLUG TEST (Hos)	-26.94 Ft. MSL
MAXIMUM HYDRAULIC HEAD DIFFERENCE (H <sub>i</sub> - H <sub>os</sub> )	29.61 Ft.
HYDRAULIC HEAD AT BEGINNING OF RECOVERY TEST (Hor)	-4.32 Ft. MSL
HYDRAULIC HEAD DIFFERENCE (Hos - Hor)	22.62 Ft.
	ł

TEST ELAPSED TIME TO BEGINNING OF SLUG TEST (t; T=0) 32.30 min. TEST ELAPSED TIME TO BEGINNING OF RECOVERY TEST (t; T'=0) 50.10 min.



Project Name: CARLSTADT / COORDINATION / NJ

Project No.: 943-6222 Test Date: 7/20/96 Analysis By:

DSL FG

Checked By: Analysis Date:

1/14/97

#### WELL MW-8R TEST 6 HVORSLEV FLOW PERIOD ANALYSIS

$$K = \frac{r_c^2}{2L_o} \ln \frac{L_o}{R_o} \left[ \frac{\ln \left( \frac{h_t}{h_2} \right)}{(t_2 - t_t)} \right] 30.48$$

where:

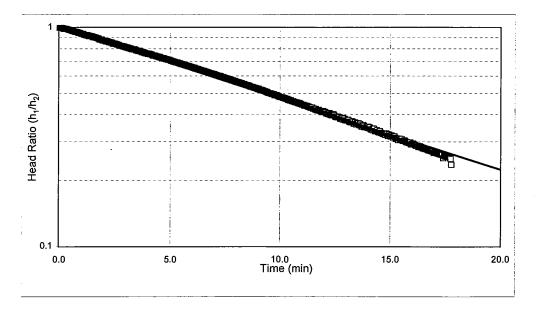
 $r_c$  = casing radius (feet);

 $R_e$  = equivalent radius (feet);

 $L_e$  = length of screened interval (feet);

t = time (seconds); and,  $h_t = \text{head at time } t \text{ (feet)}$ .

INPUT PARAI	METERS	RESULTS
r <sub>c</sub> =	0.08	
R <sub>e</sub> =	0.16	
L <sub>e</sub> =	10.00	K= 5.35E-05 cm/sec
$t_1 =$	0.00	K= 1.52E-01 ft/day
$t_2 =$	20.00	
$h_1/h_0 =$	1.00	
$h_2/h_0 =$	0.22	



Project Name: CARLSTADT / COORDINATION / NJ

Project No.: 943-6222 Test Date: 7/20/96 Analysis By: Checked By: DSL FG

Analysis Date:

1/14/97

### **HVORSLEV SLUG TEST ANALYSIS RISING HEAD TEST MW-10D**

$$K = \frac{r_c^2}{2L_e} \ln \frac{L_e}{R_e} \left[ \frac{\ln \left( \frac{h_1}{h_2} \right)}{(t2 - t1)} \right] 30.48$$

where:

 $r_c$  = casing radius (feet)

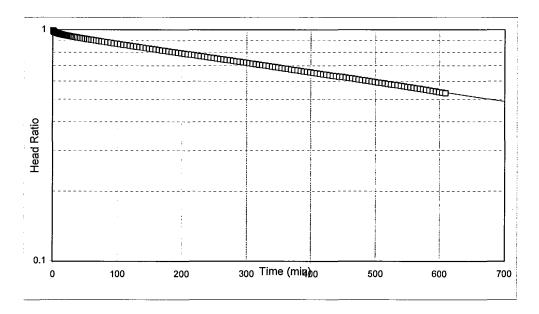
 $R_e$  = equivalent radius (feet)

 $L_e$  = length of screened interval (feet)

t = time (minutes)

 $h_t$  = head at time t (feet)

INPUT PARAM	ETERS		RESULTS
$r_c = 0$	0.17		
$R_{\theta} =$	0.33		
<i>L<sub>e</sub></i> =	6.5	K=	3.19E-06 cm/sec
t <sub>1</sub> =	0	K=	9.06E-03 ft/day
t <sub>2</sub> =	700		•
$h_1/h_0 = 0$	0.98		
$h_2/h_0 = 0$	0.49		



Project Name: 216 Paterson Plank Road Site, New Jersey

Project No.: 943-6222

Test Date: 08/29/96

Analysis By:

SDM FG

Checked By: Analysis Date:

# RISING HEAD TEST MW-10D

WELL NO. MW-10D

DATE INITIAL DEPTH TO WATER CASING DIAMETER SAND DIAMETER SAND DIAMETER TOP OF OPEN INTERVAL BOTTOM OF OPEN INTERVAL SATURATED THICKNESS WATER TABLE TO BOTTOM OF SCREEN EQUIVALENT DIAMETER OPEN INTERVAL LENGTH STATIC IN SCREEN?	8/29/96 10.05 4 8 35.5 42 7.5 31.95 5.51 6.5 N	FEET (btoc) INCHES INCHES FEET (btoc) FEET (btoc) FEET FEET INCHES FEET
STATIC IN SCREEN? MAX. HEAD CHANGE MAX. HEAD IN SCREEN?	N 12.06 N	FEET

ſ	DATE	TIME	EVENT	DEPTH TO	TEST	HEAD	HEAD
			ELAPSED	WATER	ELAPSED		RATIO
-			TIME	5.5	TIME		
	ļ	(HR:M:S)	(MIN)	(FEET)	(MIN)	(FEET)	-
Ì		,				, ,	
Ì	8/29/96	7:52:09	o	22.11		12.06	
	8/29/96	7:52:09	0.005	21.478		11.43	
	8/29/96	7:52:09	0.01	22.325		12.28	
	8/29/96	7:52:09	0.015	21.729		11.68	
	8/29/96	7:52:10	0.02	21.972		11.92	
- {	8/29/96	7:52:10	0.025	22.022		11.97	\ !
	8/29/96	7:52:10	0.03	21.99		11.94	ŀ
	8/29/96	7:52:11	0.035	22.177		12.13	
	8/29/96	7:52:11	0.04	22.087		12.04	
١	8/29/96	7:52:11	0.045	22.131	0.000	12.08	1.00
	8/29/96	7:52:12	0.05	22.103	0.005	12.05	1.00
ì	8/29/96	7:52:12	0.055	22.101	0.010	12.05	1.00
	8/29/96	7:52:12	0.06	22.124	0.015	12.07	1.00
	8/29/96	7:52:12	0.065	22.101	0.020	12.05	1.00
	8/29/96	7:52:13	0.07	22.11	0.025	12.06	1.00
	8/29/96	7:52:13	0.075	22.101	0.030	12.05	1.00
Į	8/29/96	7:52:13	0.08	22.101	0.035	12.05	1.00
	8/29/96	7:52:14	0.085	22.092	0.040	12.04	1.00
Į	8/29/96	7:52:14	0.09	22.099	0.045	12.05	1.00
ł	8/29/96	7:52:14	0.095	22.094	0.050	12.04	1.00
	8/29/96	7:52:15	0.1	22.101	. 0.055	12.05	1.00
	8/29/96	7:52:15	0.1058	22.089	0.061	12.04	1.00
- }	8/29/96	7:52:15	0.112	22.089	0.067	12.04	1.00
	8/29/96	7:52:16	0.1185	22.087	0.074	12.04	1.00
	8/29/96	7:52:16	0.1255	22.085	0.081	12.04	1.00
	8/29/96	7:52:16	0.1328	22.085	0.088	12.04	1.00
	8/29/96	7:52:17	0.1407	22.099	0.096	12.05	1.00
	8/29/96	7:52:17	0.149	22.078	0.104	12.03	1.00
1	8/29/96	7:52:18	0.1578	22.078	0.113	12.03	1.00
	8/29/96	7:52:19	0.1672	22.073	0.122	12.02	1.00
	8/29/96	7:52:19	0.177	22.073	0.132	12.02	1.00
-	8/29/96	7:52:20	0.1875	22.069	0.143	12.02	1.00
- 1	8/29/96	7:52:20	0.1985	22.069	0.154	12.02	1.00
ļ	8/29/96	7:52:21	0.2102	22.066	0.165	12.02	1.00
	8/29/96	7:52:22	0.2227	22.062	0.178	12.01	1.00
	8/29/96	7:52:23	0.2358	22.062	0.191	12.01	1.00
	8/29/96	7:52:23	0.2498	22.057	0.205	12.01	1.00
ı	8/29/96	7:52:24	0.2647	22.052	0.220	12.00	1.00
-	8/29/96	7:52:25	0.2803	22.048	0.235	12.00	0.99

DATE	TIME	EVENT	DEPTH TO	TEST	HEAD	HEAD
		ELAPSED	WATER	ELAPSED		RATIO
		TIME		TIME		
	(HR:M:S)	(MIN)	(FEET)	(MIN)	(FEET)	Agric, De
8/29/96	7:52:26	0.297	22.043	0.252	11.99	0.99
8/29/96	7:52:27	0.3147	22.041	0.270	11.99	0.99
8/29/96	7:52:29	0.3333	22.036	0.288	11.99	0.99
8/29/96	7:52:30	0.3532	22.034	0.308	11.98	0.99
8/29/96	7:52:31	0.3742	22.029	0.329	11.98	0.99
8/29/96	7:52:32	0.3963	22.027	0.351	11.98	0.99
8/29/96	7:52:34	0.4198	22.025	0.375	11.98	0.99
8/29/96	7:52:35	0.4447	22.02	0.400	11.97	0.99
8/29/96	7:52:37	0.4697	22.013	0.425	11.96	0.99
8/29/96	7:52:38	0.4963	22.009	0.451	11.96	0.99
8/29/96	7:52:40	0.5247	22.004	0.480	11.95	0.99
8/29/96	7:52:42	0.5547	21.999	0.510	11.95	0.99
8/29/96	7:52:44	0.5863	21.992	0.541	11.94	0.99
8/29/96	7:52:46	0.6213	21.986	0.576	11.94	0.99
8/29/96	7:52:48	0.658	21.981	0.613	11.93	0.99
8/29/96	7:52:50	0.6963	21.974	0.651	11.92	0.99
8/29/96	7:52:53	0.738	21.969	0.693	11.92	0.99
8/29/96	7:52:55	0.7813	21.965	0.736	11.92	0.99
8/29/96	7:52:58	0.828	21.958	0.783	11.91	0.99
8/29/96	7:53:01	0.8763	21.953	0.831	11.90	0.99
8/29/96	7:53:04	0.928	21.949	0.883	11.90	0.99
8/29/96	7:53:07	0.983	21,944	0.938	11.89	0.99
8/29/96	7:53:11	1.0413	21.937	0.996	11.89	0.99
8/29/96	7:53:15	1.103	21.93	1.058	11.88	0.99
8/29/96	7:53:19	1.168	21.926	1.123	11.88	0.98
8/29/96	7:53:23	1.238	21.919	1.193	11.87	0.98
8/29/96	7:53:27	1.3113	21.914	1.266	11.86	0.98
8/29/96	7:53:32	1.3897	21.907	1.345	11.86	0.98
8/29/96	7:53:37	1.473	21.902	1.428	11.85	0.98
8/29/96	7:53:42	1.5613	21.898	1.516	11.85	0.98
8/29/96	7:53:48	1.6547	21.893	1.610	11.84	0.98
8/29/96	7:53:54	1.753	21.886	1.708	11.84	0.98
8/29/96	7:54:00	1.858	21.882	1.813	11.83	0.98
8/29/96	7:54:07	1.968	21.877	1.923	11.83	0.98
8/29/96	7:54:14	2.0847	21.87	2.040	11.82	0.98
8/29/96	7:54:21	2.2097	21.866	2.165	11.82	0.98
8/29/96	7:54:29	2.3413	21.861	2.296	11.81	0.98
8/29/96	7:54:37	2.4813	21.854	2.436	11.80	0.98
8/29/96	7:54:46	2.6297	21.849	2.585	11.80	0.98
8/29/96	7:54:56	2.7863	21.842	2.741	11.79	0.98
8/29/96	7:55:06	2.953	21.838	2.908	11.79	0.98
8/29/96	7:55:16	3.1297	21.831	3.085	11.78	0.98
8/29/96	7:55:27	3.3163	21.824	3.271	11.77	0.98
8/29/96	7:55:39	3.5147	21.819	3.470	11.77	0.98
8/29/96	7:55:52	3.7247	21.813	3.680	11.76	0.98
8/29/96	7:56:05	3.9463	21.806	3.901	11.76	0.97
8/29/96	7:56:19	4.1813	21.799	4.136	11.75	0.97
8/29/96	7:56:34	4.4297	21.792	4.385	11.74	0.97
8/29/96	7:56:50	4.693	21.783	4.648	11.73	0.97
8/29/96	7:57:07	4.973	21.776	4.928	11.73	0.97
8/29/96	7:57:25	5.2697	21.766	5.225	11.72	0.97
8/29/96	7:57:43	5.583	21.759	5.538	11.71	0.97
8/29/96	7:58:03	5.9147	21.75	5.870	11.70	0.97
8/29/96	7:58:24	6.2663	21.741	6.221	11.69	0.97
8/29/96	7:58:47	6.6397	21.729	6.595	11.68	0.97
8/29/96	7:59:11	7.0347	21.72	6.990	11.67	0.97
5,25,00		1.00-11	21.12	0.000	11.07	0.07

DATE	TIME	EVENT	DEPTH TO	TEST	HEAD	HEAD
1		ELAPSED	WATER	ELAPSED		RATIO
		TIME		TIME		
	(HR:M:S)	(MIN)	(FEET)	(MIN)	(FEET)	
8/29/96	7:59:36	7.453	21.713	7.408	11.66	0.97
8/29/96	8:00:02	7.8963	21.702	7.851	11.65	0.97
8/29/96	8:00:30	8.3663	21.69	8.321	11.64	0.97
8/29/96	8:01:00	8.8647	21.681	8.820	11.63	0.96
8/29/96	8:01:32	9.3913	21.669	9.346	11.62	0.96
8/29/96	8:02:05	9.9497	21.658	9.905	11.61	0.96
8/29/96	8:02:41	10.5413	21.646	10.496	11.60	0.96
8/29/96	8:03:19	11.168	21.633	11.123	11.58	0.96
8/29/96	8:03:58	11.8313	21.619	11.786	11.57	0.96
8/29/96	8:04:41	12.5347	21.605	12.490	11.56	0.96
8/29/96	8:05:25	13.2797	21.591	13.235	11.54	0.96
8/29/96	8:06:13	14.0697	21.575	14.025	11.53	0.96
8/29/96	8:07:03	14.9063	21.561	14.861	11.51	0.95
8/29/96	8:07:56	15.7913	21.543	15.746	11.49	0.95
8/29/96	8:08:52	16.7297	21.529	16.685	11.48	0.95
8/29/96	8:09:52	17.723	21.513	17.678	11.46	0.95
8/29/96	8:10:55	18.7763	21.496	18.731	11.45	0.95
8/29/96	8:12:02	19.8913	21.48	19.846	11.43	0.95
8/29/96	8:13:13	21.073	21.464	21.028	11.41	0.95
8/29/96	8:14:28	22.3247	21.446	22.280	11.40	0.94
8/29/96	8:15:47	23.6497	21.427	23.605	11.38	0.94
8/29/96	8:17:12	25.0547	21.409	25.010	11.36	0.94
8/29/96	8:18:41	26.543	21.386	26.498	11.34	0.94
8/29/96	8:20:16	28.118	21.367	28.073	11.32	0.94
8/29/96	8:21:56	29.7863	21.347	29.741	11.30	0.94
8/29/96	8:23:42	31.5547	21.323	31.510	11.27	0.93
8/29/96	8:25:34	33.428	21.3	33.383	11.25	0.93
8/29/96	8:27:33	35.4113	21.275	35.366	11.23	0.93
8/29/96	8:29:39	37.513	21.247	37.468	11.20	0.93
8/29/96	8:31:53	39.7397	21.22	39.695	11.17	0.93
8/29/96	8:34:14	42.098	21.192	42.053	11.14	0.92
8/29/96	8:36:44	44.5963	21.162	44.551	11.11	0.92
8/29/96	8:39:23	47.243	21.132	47.198	11.08	0.92
8/29/96	8:42:11	50.0463	21.097	50.001	11.05 11.01	0.92 0.91
8/29/96	8:45:09 8:48:18	53.0147 56.1597	21.063 21.028	52.970 56.115	10.98	0.91
8/29/96	8:51:38	59.4913	20.991	59.446	10.98	0.91
8/29/96		63.0197	20.991	62.975	10.94	0.90
8/29/96 8/29/96	8:55:10 8:58:54	66.758	20.952	66.713	10.90	0.90
8/29/96	9:02:52	70.718	20.906	70.673	10.82	0.90
8/29/96	9:02:52	74.9113	20.823	74.866	10.62	0.89
8/29/96	9:11:30	79.3547	20.023	79.310	10.77	0.89
8/29/96	9:16:12	84.0613	20.774	84.016	10.72	0.89
8/29/96	9:21:11	89.0463	20.724	89.001	10.62	0.88
8/29/96	9:26:11	94.0463	20.62	94.001	10.57	0.88
8/29/96	9:31:11	99.0463	20.567	99.001	10.52	0.87
8/29/96	9:36:11	104.0463	20.518	104.001	10.47	0.87
8/29/96	9:41:11	109.0463	20.468	109.001	10.42	0.86
8/29/96	9:46:11	114.0463	20.417	114.001	10.37	0.86
8/29/96	9:51:11	119.0463	20.369	119.001	10.32	0.86
8/29/96	9:56:11	124.0463	20.32	124.001	10.27	0.85
8/29/96	10:01:11	129.0463	20.272	129.001	10.22	0.85
8/29/96	10:06:11	134.0463	20.272	134.001	10.17	0.84
8/29/96	10:00:11	139.0463	20.223	139.001	10.17	0.84
8/29/96	10:16:11	144.0463	20.173	144.001	10.18	0.84
8/29/96	10:21:11	149.0463	20.123	149.001	10.03	0.83
3/23/30	19.61.11	. 70.0700		, -0.001	10.00	0.00

R2-0000456

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RATIO   TIME	DATE	TIME	EVENT	DEPTH TO	TEST	HEAD	HEAD
R/29/96	[ {						RATIO
8/29/96 10:36:11 154.0463 20.032 154.001 9.88 0.83 8/29/96 10:36:11 169.0463 19.986 159.001 9.89 0.82 8/29/96 10:46:11 169.0463 19.987 164.001 9.89 0.82 8/29/96 10:46:11 174.0463 19.845 174.001 9.80 0.81 8/29/96 10:56:11 184.0463 19.851 179.001 9.75 0.81 8/29/96 10:56:11 184.0463 19.801 179.001 9.75 0.80 8/29/96 11:06:11 184.0463 19.753 184.001 9.66 0.80 8/29/96 11:06:11 194.0463 19.663 194.001 9.61 0.80 8/29/96 11:11:11 199.0463 19.673 194.001 9.67 0.80 8/29/96 11:26:11 209.0463 19.577 204.001 9.52 0.79 8/29/96 11:26:11 209.0463 19.577 204.001 9.52 0.79 8/29/96 11:36:11 224.0463 19.48 214.001 9.43 0.78 8/29/96 11:36:11 224.0463 19.48 214.001 9.43 0.78 8/29/96 11:36:11 224.0463 19.48 214.001 9.43 0.78 8/29/96 11:36:11 224.0463 19.48 214.001 9.43 0.78 8/29/96 11:36:11 224.0463 19.37 219.001 9.39 0.78 8/29/96 11:36:11 224.0463 19.347 219.001 9.39 0.78 8/29/96 11:36:11 224.0463 19.347 219.001 9.39 0.78 8/29/96 11:36:11 224.0463 19.347 219.001 9.39 0.78 8/29/96 11:36:11 224.0463 19.349 229.001 9.30 0.77 8/29/96 11:56:11 239.0463 19.349 229.001 9.30 0.77 8/29/96 11:56:11 249.0463 19.247 244.001 9.77 0.76 8/29/96 12:06:11 249.0463 19.217 244.001 9.77 0.76 8/29/96 12:06:11 249.0463 19.217 244.001 9.77 0.76 8/29/96 12:11:11 249.0463 19.217 244.001 9.77 0.76 8/29/96 12:16:11 249.0463 19.03 259.001 9.00 0.75 8/29/96 12:11:11 259.0463 19.088 259.001 9.04 0.75 8/29/96 12:11:11 280.0463 19.008 259.001 8.99 0.75 8/29/96 12:26:11 274.0463 19.008 259.001 8.99 0.75 8/29/96 12:26:11 274.0463 19.008 259.001 8.99 0.75 8/29/96 12:26:11 274.0463 19.008 259.001 8.99 0.75 8/29/96 12:26:11 274.0463 19.008 259.001 8.95 0.74 8/29/96 12:31:11 280.0463 18.566 280.001 8.99 0.75 8/29/96 12:31:11 280.0463 18.566 280.001 8.99 0.75 8/29/96 12:31:11 280.0463 18.567 390.001 8.55 0.74 8/29/96 13:36:11 380.0463 18.568 390.001 8.55 0.70 8/29/96 13:36:11 340.0463 18.569 324.001 8.50 0.70 8/29/96 13:36:11 340.0463 18.569 324.001 8.50 0.70 8/29/96 13:36:11 340.0463 18.569 334.001 8.42 0.68 8/29/96 13:36:11 340.0463 18.569 334.001 8.42 0.68 8/29/96 13:3			TIME		TIME		
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8/29/96 10:41:11 159.0463 19.841 169.001 9.84 0.82 8/29/96 10:56:11 179.0463 19.801 179.001 9.75 0.81 8/29/96 10:56:11 184.0463 19.703 184.001 9.70 0.80 8/29/96 11:06:11 189.0463 19.709 189.001 9.66 0.80 8/29/96 11:06:11 194.0463 19.63 194.001 9.57 0.79 8/29/96 11:11:11 199.0463 19.63 194.001 9.57 0.79 8/29/96 11:21:11 204.0463 19.57 204.001 9.52 0.79 8/29/96 11:21:11 204.0463 19.57 204.001 9.52 0.79 8/29/96 11:26:11 214.0463 19.57 204.001 9.52 0.79 8/29/96 11:26:11 214.0463 19.57 209.001 9.48 0.79 8/29/96 11:31:11 219.0463 19.37 219.001 9.39 0.78 8/29/96 11:36:11 224.0463 19.39 224.001 9.30 0.78 8/29/96 11:36:11 224.0463 19.39 224.001 9.30 0.77 8/29/96 11:46:11 234.0463 19.39 229.001 9.30 0.77 8/29/96 11:56:11 234.0463 19.30 234.001 9.26 0.77 8/29/96 11:51:11 239.0463 19.261 239.001 9.26 0.77 8/29/96 12:06:11 254.0463 19.261 239.001 9.21 0.76 8/29/96 12:06:11 254.0463 19.132 254.001 9.26 0.77 8/29/96 12:06:11 254.0463 19.132 254.001 9.12 0.76 8/29/96 12:06:11 254.0463 19.132 254.001 9.08 0.75 8/29/96 12:16:11 254.0463 19.132 254.001 9.08 0.75 8/29/96 12:16:11 269.0463 19.08 259.001 9.04 0.75 8/29/96 12:16:11 269.0463 19.08 259.001 9.04 0.75 8/29/96 12:16:11 269.0463 19.003 269.001 8.95 0.74 8/29/96 12:26:11 269.0463 19.003 269.001 8.95 0.74 8/29/96 12:26:11 269.0463 19.003 269.001 8.95 0.74 8/29/96 12:26:11 269.0463 19.003 269.001 8.95 0.74 8/29/96 12:36:11 269.0463 18.959 274.001 8.87 0.74 8/29/96 12:36:11 269.0463 18.959 274.001 8.87 0.74 8/29/96 12:36:11 269.0463 18.679 299.001 8.75 0.73 8/29/96 12:36:11 369.0463 18.879 299.001 8.87 0.73 8/29/96 12:36:11 369.0463 18.879 299.001 8.87 0.73 8/29/96 12:36:11 369.0463 18.879 299.001 8.87 0.74 8/29/96 12:36:11 369.0463 18.879 299.001 8.87 0.73 8/29/96 12:36:11 399.0463 18.879 299.001 8.87 0.73 8/29/96 13:36:11 399.0463 18.879 399.001 8.60 0.75 0.73 8/29/96 13:36:11 399.0463 18.879 399.001 8.60 0.75 0.73 8/29/96 13:36:11 399.0463 18.879 399.001 8.60 0.75 0.73 8/29/96 13:36:11 399.0463 18.879 399.001 8.60 0.75 0.73 8/29/96 13:36:11 399.0463 18.879 399.001 8.60 0.75	8/29/96	10:31:11	159.0463	19.986	159.001	9.94	0.82
8/29/96 10:46:11 174.0463 19.801 179.001 9.80 0.81 8/29/96 10:56:11 184.0463 19.753 184.001 9.70 0.80 8/29/96 11:01:11 189.0463 19.753 184.001 9.66 0.80 8/29/96 11:06:11 194.0463 19.663 194.001 9.61 0.80 8/29/96 11:11:11 199.0463 19.671 199.001 9.57 0.79 8/29/96 11:11:11 199.0463 19.57 204.001 9.57 0.79 8/29/96 11:21:11 209.0463 19.57 209.001 9.48 0.79 8/29/96 11:26:11 214.0463 19.48 214.001 9.43 0.78 8/29/96 11:36:11 224.0463 19.48 214.001 9.43 0.78 8/29/96 11:36:11 224.0463 19.48 214.001 9.30 0.78 8/29/96 11:36:11 224.0463 19.48 214.001 9.30 0.77 8/29/96 11:36:11 224.0463 19.349 229.001 9.30 0.77 8/29/96 11:56:11 234.0463 19.349 229.001 9.30 0.77 8/29/96 11:56:11 234.0463 19.247 219.001 9.26 0.77 8/29/96 11:56:11 234.0463 19.247 249.001 9.26 0.77 8/29/96 11:56:11 239.0463 19.20 19.21 0.76 8/29/96 12:06:11 254.0463 19.21 239.001 9.21 0.76 8/29/96 12:06:11 254.0463 19.174 249.001 9.17 0.76 8/29/96 12:06:11 254.0463 19.048 264.001 9.10 0.75 8/29/96 12:26:11 254.0463 19.048 264.001 9.10 0.75 8/29/96 12:26:11 254.0463 19.048 264.001 8.99 0.75 8/29/96 12:26:11 254.0463 19.034 269.001 8.95 0.75 8/29/96 12:26:11 254.0463 19.034 269.001 8.95 0.75 8/29/96 12:26:11 254.0463 19.034 269.001 8.95 0.75 8/29/96 12:26:11 279.0463 18.968 279.001 8.87 0.73 8/29/96 12:26:11 279.0463 18.969 274.001 8.87 0.73 8/29/96 12:26:11 279.0463 18.969 274.001 8.87 0.73 8/29/96 12:26:11 279.0463 18.969 274.001 8.87 0.73 8/29/96 12:26:11 299.0463 18.875 299.001 8.70 0.72 8/29/96 13:26:11 239.0463 18.876 284.001 8.83 0.73 8/29/96 12:26:11 299.0463 18.875 299.001 8.70 0.72 8/29/96 13:26:11 339.0463 18.875 299.001 8.70 0.72 8/29/96 13:26:11 339.0463 18.875 299.001 8.75 0.73 8/29/96 13:26:11 339.0463 18.875 299.001 8.70 0.72 8/29/96 13:26:11 339.0463 18.875 299.001 8.70 0.72 8/29/96 13:26:11 339.0463 18.875 299.001 8.70 0.72 8/29/96 13:26:11 339.0463 18.875 299.001 8.70 0.72 8/29/96 13:26:11 339.0463 18.875 399.001 8.46 0.70 0.72 8/29/96 13:36:11 339.0463 18.879 399.001 8.46 0.70 0.72 8/29/96 13:36:11 339.0463 18.875 399.001 8.46 0.70 0.72 8/29/9	8/29/96	10:36:11	164.0463	19.937	164.001	9.89	0.82
8/29/96 10:56:11 179.0463 19.801 179.001 9.75 0.81 8/29/96 11:06:11 184.0463 19.763 184.001 9.66 0.80 8/29/96 11:06:11 199.0463 19.663 19.4001 9.66 0.80 8/29/96 11:11:11 199.0463 19.663 19.4001 9.57 0.79 8/29/96 11:11:11 199.0463 19.677 204.001 9.52 0.79 8/29/96 11:26:11 204.0463 19.57 204.001 9.52 0.79 8/29/96 11:26:11 204.0463 19.57 204.001 9.48 0.79 8/29/96 11:26:11 214.0463 19.48 214.001 9.43 0.78 8/29/96 11:36:11 214.0463 19.47 214.001 9.43 0.78 8/29/96 11:36:11 224.0463 19.47 219.001 9.39 0.78 8/29/96 11:36:11 229.0463 19.437 219.001 9.39 0.78 8/29/96 11:46:11 224.0463 19.393 224.001 9.30 0.77 8/29/96 11:56:11 234.0463 19.307 234.001 9.26 0.77 8/29/96 11:56:11 234.0463 19.207 234.001 9.26 0.77 8/29/96 11:56:11 234.0463 19.217 244.001 9.17 0.76 8/29/96 12:06:11 244.0463 19.217 244.001 9.17 0.76 8/29/96 12:06:11 254.0463 19.174 249.001 9.12 0.76 8/29/96 12:11:11 259.0463 19.132 254.001 9.08 0.75 8/29/96 12:11:12 259.0463 19.03 259.001 9.04 0.75 8/29/96 12:21:11 259.0463 19.03 259.001 9.04 0.75 8/29/96 12:21:11 259.0463 19.03 259.001 9.04 0.75 8/29/96 12:21:11 259.0463 19.03 259.001 9.04 0.75 8/29/96 12:21:11 259.0463 19.03 259.001 9.04 0.75 8/29/96 12:21:11 259.0463 19.03 259.001 9.04 0.75 8/29/96 12:21:11 259.0463 19.03 259.001 9.04 0.75 8/29/96 12:21:11 259.0463 18.59 274.001 8.91 0.74 8/29/96 12:31:11 279.0463 18.59 274.001 8.91 0.74 8/29/96 12:31:11 279.0463 18.59 274.001 8.91 0.74 8/29/96 12:31:11 279.0463 18.59 274.001 8.91 0.74 8/29/96 12:31:11 239.0463 18.59 274.001 8.87 0.73 8/29/96 13:31:11 399.0463 18.59 399.001 8.50 0.74 8/29/96 13:31:11 399.0463 18.59 399.001 8.79 0.73 8/29/96 13:31:11 399.0463 18.59 399.001 8.79 0.73 8/29/96 13:31:11 399.0463 18.59 399.001 8.50 0.70 8/29/96 13:31:11 399.0463 18.59 399.001 8.50 0.70 8/29/96 13:31:11 399.0463 18.59 399.001 8.50 0.70 8/29/96 13:31:11 399.0463 18.59 399.001 8.50 0.70 8/29/96 13:31:11 399.0463 18.59 399.001 8.50 0.70 8/29/96 13:31:11 399.0463 18.59 399.001 8.50 0.70 8/29/96 13:31:11 399.0463 18.59 399.001 8.50 0.70 8/29/96 13:31:11 399.0463 18.59 3	8/29/96	10:41:11	169.0463	19.891	169.001		0.82
8/29/96 11:06:11 184.0463 19.763 184.001 9.70 0.80 8/29/96 11:06:11 194.0463 19.663 194.001 9.61 0.80 8/29/96 11:11:11 199.0463 19.663 194.001 9.57 0.79 8/29/96 11:26:11 209.0463 19.67 209.001 9.57 0.79 8/29/96 11:26:11 209.0463 19.57 209.001 9.48 0.79 8/29/96 11:26:11 214.0463 19.48 214.001 9.43 0.78 8/29/96 11:36:11 224.0463 19.48 214.001 9.30 0.78 8/29/96 11:36:11 224.0463 19.48 214.001 9.30 0.78 8/29/96 11:36:11 224.0463 19.48 214.001 9.30 0.78 8/29/96 11:36:11 224.0463 19.349 229.001 9.30 0.77 8/29/96 11:41:11 229.0463 19.349 229.001 9.30 0.77 8/29/96 11:46:11 234.0463 19.349 229.001 9.30 0.77 8/29/96 11:56:11 234.0463 19.21 239.001 9.21 0.76 8/29/96 11:56:11 234.0463 19.217 244.001 9.17 0.76 8/29/96 12:06:11 254.0463 19.217 244.001 9.17 0.76 8/29/96 12:06:11 254.0463 19.174 249.001 9.12 0.76 8/29/96 12:06:11 254.0463 19.174 249.001 9.12 0.76 8/29/96 12:06:11 259.0463 19.088 259.001 9.04 0.75 8/29/96 12:11:11 259.0463 19.088 259.001 9.04 0.75 8/29/96 12:26:11 274.0463 19.044 264.001 8.99 0.75 8/29/96 12:26:11 274.0463 18.959 274.001 8.91 0.74 8/29/96 12:26:11 289.0463 18.918 279.001 8.95 0.74 8/29/96 12:36:11 289.0463 18.918 279.001 8.87 0.74 8/29/96 12:36:11 289.0463 18.918 279.001 8.87 0.74 8/29/96 12:36:11 289.0463 18.876 284.001 8.83 0.73 8/29/96 12:36:11 289.0463 18.875 289.001 8.79 0.73 8/29/96 12:36:11 324.0463 18.875 289.001 8.79 0.73 8/29/96 12:36:11 329.0463 18.875 289.001 8.79 0.73 8/29/96 13:36:11 339.0463 18.875 289.001 8.79 0.73 8/29/96 13:36:11 339.0463 18.875 289.001 8.70 0.72 8/29/96 13:36:11 339.0463 18.875 39.001 8.60 0.72 8/29/96 13:36:11 339.0463 18.875 39.001 8.60 0.72 8/29/96 13:36:11 339.0463 18.875 39.001 8.60 0.72 8/29/96 13:36:11 339.0463 18.875 39.001 8.60 0.72 8/29/96 13:36:11 339.0463 18.875 39.001 8.60 0.72 8/29/96 13:36:11 339.0463 18.875 39.001 8.60 0.72 8/29/96 13:36:11 339.0463 18.875 39.001 8.60 0.75 8/29/96 13:36:11 339.0463 18.875 39.001 8.40 0.75 8/29/96 13:36:11 339.0463 18.836 339.001 8.90 0.86 8/29/96 13:36:11 339.0463 18.836 339.001 8.90 0.75 8/29/96 13:36:11 339.	8/29/96	10:46:11	174.0463	19.845	174.001	9.80	
8/29/96 11:01:11 189.0463 19.670 189.001 9.66 0.80 8/29/96 11:01:11 199.0463 19.671 199.001 9.57 0.79 8/29/96 11:16:11 290.0463 19.57 204.001 9.52 0.79 8/29/96 11:21:11 290.0463 19.57 204.001 9.52 0.79 8/29/96 11:21:11 214.0463 19.57 204.001 9.43 0.78 8/29/96 11:23:11 214.0463 19.57 209.001 9.48 0.79 8/29/96 11:31:11 214.0463 19.437 219.001 9.39 0.78 8/29/96 11:36:11 224.0463 19.437 219.001 9.39 0.78 8/29/96 11:46:11 234.0463 19.393 224.001 9.30 0.77 8/29/96 11:46:11 234.0463 19.307 234.001 9.26 0.77 8/29/96 11:56:11 239.0463 19.261 239.001 9.30 0.77 8/29/96 11:56:11 234.0463 19.261 239.001 9.26 0.77 8/29/96 11:56:11 244.0463 19.261 239.001 9.21 0.76 8/29/96 12:01:11 249.0463 19.261 239.001 9.17 0.76 8/29/96 12:01:11 249.0463 19.174 249.001 9.17 0.76 8/29/96 12:01:11 259.0463 19.132 254.001 9.08 0.75 8/29/96 12:11:11 259.0463 19.032 259.001 9.04 0.75 8/29/96 12:11:11 259.0463 19.038 259.001 9.04 0.75 8/29/96 12:21:11 269.0463 19.038 259.001 9.04 0.75 8/29/96 12:21:11 269.0463 19.003 269.001 8.99 0.75 8/29/96 12:21:11 269.0463 19.003 269.001 8.99 0.75 8/29/96 12:21:11 269.0463 18.595 274.001 8.91 0.74 8/29/96 12:31:11 274.0463 18.595 274.001 8.91 0.74 8/29/96 12:31:11 299.0463 18.876 284.001 8.87 0.74 8/29/96 12:31:11 299.0463 18.875 289.001 8.79 0.73 8/29/96 12:31:11 299.0463 18.875 289.001 8.79 0.73 8/29/96 12:31:11 299.0463 18.875 289.001 8.79 0.73 8/29/96 12:31:11 299.0463 18.875 289.001 8.79 0.73 8/29/96 12:31:11 299.0463 18.875 289.001 8.79 0.73 8/29/96 12:31:11 399.0463 18.875 289.001 8.79 0.73 8/29/96 13:31:11 399.0463 18.875 289.001 8.79 0.73 8/29/96 13:31:11 399.0463 18.875 289.001 8.79 0.73 8/29/96 13:31:11 399.0463 18.875 289.001 8.79 0.73 8/29/96 13:31:11 399.0463 18.875 289.001 8.79 0.73 8/29/96 13:31:11 399.0463 18.875 289.001 8.79 0.73 8/29/96 13:31:11 399.0463 18.875 299.001 8.00 0.70 8.60 0.70 8/29/96 13:31:11 399.0463 18.875 399.001 8.60 0.70 8/29/96 13:31:11 399.0463 18.875 399.001 8.50 0.70 8.60 8/29/96 13:31:11 399.0463 18.875 399.001 8.50 0.70 8.20 9.20 9.20 9.20 9.20 9.20 9.20 9.20 9	8/29/96	10:51:11	179.0463	19.801	179.001	9.75	0.81
8/29/96	8/29/96	10:56:11	184.0463	19.753	184.001	9.70	0.80
8/29/96         11:11:11         199.0463         19.617         199.001         9.57         0.79           8/29/96         11:16:11         204.04043         19.57         204.001         9.52         0.79           8/29/96         11:26:11         214.0463         19.48         214.001         9.43         0.78           8/29/96         11:36:11         219.0463         19.393         224.001         9.39         0.78           8/29/96         11:36:11         224.0463         19.393         224.001         9.30         0.77           8/29/96         11:46:11         234.0463         19.349         229.001         9.30         0.77           8/29/96         11:56:11         239.0463         19.261         239.001         9.26         0.77           8/29/96         12:06:11         224.0463         19.217         244.001         9.17         0.76           8/29/96         12:06:11         224.0463         19.217         244.001         9.17         0.76           8/29/96         12:06:11         249.0463         19.17         249.001         9.12         0.76           8/29/96         12:11:11         259.0463         19.088         259.001         9.04	8/29/96	11:01:11	189.0463	19.709	189.001	9.66	
8/29/96         11:16:11         204.0463         19.57         204.001         9.52         0.79           8/29/96         11:26:11         290.0463         19.527         209.001         9.48         0.79           8/29/96         11:36:11         214.0463         19.487         219.001         9.39         0.78           8/29/96         11:36:11         224.0463         19.349         229.001         9.30         0.77           8/29/96         11:46:11         229.0463         19.349         229.001         9.30         0.77           8/29/96         11:51:11         239.0463         19.349         229.001         9.30         0.77           8/29/96         11:56:11         239.0463         19.349         229.001         9.20         0.77           8/29/96         11:56:11         249.0463         19.21         239.001         9.21         0.76           8/29/96         12:06:11         249.0463         19.174         249.001         9.12         0.76           8/29/96         12:16:11         259.0463         19.088         259.001         9.04         0.75           8/29/96         12:21:11         269.0463         19.044         264.001         8.99	8/29/96	11:06:11	194.0463	19.663			
8/29/96         11:21:11         209.0463         19.527         209.001         9.48         0.79           8/29/96         11:26:11         214.0463         19.48         214.001         9.43         0.78           8/29/96         11:36:11         224.0463         19.393         224.001         9.34         0.77           8/29/96         11:41:11         229.0463         19.393         224.001         9.30         0.77           8/29/96         11:46:11         239.0463         19.307         234.001         9.26         0.77           8/29/96         11:56:11         239.0463         19.261         239.001         9.21         0.76           8/29/96         11:56:11         249.0463         19.217         244.001         9.17         0.76           8/29/96         12:06:11         254.0463         19.132         254.001         9.08         0.75           8/29/96         12:16:11         259.0463         19.042         259.001         9.04         0.76           8/29/96         12:16:11         259.0463         19.032         259.001         8.95         0.74           8/29/96         12:31:11         259.0463         19.032         259.001         8.95 <td>8/29/96</td> <td></td> <td>199.0463</td> <td></td> <td></td> <td></td> <td></td>	8/29/96		199.0463				
8/29/96         11:26:11         214.0463         19.48         214.001         9.43         0.78           8/29/96         11:38:11         219.0463         19.393         224.001         9.39         0.78           8/29/96         11:36:11         224.0463         19.393         224.001         9.34         0.77           8/29/96         11:46:11         234.0463         19.307         234.001         9.26         0.77           8/29/96         11:56:11         234.0463         19.307         234.001         9.26         0.77           8/29/96         11:56:11         244.0463         19.217         244.001         9.17         0.76           8/29/96         12:01:11         254.0463         19.174         249.001         9.12         0.76           8/29/96         12:11:11         254.0463         19.042         254.001         9.08         0.75           8/29/96         12:11:11         259.0463         19.082         259.001         8.99         0.75           8/29/96         12:21:11         259.0463         19.093         269.001         8.99         0.74           8/29/96         12:31:11         279.0463         18.918         279.001         8.81 <td>8/29/96</td> <td>11:16:11</td> <td>204.0463</td> <td>19.57</td> <td></td> <td></td> <td></td>	8/29/96	11:16:11	204.0463	19.57			
8/29/96         11:31:11         219.0463         19.437         219.001         9.39         0.78           8/29/96         11:41:11         224.0463         19.349         224.001         9.34         0.77           8/29/96         11:41:11         229.0463         19.349         229.001         9.26         0.77           8/29/96         11:51:11         234.0463         19.307         234.001         9.26         0.77           8/29/96         11:56:11         239.0463         19.217         244.001         9.17         0.76           8/29/96         12:01:11         249.0463         19.174         249.001         9.17         0.76           8/29/96         12:06:11         254.0463         19.132         254.001         9.08         0.75           8/29/96         12:16:11         259.0463         19.032         254.001         9.08         0.75           8/29/96         12:16:11         264.0463         19.042         264.001         8.99         0.75           8/29/96         12:26:11         274.0463         18.959         274.001         8.91         0.74           8/29/96         12:31:11         299.0463         18.876         284.001         8.83 <td>8/29/96</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>	8/29/96						
8/29/96         11:36:11         224.0463         19.393         224.001         9.34         0.77           8/29/96         11:46:11         234.0463         19.349         229.001         9.30         0.77           8/29/96         11:56:11         234.0463         19.307         234.001         9.26         0.77           8/29/96         11:56:11         239.0463         19.261         239.001         9.21         0.76           8/29/96         11:56:11         249.0463         19.217         244.001         9.17         0.76           8/29/96         12:06:11         259.0463         19.132         254.001         9.04         0.75           8/29/96         12:11:11         259.0463         19.088         259.001         9.04         0.75           8/29/96         12:21:11         269.0463         19.03         269.001         8.95         0.74           8/29/96         12:23:11         279.0463         18.959         274.001         8.91         0.74           8/29/96         12:36:11         284.0463         18.876         284.001         8.87         0.74           8/29/96         12:46:11         299.0463         18.878         284.001         8.75 <td>8/29/96</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>	8/29/96						
8/29/96         11:41:11         229.0463         19.349         229.001         9.30         0.77           8/29/96         11:46:11         234.0463         19.307         234.001         9.26         0.76           8/29/96         11:56:11         234.0463         19.261         239.001         9.21         0.76           8/29/96         12:01:11         249.0463         19.174         249.001         9.12         0.76           8/29/96         12:06:11         254.0463         19.174         249.001         9.12         0.76           8/29/96         12:11:11         254.0463         19.042         254.001         9.08         0.75           8/29/96         12:11:11         264.0463         19.044         264.001         8.99         0.75           8/29/96         12:21:11         269.0463         18.909         274.001         8.91         0.74           8/29/96         12:31:11         279.0463         18.878         274.001         8.91         0.74           8/29/96         12:31:11         289.0463         18.878         284.001         8.87         0.74           8/29/96         12:46:11         294.0463         18.795         294.001         8.75 <td>8/29/96</td> <td></td> <td>1</td> <td></td> <td></td> <td></td> <td></td>	8/29/96		1				
8/29/96         11:46:11         234.0463         19.307         234.001         9.26         0.77           8/29/96         11:51:11         239.0463         19.261         239.001         9.21         0.76           8/29/96         11:56:11         244.0463         19.217         244.001         9.17         0.76           8/29/96         12:06:11         254.0463         19.132         254.001         9.08         0.75           8/29/96         12:11:11         259.0463         19.088         259.001         9.04         0.75           8/29/96         12:16:11         254.0463         19.032         269.001         8.99         0.75           8/29/96         12:26:11         274.0463         19.032         269.001         8.95         0.74           8/29/96         12:36:11         274.0463         18.958         274.001         8.91         0.74           8/29/96         12:36:11         274.0463         18.876         284.001         8.83         0.73           8/29/96         12:36:11         284.0463         18.876         284.001         8.83         0.73           8/29/96         12:46:11         294.0463         18.754         299.001         8.75 <td>1</td> <td></td> <td>224.0463</td> <td></td> <td>1 1</td> <td></td> <td></td>	1		224.0463		1 1		
8/29/96         11:51:11         239.0463         19.261         239.001         9.21         0.76           8/29/96         12:01:11         244.0463         19.217         244.001         9.17         0.76           8/29/96         12:06:11         249.0463         19.174         249.001         9.12         0.76           8/29/96         12:11:11         259.0463         19.088         259.001         9.04         0.75           8/29/96         12:16:11         264.0463         19.088         259.001         8.99         0.75           8/29/96         12:21:11         269.0463         19.003         269.001         8.99         0.75           8/29/96         12:26:11         274.0463         18.969         274.001         8.99         0.75           8/29/96         12:36:11         229.0463         18.876         284.001         8.83         0.73           8/29/96         12:36:11         284.0463         18.876         284.001         8.83         0.73           8/29/96         12:46:11         294.0463         18.795         294.001         8.79         0.73           8/29/96         12:56:11         299.0463         18.754         299.001         8.70 <td>8/29/96</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>	8/29/96						
8/29/96         11:56:11         244.0463         19.217         244.001         9.17         0.76           8/29/96         12:01:11         249.0463         19.174         249.001         9.12         0.76           8/29/96         12:11:11         254.0463         19.132         254.001         9.08         0.75           8/29/96         12:16:11         264.0463         19.042         264.001         8.99         0.75           8/29/96         12:26:11         269.0463         19.003         269.001         8.95         0.74           8/29/96         12:31:11         274.0463         18.959         274.001         8.91         0.74           8/29/96         12:31:11         279.0463         18.876         284.001         8.83         0.73           8/29/96         12:36:11         289.0463         18.835         289.001         8.79         0.73           8/29/96         12:36:11         294.0463         18.876         284.001         8.75         0.73           8/29/96         12:46:11         294.0463         18.754         299.001         8.75         0.73           8/29/96         12:56:11         394.0463         18.754         299.001         8.70 <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>							
8/29/96         12:01:11         249.0463         19.174         249.001         9.12         0.76           8/29/96         12:06:11         254.0463         19.132         254.001         9.08         0.75           8/29/96         12:11:11         259.0463         19.088         259.001         8.09         0.75           8/29/96         12:21:11         269.0463         19.003         269.001         8.99         0.75           8/29/96         12:26:11         274.0463         18.959         274.001         8.91         0.74           8/29/96         12:36:11         279.0463         18.918         279.001         8.87         0.74           8/29/96         12:36:11         284.0463         18.876         284.001         8.83         0.73           8/29/96         12:46:11         294.0463         18.795         294.001         8.75         0.73           8/29/96         12:56:11         299.0463         18.754         299.001         8.70         0.72           8/29/96         12:56:11         304.0463         18.712         304.001         8.62         0.71           8/29/96         13:06:11         310.0463         18.671         309.001         8.62 <td>8/29/96</td> <td></td> <td>1</td> <td></td> <td></td> <td></td> <td></td>	8/29/96		1				
8/29/96         12:06:11         254.0463         19.132         254.001         9.08         0.75           8/29/96         12:11:11         259.0463         19.088         259.001         9.04         0.75           8/29/96         12:26:11         264.0463         19.003         269.001         8.99         0.75           8/29/96         12:26:11         269.0463         19.003         269.001         8.91         0.74           8/29/96         12:31:11         279.0463         18.959         274.001         8.91         0.74           8/29/96         12:36:11         284.0463         18.876         284.001         8.83         0.73           8/29/96         12:41:11         289.0463         18.876         284.001         8.79         0.73           8/29/96         12:46:11         299.0463         18.795         294.001         8.75         0.73           8/29/96         12:56:11         309.0463         18.712         304.001         8.66         0.72           8/29/96         13:06:11         309.0463         18.671         309.001         8.62         0.71           8/29/96         13:11:11         319.0463         18.588         319.001         8.54 <td>_</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>	_						
8/29/96         12:11:11         259.0463         19.088         259.001         9.04         0.75           8/29/96         12:16:11         264.0463         19.044         264.001         8.99         0.75           8/29/96         12:21:11         269.0463         19.003         269.001         8.95         0.74           8/29/96         12:26:11         274.0463         18.959         274.001         8.91         0.74           8/29/96         12:36:11         274.0463         18.876         284.001         8.87         0.74           8/29/96         12:46:11         289.0463         18.876         284.001         8.79         0.73           8/29/96         12:46:11         299.0463         18.755         294.001         8.75         0.73           8/29/96         12:56:11         304.0463         18.754         299.001         8.70         0.72           8/29/96         13:01:11         309.0463         18.671         309.001         8.62         0.71           8/29/96         13:01:11         309.0463         18.5671         309.001         8.62         0.71           8/29/96         13:01:11         309.0463         18.569         324.001         8.50 </td <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>							
8/29/96         12:16:11         264.0463         19.044         264.001         8.99         0.75           8/29/96         12:21:11         269.0463         19.003         269.001         8.95         0.74           8/29/96         12:26:11         274.0463         18.959         274.001         8.91         0.74           8/29/96         12:36:11         279.0463         18.876         284.001         8.83         0.73           8/29/96         12:41:11         289.0463         18.876         284.001         8.83         0.73           8/29/96         12:46:11         294.0463         18.755         294.001         8.75         0.73           8/29/96         12:56:11         294.0463         18.754         299.001         8.75         0.73           8/29/96         12:56:11         304.0463         18.754         299.001         8.70         0.72           8/29/96         13:06:11         309.0463         18.629         314.001         8.56         0.71           8/29/96         13:06:11         309.0463         18.581         314.001         8.58         0.71           8/29/96         13:16:11         324.0463         18.584         324.001         8.50 <td>_</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>	_						
8/29/96         12:21:11         269.0463         19.003         269.001         8.95         0.74           8/29/96         12:26:11         274.0463         18.959         274.001         8.91         0.74           8/29/96         12:31:11         279.0463         18.918         279.001         8.87         0.74           8/29/96         12:36:11         284.0463         18.876         284.001         8.83         0.73           8/29/96         12:41:11         289.0463         18.876         284.001         8.79         0.73           8/29/96         12:46:11         294.0463         18.795         294.001         8.75         0.73           8/29/96         12:56:11         304.0463         18.754         299.001         8.70         0.72           8/29/96         13:01:11         309.0463         18.671         309.001         8.66         0.72           8/29/96         13:01:11         319.0463         18.581         314.001         8.58         0.71           8/29/96         13:16:11         324.0463         18.588         319.001         8.54         0.71           8/29/96         13:21:11         329.0463         18.468         334.001         8.42 <td></td> <td></td> <td>I</td> <td></td> <td></td> <td></td> <td></td>			I				
8/29/96         12:26:11         274.0463         18.959         274.001         8.91         0.74           8/29/96         12:31:11         279.0463         18.918         279.001         8.87         0.74           8/29/96         12:36:11         284.0463         18.876         284.001         8.83         0.73           8/29/96         12:41:11         289.0463         18.875         289.001         8.79         0.73           8/29/96         12:51:11         299.0463         18.754         299.001         8.70         0.72           8/29/96         12:56:11         304.0463         18.712         304.001         8.66         0.72           8/29/96         13:01:11         309.0463         18.671         309.001         8.62         0.71           8/29/96         13:06:11         314.0463         18.588         319.001         8.58         0.71           8/29/96         13:16:11         324.0463         18.588         319.001         8.54         0.71           8/29/96         13:26:11         334.0463         18.468         334.001         8.42         0.70           8/29/96         13:31:11         339.0463         18.429         339.001         8.34 <td></td> <td></td> <td></td> <td>1</td> <td>1 1</td> <td></td> <td></td>				1	1 1		
8/29/96         12:31:11         279.0463         18.918         279.001         8.87         0.74           8/29/96         12:36:11         284.0463         18.876         284.001         8.83         0.73           8/29/96         12:41:11         289.0463         18.835         289.001         8.79         0.73           8/29/96         12:46:11         294.0463         18.754         299.001         8.70         0.72           8/29/96         12:56:11         299.0463         18.754         299.001         8.70         0.72           8/29/96         12:56:11         304.0463         18.712         304.001         8.66         0.72           8/29/96         13:01:11         309.0463         18.671         309.001         8.62         0.71           8/29/96         13:06:11         314.0463         18.629         314.001         8.58         0.71           8/29/96         13:11:11         319.0463         18.549         324.001         8.50         0.70           8/29/96         13:26:11         324.0463         18.567         329.001         8.46         0.70           8/29/96         13:26:11         339.0463         18.468         334.001         8.42 <td>1 - 1</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>	1 - 1						
8/29/96         12:36:11         284.0463         18.876         284.001         8.83         0.73           8/29/96         12:41:11         289.0463         18.835         289.001         8.79         0.73           8/29/96         12:46:11         294.0463         18.795         294.001         8.75         0.73           8/29/96         12:51:11         299.0463         18.754         299.001         8.70         0.72           8/29/96         12:56:11         304.0463         18.712         304.001         8.66         0.72           8/29/96         13:06:11         309.0463         18.671         309.001         8.62         0.71           8/29/96         13:11:11         319.0463         18.629         314.001         8.58         0.71           8/29/96         13:11:11         319.0463         18.588         319.001         8.54         0.71           8/29/96         13:21:11         329.0463         18.507         329.001         8.46         0.70           8/29/96         13:31:11         339.0463         18.507         329.001         8.46         0.70           8/29/96         13:31:11         339.0463         18.429         339.001         8.38 <td>_</td> <td></td> <td></td> <td></td> <td>1</td> <td></td> <td></td>	_				1		
8/29/96         12:41:11         289.0463         18.835         289.001         8.79         0.73           8/29/96         12:46:11         294.0463         18.795         294.001         8.75         0.73           8/29/96         12:51:11         299.0463         18.754         299.001         8.70         0.72           8/29/96         12:56:11         304.0463         18.712         304.001         8.66         0.72           8/29/96         13:06:11         309.0463         18.671         309.001         8.62         0.71           8/29/96         13:06:11         314.0463         18.629         314.001         8.58         0.71           8/29/96         13:11:11         319.0463         18.588         319.001         8.54         0.71           8/29/96         13:21:11         329.0463         18.549         324.001         8.50         0.70           8/29/96         13:26:11         334.0463         18.468         334.001         8.42         0.70           8/29/96         13:36:11         344.0463         18.387         344.001         8.34         0.69           8/29/96         13:36:11         344.0463         18.387         344.001         8.34 <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>							
8/29/96         12:46:11         294.0463         18.795         294.001         8.75         0.73           8/29/96         12:51:11         299.0463         18.754         299.001         8.70         0.72           8/29/96         12:56:11         304.0463         18.712         304.001         8.66         0.72           8/29/96         13:01:11         309.0463         18.671         309.001         8.62         0.71           8/29/96         13:01:11         314.0463         18.588         319.001         8.58         0.71           8/29/96         13:11:11         319.0463         18.549         324.001         8.50         0.70           8/29/96         13:26:11         324.0463         18.549         324.001         8.46         0.70           8/29/96         13:26:11         334.0463         18.468         334.001         8.42         0.70           8/29/96         13:31:11         339.0463         18.387         344.001         8.38         0.69           8/29/96         13:41:11         349.0463         18.387         344.001         8.34         0.69           8/29/96         13:41:11         349.0463         18.387         344.001         8.34 <td>_</td> <td></td> <td>J.</td> <td></td> <td></td> <td></td> <td></td>	_		J.				
8/29/96         12:51:11         299.0463         18.754         299.001         8.70         0.72           8/29/96         12:56:11         304.0463         18.712         304.001         8.66         0.72           8/29/96         13:01:11         309.0463         18.671         309.001         8.62         0.71           8/29/96         13:06:11         314.0463         18.629         314.001         8.58         0.71           8/29/96         13:11:11         319.0463         18.588         319.001         8.54         0.71           8/29/96         13:16:11         329.0463         18.549         324.001         8.50         0.70           8/29/96         13:26:11         329.0463         18.507         329.001         8.46         0.70           8/29/96         13:36:11         334.0463         18.468         334.001         8.42         0.70           8/29/96         13:36:11         344.0463         18.387         344.001         8.38         0.69           8/29/96         13:46:11         354.0463         18.387         344.001         8.34         0.69           8/29/96         13:51:11         359.0463         18.267         359.001         8.22 <td>1 1</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>	1 1						
8/29/96         12:56:11         304.0463         18.712         304.001         8.66         0.72           8/29/96         13:01:11         309.0463         18.671         309.001         8.62         0.71           8/29/96         13:06:11         314.0463         18.629         314.001         8.58         0.71           8/29/96         13:11:11         319.0463         18.588         319.001         8.54         0.71           8/29/96         13:16:11         324.0463         18.549         324.001         8.50         0.70           8/29/96         13:26:11         329.0463         18.507         329.001         8.46         0.70           8/29/96         13:26:11         334.0463         18.468         334.001         8.42         0.70           8/29/96         13:36:11         344.0463         18.387         344.001         8.38         0.69           8/29/96         13:36:11         349.0463         18.387         344.001         8.34         0.69           8/29/96         13:46:11         354.0463         18.387         344.001         8.30         0.69           8/29/96         13:51:11         359.0463         18.23         364.001         8.26 <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>							
8/29/96         13:01:11         309.0463         18.671         309.001         8.62         0.71           8/29/96         13:06:11         314.0463         18.629         314.001         8.58         0.71           8/29/96         13:11:11         319.0463         18.588         319.001         8.54         0.71           8/29/96         13:16:11         324.0463         18.549         324.001         8.50         0.70           8/29/96         13:21:11         329.0463         18.507         329.001         8.46         0.70           8/29/96         13:26:11         334.0463         18.468         334.001         8.42         0.70           8/29/96         13:31:11         339.0463         18.429         339.001         8.38         0.69           8/29/96         13:36:11         344.0463         18.387         344.001         8.34         0.69           8/29/96         13:41:11         349.0463         18.348         349.001         8.30         0.69           8/29/96         13:55:11         359.0463         18.267         359.001         8.22         0.68           8/29/96         14:06:11         364.0463         18.191         369.001         8.14 <td>_</td> <td></td> <td>l</td> <td>1</td> <td></td> <td></td> <td></td>	_		l	1			
8/29/96         13:06:11         314.0463         18.629         314.001         8.58         0.71           8/29/96         13:11:11         319.0463         18.588         319.001         8.54         0.71           8/29/96         13:16:11         324.0463         18.549         324.001         8.50         0.70           8/29/96         13:21:11         329.0463         18.507         329.001         8.46         0.70           8/29/96         13:26:11         334.0463         18.468         334.001         8.42         0.70           8/29/96         13:31:11         339.0463         18.429         339.001         8.38         0.69           8/29/96         13:36:11         344.0463         18.387         344.001         8.34         0.69           8/29/96         13:41:11         349.0463         18.388         349.001         8.30         0.69           8/29/96         13:51:11         354.0463         18.36         354.001         8.26         0.68           8/29/96         13:55:11         364.0463         18.23         364.001         8.18         0.68           8/29/96         14:06:11         374.0463         18.152         374.001         8.07	1 1						
8/29/96         13:11:11         319.0463         18.588         319.001         8.54         0.71           8/29/96         13:16:11         324.0463         18.549         324.001         8.50         0.70           8/29/96         13:21:11         329.0463         18.507         329.001         8.46         0.70           8/29/96         13:26:11         334.0463         18.468         334.001         8.42         0.70           8/29/96         13:31:11         339.0463         18.429         339.001         8.38         0.69           8/29/96         13:36:11         344.0463         18.387         344.001         8.34         0.69           8/29/96         13:41:11         349.0463         18.348         349.001         8.30         0.69           8/29/96         13:46:11         354.0463         18.306         354.001         8.26         0.68           8/29/96         13:55:11         359.0463         18.267         359.001         8.22         0.68           8/29/96         14:01:11         369.0463         18.191         369.001         8.14         0.68           8/29/96         14:16:11         374.0463         18.152         374.001         8.07 <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>							
8/29/96         13:16:11         324.0463         18.549         324.001         8.50         0.70           8/29/96         13:21:11         329.0463         18.507         329.001         8.46         0.70           8/29/96         13:26:11         334.0463         18.468         334.001         8.42         0.70           8/29/96         13:31:11         339.0463         18.429         339.001         8.38         0.69           8/29/96         13:36:11         344.0463         18.387         344.001         8.34         0.69           8/29/96         13:41:11         349.0463         18.348         349.001         8.30         0.69           8/29/96         13:46:11         354.0463         18.306         354.001         8.26         0.68           8/29/96         13:51:11         359.0463         18.267         359.001         8.22         0.68           8/29/96         14:01:11         369.0463         18.191         369.001         8.18         0.68           8/29/96         14:11:11         374.0463         18.152         374.001         8.07         0.67           8/29/96         14:16:11         384.0463         18.076         384.001         8.03 <td>1 1</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>	1 1						
8/29/96         13:21:11         329.0463         18:507         329.001         8.46         0.70           8/29/96         13:26:11         334.0463         18:468         334.001         8.42         0.70           8/29/96         13:31:11         339.0463         18:429         339.001         8:38         0.69           8/29/96         13:36:11         344.0463         18:387         344.001         8:34         0.69           8/29/96         13:41:11         349.0463         18:348         349.001         8:30         0.69           8/29/96         13:46:11         354.0463         18:306         354.001         8:26         0.68           8/29/96         13:51:11         359.0463         18:267         359.001         8:22         0.68           8/29/96         13:56:11         364.0463         18:23         364.001         8:18         0.68           8/29/96         14:01:11         369.0463         18:191         369.001         8:14         0.68           8/29/96         14:11:11         379.0463         18:152         374.001         8:07         0.67           8/29/96         14:16:11         384.0463         18:076         384.001         8:07 <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>							
8/29/96         13:26:11         334.0463         18.468         334.001         8.42         0.70           8/29/96         13:31:11         339.0463         18.429         339.001         8.38         0.69           8/29/96         13:36:11         344.0463         18.387         344.001         8.34         0.69           8/29/96         13:41:11         349.0463         18.348         349.001         8.30         0.69           8/29/96         13:46:11         354.0463         18.306         354.001         8.26         0.68           8/29/96         13:51:11         359.0463         18.267         359.001         8.22         0.68           8/29/96         13:56:11         364.0463         18.23         364.001         8.18         0.68           8/29/96         14:01:11         369.0463         18.191         369.001         8.14         0.68           8/29/96         14:11:11         374.0463         18.152         374.001         8.10         0.67           8/29/96         14:16:11         384.0463         18.076         384.001         8.07         0.67           8/29/96         14:26:11         389.0463         18.036         389.001         7.99 <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>							
8/29/96         13:31:11         339.0463         18.429         339.001         8.38         0.69           8/29/96         13:36:11         344.0463         18.387         344.001         8.34         0.69           8/29/96         13:41:11         349.0463         18.348         349.001         8.30         0.69           8/29/96         13:46:11         354.0463         18.306         354.001         8.26         0.68           8/29/96         13:51:11         359.0463         18.267         359.001         8.22         0.68           8/29/96         13:56:11         364.0463         18.23         364.001         8.18         0.68           8/29/96         14:01:11         369.0463         18.191         369.001         8.14         0.68           8/29/96         14:06:11         374.0463         18.152         374.001         8.10         0.67           8/29/96         14:11:11         379.0463         18.152         374.001         8.07         0.67           8/29/96         14:21:11         384.0463         18.076         384.001         8.03         0.67           8/29/96         14:26:11         394.0463         17.997         394.001         7.99 <td></td> <td></td> <td>1</td> <td></td> <td></td> <td></td> <td></td>			1				
8/29/96         13:36:11         344.0463         18:387         344.001         8:34         0.69           8/29/96         13:41:11         349.0463         18:348         349.001         8:30         0.69           8/29/96         13:46:11         354.0463         18:306         354.001         8:26         0.68           8/29/96         13:51:11         359.0463         18:267         359.001         8:22         0.68           8/29/96         13:56:11         364.0463         18:23         364.001         8:18         0.68           8/29/96         14:01:11         369.0463         18:191         369.001         8:14         0.68           8/29/96         14:06:11         374.0463         18:152         374.001         8:10         0.67           8/29/96         14:11:11         379.0463         18:152         374.001         8:07         0.67           8/29/96         14:16:11         384.0463         18:076         384.001         8:07         0.67           8/29/96         14:21:11         389.0463         18:036         389.001         7:99         0.66           8/29/96         14:31:11         394.0463         17:997         394.001         7:95 <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>							
8/29/96         13:41:11         349.0463         18.348         349.001         8.30         0.69           8/29/96         13:46:11         354.0463         18.306         354.001         8.26         0.68           8/29/96         13:51:11         359.0463         18.267         359.001         8.22         0.68           8/29/96         13:56:11         364.0463         18.23         364.001         8.18         0.68           8/29/96         14:01:11         369.0463         18.191         369.001         8.14         0.68           8/29/96         14:06:11         374.0463         18.152         374.001         8.10         0.67           8/29/96         14:11:11         379.0463         18.152         374.001         8.07         0.67           8/29/96         14:16:11         384.0463         18.076         384.001         8.03         0.67           8/29/96         14:21:11         389.0463         18.036         389.001         7.99         0.66           8/29/96         14:31:11         394.0463         17.997         394.001         7.95         0.66           8/29/96         14:36:11         404.0463         17.921         404.001         7.87 <td></td> <td></td> <td></td> <td></td> <td></td> <td>1</td> <td></td>						1	
8/29/96         13:46:11         354.0463         18.306         354.001         8.26         0.68           8/29/96         13:51:11         359.0463         18.267         359.001         8.22         0.68           8/29/96         13:56:11         364.0463         18.23         364.001         8.18         0.68           8/29/96         14:01:11         369.0463         18.191         369.001         8.14         0.68           8/29/96         14:06:11         374.0463         18.152         374.001         8.10         0.67           8/29/96         14:11:11         379.0463         18.115         379.001         8.07         0.67           8/29/96         14:16:11         384.0463         18.076         384.001         8.03         0.67           8/29/96         14:21:11         389.0463         18.036         389.001         7.99         0.66           8/29/96         14:31:11         394.0463         17.997         394.001         7.95         0.66           8/29/96         14:36:11         404.0463         17.958         399.001         7.91         0.66           8/29/96         14:41:11         409.0463         17.847         404.001         7.87 <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>							
8/29/96         13:51:11         359.0463         18.267         359.001         8.22         0.68           8/29/96         13:56:11         364.0463         18.23         364.001         8.18         0.68           8/29/96         14:01:11         369.0463         18.191         369.001         8.14         0.68           8/29/96         14:06:11         374.0463         18.152         374.001         8.10         0.67           8/29/96         14:11:11         379.0463         18.115         379.001         8.07         0.67           8/29/96         14:16:11         384.0463         18.076         384.001         8.03         0.67           8/29/96         14:21:11         389.0463         18.036         389.001         7.99         0.66           8/29/96         14:31:11         399.0463         17.997         394.001         7.95         0.66           8/29/96         14:36:11         404.0463         17.958         399.001         7.91         0.66           8/29/96         14:41:11         409.0463         17.847         404.001         7.87         0.65           8/29/96         14:46:11         414.0463         17.847         414.001         7.80 <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>							
8/29/96         13:56:11         364.0463         18.23         364.001         8.18         0.68           8/29/96         14:01:11         369.0463         18.191         369.001         8.14         0.68           8/29/96         14:06:11         374.0463         18.152         374.001         8.10         0.67           8/29/96         14:11:11         379.0463         18.115         379.001         8.07         0.67           8/29/96         14:16:11         384.0463         18.076         384.001         8.03         0.67           8/29/96         14:21:11         389.0463         18.036         389.001         7.99         0.66           8/29/96         14:31:11         399.0463         17.997         394.001         7.95         0.66           8/29/96         14:36:11         404.0463         17.958         399.001         7.91         0.66           8/29/96         14:41:11         409.0463         17.847         404.001         7.87         0.65           8/29/96         14:46:11         414.0463         17.847         414.001         7.80         0.65           8/29/96         14:51:11         419.0463         17.808         419.001         7.76 <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>							
8/29/96         14:01:11         369.0463         18.191         369.001         8.14         0.68           8/29/96         14:06:11         374.0463         18.152         374.001         8.10         0.67           8/29/96         14:11:11         379.0463         18.115         379.001         8.07         0.67           8/29/96         14:16:11         384.0463         18.076         384.001         8.03         0.67           8/29/96         14:21:11         389.0463         18.036         389.001         7.99         0.66           8/29/96         14:31:11         399.0463         17.997         394.001         7.95         0.66           8/29/96         14:36:11         404.0463         17.958         399.001         7.91         0.66           8/29/96         14:41:11         409.0463         17.844         409.001         7.87         0.65           8/29/96         14:46:11         414.0463         17.847         414.001         7.80         0.65           8/29/96         14:51:11         419.0463         17.808         419.001         7.76         0.64           8/29/96         14:51:11         419.0463         17.771         424.001         7.72 <td></td> <td></td> <td></td> <td></td> <td>1</td> <td></td> <td></td>					1		
8/29/96         14:06:11         374.0463         18.152         374.001         8.10         0.67           8/29/96         14:11:11         379.0463         18.115         379.001         8.07         0.67           8/29/96         14:16:11         384.0463         18.076         384.001         8.03         0.67           8/29/96         14:21:11         389.0463         18.036         389.001         7.99         0.66           8/29/96         14:26:11         394.0463         17.997         394.001         7.95         0.66           8/29/96         14:31:11         399.0463         17.958         399.001         7.91         0.66           8/29/96         14:36:11         404.0463         17.921         404.001         7.87         0.65           8/29/96         14:41:11         409.0463         17.884         409.001         7.83         0.65           8/29/96         14:46:11         414.0463         17.847         414.001         7.80         0.65           8/29/96         14:51:11         419.0463         17.808         419.001         7.76         0.64           8/29/96         14:56:11         424.0463         17.771         424.001         7.72 <td>1 1</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>	1 1						
8/29/96         14:11:11         379.0463         18.115         379.001         8.07         0.67           8/29/96         14:16:11         384.0463         18.076         384.001         8.03         0.67           8/29/96         14:21:11         389.0463         18.036         389.001         7.99         0.66           8/29/96         14:26:11         394.0463         17.997         394.001         7.95         0.66           8/29/96         14:31:11         399.0463         17.958         399.001         7.91         0.66           8/29/96         14:36:11         404.0463         17.921         404.001         7.87         0.65           8/29/96         14:41:11         409.0463         17.884         409.001         7.83         0.65           8/29/96         14:46:11         414.0463         17.847         414.001         7.80         0.65           8/29/96         14:51:11         419.0463         17.808         419.001         7.76         0.64           8/29/96         14:56:11         424.0463         17.771         424.001         7.72         0.64							
8/29/96         14:16:11         384.0463         18.076         384.001         8.03         0.67           8/29/96         14:21:11         389.0463         18.036         389.001         7.99         0.66           8/29/96         14:26:11         394.0463         17.997         394.001         7.95         0.66           8/29/96         14:31:11         399.0463         17.958         399.001         7.91         0.66           8/29/96         14:36:11         404.0463         17.921         404.001         7.87         0.65           8/29/96         14:41:11         409.0463         17.884         409.001         7.83         0.65           8/29/96         14:46:11         414.0463         17.847         414.001         7.80         0.65           8/29/96         14:51:11         419.0463         17.808         419.001         7.76         0.64           8/29/96         14:56:11         424.0463         17.771         424.001         7.72         0.64			ł.				
8/29/96         14:21:11         389.0463         18.036         389.001         7.99         0.66           8/29/96         14:26:11         394.0463         17.997         394.001         7.95         0.66           8/29/96         14:31:11         399.0463         17.958         399.001         7.91         0.66           8/29/96         14:36:11         404.0463         17.921         404.001         7.87         0.65           8/29/96         14:41:11         409.0463         17.884         409.001         7.83         0.65           8/29/96         14:46:11         414.0463         17.847         414.001         7.80         0.65           8/29/96         14:51:11         419.0463         17.808         419.001         7.76         0.64           8/29/96         14:56:11         424.0463         17.771         424.001         7.72         0.64	I						
8/29/96         14:26:11         394.0463         17.997         394.001         7.95         0.66           8/29/96         14:31:11         399.0463         17.958         399.001         7.91         0.66           8/29/96         14:36:11         404.0463         17.921         404.001         7.87         0.65           8/29/96         14:41:11         409.0463         17.884         409.001         7.83         0.65           8/29/96         14:46:11         414.0463         17.847         414.001         7.80         0.65           8/29/96         14:51:11         419.0463         17.808         419.001         7.76         0.64           8/29/96         14:56:11         424.0463         17.771         424.001         7.72         0.64	I	(		t			
8/29/96     14:31:11     399.0463     17.958     399.001     7.91     0.66       8/29/96     14:36:11     404.0463     17.921     404.001     7.87     0.65       8/29/96     14:41:11     409.0463     17.884     409.001     7.83     0.65       8/29/96     14:46:11     414.0463     17.847     414.001     7.80     0.65       8/29/96     14:51:11     419.0463     17.808     419.001     7.76     0.64       8/29/96     14:56:11     424.0463     17.771     424.001     7.72     0.64							
8/29/96     14:36:11     404.0463     17.921     404.001     7.87     0.65       8/29/96     14:41:11     409.0463     17.884     409.001     7.83     0.65       8/29/96     14:46:11     414.0463     17.847     414.001     7.80     0.65       8/29/96     14:51:11     419.0463     17.808     419.001     7.76     0.64       8/29/96     14:56:11     424.0463     17.771     424.001     7.72     0.64	i i						
8/29/96     14:41:11     409.0463     17.884     409.001     7.83     0.65       8/29/96     14:46:11     414.0463     17.847     414.001     7.80     0.65       8/29/96     14:51:11     419.0463     17.808     419.001     7.76     0.64       8/29/96     14:56:11     424.0463     17.771     424.001     7.72     0.64					1		
8/29/96     14:46:11     414.0463     17.847     414.001     7.80     0.65       8/29/96     14:51:11     419.0463     17.808     419.001     7.76     0.64       8/29/96     14:56:11     424.0463     17.771     424.001     7.72     0.64							
8/29/96     14:51:11     419.0463     17.808     419.001     7.76     0.64       8/29/96     14:56:11     424.0463     17.771     424.001     7.72     0.64							
8/29/96 14:56:11 424.0463 17.771 424.001 7.72 0.64		i e	5	1	1 1	1	
1 1 1 1			1	l .			
, -,,, ,-,-,,,, ,,,,,,,,,,,,,,,,,	8/29/96	15:01:11	429.0463	17.734	429.001	7.68	0.64

DATE	TIME	EVENT	DEPTH TO	TEST	HEAD	HEAD
		ELAPSED	WATER	ELAPSED		RATIO
		TIME		TIME		
	(HR:M:S)	(MIN)	(FEET)	(MIN)	(FEET)	
		_	·			
8/29/96	15:06:11	434.0463	17.695	434.001	7.65	0.63
8/29/96	15:11:11	439.0463	17.663	439.001	7.61	0.63
8/29/96	15:16:11	444.0463	17.626	444.001	7.58	0.63
8/29/96	15:21:11	449.0463	17.589	449.001	7.54	0.63
8/29/96	15:26:11	454.0463	17.552	454.001	7.50	0.62
8/29/96	15:31:11	459.0463	17.515	459.001	7.47	0.62
8/29/96	15:36:11	464.0463	17.481	464.001	7.43	0.62
8/29/96	15:41:11	469.0463	17.441	469.001	7.39	0.61
8/29/96	15:46:11	474.0463	17.407	474.001	7.36	0.61
8/29/96	15:51:11	479.0463	17.37	479.001	7.32	0.61
8/29/96	15:56:11	484.0463	17.335	484.001	7.29	0.60
8/29/96	16:01:11	489.0463	17.298	489.001	7.25	0.60
8/29/96	16:06:11	494.0463	17.264	494.001	7.21	0.60
8/29/96	16:11:11	499.0463	17.229	499.001	7.18	0.60
8/29/96	16:16:11	504.0463	17.192	504.001	7.14	0.59
8/29/96	16:21:11	509.0463	17.16	509.001	7.11	0.59
8/29/96	16:26:11	514.0463	17.123	514.001	7.07	0.59
8/29/96	16:31:11	519.0463	17.088	519.001	7.04	0.58
8/29/96	16:36:11	524.0463	17.056	524.001	7.01	0.58
8/29/96	16:41:11	529.0463	17.024	529.001	6.97	0.58
8/29/96	16:46:11	534.0463	16.989	534.001	6.94	0.58
8/29/96	16:51:11	539.0463	16.955	539.001	6.91	0.57
8/29/96	16:56:11	544.0463	16.92	544.001	6.87	0.57
8/29/96	17:01:11	549.0463	16.888	549.001	6.84	0.57
8/29/96	17:06:11	554.0463	16.853	554.001	6.80	0.56
8/29/96	17:11:11	559.0463	16.821	559.001	6.77	0.56
8/29/96	17:16:11	564.0463	16.786	564.001	6.74	0.56
8/29/96	17:21:11	569.0463	16.752	569.001	6.70	0.56
8/29/96	17:26:11	574.0463	16.719	574.001	6.67	0.55
8/29/96	17:31:11	579.0463	16.687	579.001	6.64	0.55
8/29/96	17:36:11	584.0463	16.652	584.001	6.60	0.55
8/29/96	17:41:11	589.0463	16.616	589.001	6.57	0.54
8/29/96	17:46:11	594.0463	16.579	594.001	6.53	0.54
8/29/96	17:51:11	599.0463	16.539	599.001	6.49	0.54
8/29/96	17:56:11	604.0463	16.507	604.001	6.46	0.54
8/29/96	18:01:11	609.0463	16.47	609.001	6.42	0.53

#### HVORSLEV SLUG TEST ANALYSIS RISING HEAD TEST MW-10R

$$K = \frac{r_c^2}{2L_e} \ln \frac{L_e}{R_e} \left[ \frac{\ln \left(\frac{h_1}{h_2}\right)}{(t2 - t1)} \right] 30.48$$

where:

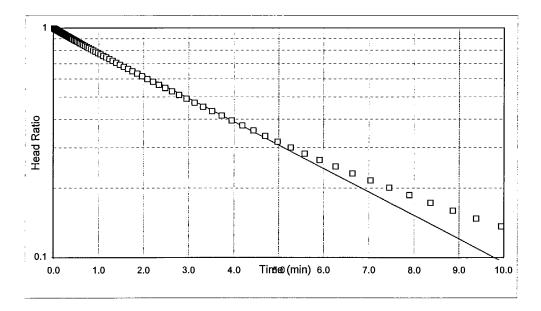
 $r_c$  = casing radius (feet)

R<sub>e</sub> = equivalent radius (feet)

 $L_e$  = length of screened interval (feet)

t = time (minutes) $h_t = \text{head at time } t \text{ (feet)}$ 

INPUT PARAMETER	RS RESULTS
$r_c = 0.08$	
$R_e = 0.15$	
$L_{e} = 10$	K= 1.76E-04 cm/sec
$t_1 = 0$	K= 4.98E-01 ft/day
$t_2 = 10$	
$h_1/h_0 = 1.00$	
$h_2/h_0 = 0.095$	



Project Name: 216 Paterson Plank Road Site, New Jersey

Project No.: 943-6222

Test Date: 08/29/96

Analysis By:

Checked By:

/: FG

Analysis Date:

1/17/97

SDM

# RISING HEAD TEST MW-10R

WELL NO. MW-10R

•		
DATE	8/29/9	96
INITIAL DEPTH TO WATER	6.79	FEET (btoc)
CASING DIAMETER	? 2	INCHES
SAND DIAMETER	3.5	INCHES
TOP OF OPEN INTERVAL	_ 55.5	FEET (btoc)
BOTTOM OF OPEN INTERVAL	_ 65.5	FEET (btoc)
SATURATED THICKNESS	100	FEET
WATER TABLE TO BOTTOM OF SCREEN	\$ 58.7°	1 FEET
EQUIVALENT DIAMETER	2.54	INCHES
OPEN INTERVAL LENGTH	1 10	FEET
STATIC IN SCREEN?	? N	
MAX. HEAD CHANGE	16.2	1 FEET
MAX. HEAD IN SCREEN?	? N	

DATE	TIME	EVENT	DEPTH TO	TEST	HEAD	HEAD
		ELAPSED	WATER	ELAPSED		RATIO
1 1		TIME		TIME		-
	(HR:M:S)	(MIN)	(FEET)	(MIN)	(FEET)	
	,					-
8/29/96	18:15:24	0.0000	22.996	0.000	16.21	1.00
8/29/96	18:15:24	0.0050	22.968	0.005	16.18	1.00
8/29/96	18:15:24	0.0100	22.954	0.010	16.16	1.00
8/29/96	18:15:24	0.0150	22.936	0.015	16.15	1.00
8/29/96	18:15:25	0.0200	22.922	0.020	16.13	1.00
8/29/96	18:15:25	0.0250	22.894	0.025	16.10	0.99
8/29/96	18:15:25	0.0300	22.871	0.030	16.08	0.99
8/29/96	18:15:26	0.0350	22.853	0.035	16.06	0.99
8/29/96	18:15:26	0.0400	22.830	0.040	16.04	0.99
8/29/96	18:15:26	0.0450	22.816	0.045	16.03	0.99
8/29/96	18:15:27	0.0500	22.805	0.050	16.02	0.99
8/29/96	18:15:27	0.0550	22.772	0.055	15.98	0.99
8/29/96	18:15:27	0.0600	22.758	0.060	15.97	0.99
8/29/96	18:15:27	0.0650	22.731	0.065	15.94	0.98
8/29/96	18:15:28	0.0700	22.708	0.070	15.92	0.98
8/29/96	18:15:28	0.0750	22.694	0.075	15.90	0.98
8/29/96	18:15:28	0.0800	22.648	0.080	15.86	0.98
8/29/96	18:15:29	0.0850	22.632	0.085	15.84	0.98
8/29/96	18:15:29	0.0900	22.613	0.090	15.82	0.98
8/29/96	18:15:29	0.0950	22.599	0.095	15.81	0.98
8/29/96	18:15:30	0.1000	22.581	0.100	15.79	0.97
8/29/96	18:15:30	0.1058	22.558	0.106	15.77	0.97
8/29/96	18:15:30	0.1120	22.530	0.112	15.74	0.97
8/29/96	18:15:31	0.1185	22.507	0.119	15.72	0.97
8/29/96	18:15:31	0.1255	22.479	0.126	15.69	0.97
8/29/96	18:15:31	0.1328	22.449	0.133	15.66	0.97
8/29/96	18:15:32	0.1407	22.417	0.141	15.63	0.96
8/29/96	18:15:32	0.1490	22.362	0.149	15.57	0.96
8/29/96	18:15:33	0.1578	22.329	0.158	15.54	0.96
8/29/96	18:15:34	0.1672	22.297	0.167	15.51	0.96
8/29/96	18:15:34	0.1770	22.258	0.177	15.47	0.95
8/29/96	18:15:35	0.1875	22.216	0.188	15.43	0.95
8/29/96	18:15:35	0.1985	22.175	0.199	15.39	0.95
8/29/96	18:15:36	0.2102	22.129	0.210	15.34	0.95
8/29/96	18:15:37	0.2227	22.078	0.223	15.29	0.94
8/29/96	18:15:38	0.2358	22.029	0.236	15.24	0.94
8/29/96	18:15:38	0.2498	21.974	0.250	15.18	0.94
8/29/96	18:15:39	0.2647	21.914	0.265	15.12	0.93

DATE	TIME	EVENT	DEPTH TO	TEST	HEAD	HEAD
1		ELAPSED	WATER	ELAPSED		RATIO
		TIME		TIME		
Ì	(HR:M:S)	(MIN)	(FEET)	(MIN)	(FEET)	
	,		•			
8/29/96	18:15:40	0.2803	21.856	0.280	15.07	0.93
8/29/96	18:15:41	0.2970	21.792	0.297	15.00	0.93
8/29/96	18:15:42	0.3147	21.727	0.315	14.94	0.92
8/29/96	18:15:44	0.3333	21.651	0.333	14.86	0.92
8/29/96	18:15:45	0.3532	21.577	0.353	14.79	0.91
8/29/96	18:15:46	0.3742	21.497	0.374	14.71	0.91
8/29/96	18:15:47	0.3963	21.414	0.396	14.62	0.90
8/29/96	18:15:49	0.4198	21.324	0.420	14.53	0.90
8/29/96	18:15:50	0.4447	21.236	0.445	14.45	0.89
8/29/96	18:15:52	0.4697	21.144	0.470	14.35	0.89
8/29/96	18:15:53	0.4963	21.049	0.496	14.26	0.88
8/29/96	18:15:55	0.5247	20.948	0.525	14.16	0.87
8/29/96	18:15:57	0.5547	20.844	0.555	14.05	0.87
8/29/96	18:15:59	0.5863	20.731	0.586	13.94	0.86
8/29/96	18:16:01	0.6213	20.611	0.621	13.82	0.85
8/29/96	18:16:03	0.6580	20.484	0.658	13.69	0.84
8/29/96	18:16:05	0.6963	20.357	0.696	13.57	0.84
8/29/96	18:16:08	0.7380	20.214	0.738	13.42	0.83
8/29/96	18:16:10	0.7813	20.073	0.781	13.28	0.82
8/29/96	18:16:13	0.8280	19.919	0.828	13.13	0.81
8/29/96	18:16:16	0.8763	19.764	0.876	12.97	0.80
8/29/96	18:16:19	0.9280	19.598	0.928	12.81	0.79
8/29/96	18:16:22	0.9830	19.430	0.983	12.64	0.78
8/29/96	18:16:26	1.0413	19.252	1.041	12.46	0.77
8/29/96	18:16:30	1.1030	19.065	1.103	12.28	0.76
8/29/96	18:16:34	1.1680	18.879	1.168	12.09	0.75
8/29/96	18:16:38	1.2380	18.673	1.238	11.88	0.73
8/29/96	18:16:42	1.3113	18.459	1.311	11.67	0.72
8/29/96	18:16:47	1.3897	18.240	1.390	11.45	0.71
8/29/96	18:16:52	1.4730	18.016	1.473	11.23	0.69
8/29/96	18:16:57	1.5613	17.783	1.561	10.99	0.68
8/29/96	18:17:03	1.6547	17.543	1.655	10.75	0.66
8/29/96	18:17:09	1.7530	17.296	1.753	10.51	0.65
8/29/96	18:17:15	1.8580	17.045	1.858	10.26	0.63
8/29/96	18:17:22	1.9680	16.784	1.968	9.99	0.62
8/29/96	18:17:29	2.0847	16.510	2.085	9.72	0.60
8/29/96	18:17:36	2.2097	16.237	2.210	9.45	0.58
8/29/96	18:17:44 18:17:52	2.3413 2.4813	15.954 15.670	2.341 2.481	9.16 8.88	0.57 0.55
8/29/96		2.4613			8.59	
8/29/96 8/29/96	18:18:01 18:18:11	2.6297	15.375 15.063	2.630 2.786	8.27	0.53 0.51
8/29/96	18:18:21	2.7663	14.757	2.760	7.97	0.51
8/29/96	18:18:31	3.1297	14.757	3.130	7.87	0.49
8/29/96	18:18:42	3.3163	14.136	3.316	7.35	0.47
8/29/96	18:18:54	3.5147	13.822	3,515	7.03	0.43
8/29/96	18:19:07	3.7247	13.506	3.725	6.72	0.43
8/29/96	18:19:20	3.7247	13.195	3.725	6.41	0.40
8/29/96	18:19:34	4.1813	12.886	4.181	6.10	0.40
8/29/96	18:19:49	4.1013	12.574	4.430	5.78	0.36
8/29/96	18:20:05	4.6930	12.268	4,693	5.48	0.34
8/29/96	18:20:22	4.0930	11.961	4.973	5.40	0.34
8/29/96	18:20:40	5.2697	11.666	5.270	4.88	0.32
8/29/96	18:20:58	5.5830	11.373	5.583	4.58	0.30
8/29/96	18:21:18	5.9147	11.089	5.915	4.30	0.20
8/29/96	18:21:39	6.2663	10.814	6.266	4.02	0.27
8/29/96	18:22:02	6.6397	10.545	6.640	3.76	0.23
0123130	10.22.02	0.0091	10.540	0.070	3.70	0.23

DATE	TIME	EVENT	DEPTH TO	TEST	HEAD	HEAD
	i i	ELAPSED	WATER	ELAPSED		RATIO
		TIME		TIME		
<u> </u>	(HR:M:S)	(MIN)	(FEET)	(MIN)	(FEET)	
8/29/96	18:22:26	7.0347	10.293	7.035	3.50	0.22
8/29/96	18:22:51	7.4530	10.046	7.453	3.26	0.20
8/29/96	18:23:17	7.8963	9.809	7.896	3.02	0.19
8/29/96	18:23:45	8.3663	9.585	8.366	2.80	0.17
8/29/96	18:24:15	8.8647	9.375	8.865	2.59	0.16
8/29/96	18:24:47	9.3913	9.177	9.391	2.39	0.15
8/29/96	18:25:20	9.9497	8.994	9.950	2.20	0.14
8/29/96	18:25:56	10.5413	8.821	10.541	2.03	0.13
8/29/96	18:26:34	11.1680	8.651	11.168	1.86	0.11
8/29/96	18:27:13	11.8313	8.492	11.831	1.70	0.11
8/29/96	18:27:56	12.5347	8.344	12.535	1.55	0.10
8/29/96	18:28:40	13.2797	8.217	13.280	1.43	0.09
8/29/96	18:29:28	14.0697	8.088	14.070	1.30	0.08
8/29/96	18:30:18	14.9063	7.980	14.906	1.19	0.07
8/29/96	18:31:11	15.7913	7.869	15.791	1.08	0.07
8/29/96	18:32:07	16.7297	7.770	16.730	0.98	0.06
8/29/96	18:33:07	17.7230	7.677	17.723	0.89	0.05
8/29/96	18:34:10	18.7763	7.594	18.776	0.80	0.05
8/29/96	18:35:17	19.8913	7.516	19.891	0.73	0.04
8/29/96	18:36:28	21.0730	7.449	21.073	0.66	0.04
8/29/96	18:37:43	22.3247	7.384	22.325	0.59	0.04
8/29/96	18:39:02	23.6497	7.324	23.650	0.53	0.03
8/29/96	18:40:27	25.0547	7.269	25.055	0.48	0.03
8/29/96	18:41:56	26.5430	7.221	26.543	0.43	0.03
8/29/96	18:43:31	28.1180	7.175	28.118	0.39	0.02
8/29/96	18:45:11	29.7863	7.138	29.786	0.35	0.02
8/29/96	18:46:57	31.5547	7.101	31.555	0.31	0.02
8/29/96	18:48:49	33.4280	7.064	33.428	0.27	0.02
8/29/96	18:50:48	35.4113	7.036	35.411	0.25	0.02
8/29/96	18:52:54	37.5130	7.008	37.513	0.22	0.01
8/29/96	18:55:08	39.7397	6.985	39.740	0.20	0.01
8/29/96	18:57:29	42.0980	6.962	42.098	0.17	0.01
8/29/96	18:59:59	44.5963	6.946	44.596	0.16	0.01
8/29/96	19:02:38	47.2430	6.932	47.243	0.14	0.01
8/29/96	19:05:26	50.0463	6.914	50.046	0.12	0.01
8/29/96	19:08:24	53.0147	6.900	53.015	0.11	0.01

# HVORSLEV SLUG TEST ANALYSIS RISING HEAD TEST MW-11R TEST 1

$$K = \frac{r_c^2}{2L_e} \ln \frac{L_e}{R_e} \left[ \frac{\ln \left( \frac{h_t}{h_2} \right)}{(t2 - t1)} \right] 30.48$$

where:

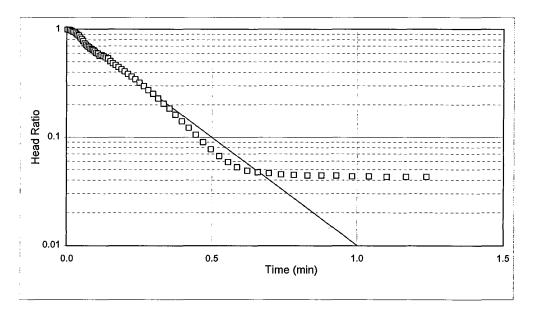
 $r_c$  = casing radius (feet)

 $R_e$  = equivalent radius (feet)

 $L_e$  = length of screened interval (feet)

t = time (minutes) $h_t = \text{head at time } t \text{ (feet)}$ 

INPUT PARAMETERS	RESULTS
$r_c = 0.15$	
$R_e = 0.15$	
$L_e = 10$	K= 1.05E-02 cm/sec
$t_1 = 0$	K= 2.98E+01 ft/day
$t_2 = 1$	
$h_1/h_0 = 1.00$	
$h_2/h_0 = 0.01$	



Project Name: 216 Paterson Plank Road Site, New Jersey

Project No.: 943-6222

Test Date: 08/27/96

Analysis By:

Checked By:

Analysis Date:

SDM FG 1/20/97

# RISING HEAD TEST MW-11R TEST 1 WELL NO. W-11R TES

DATE 8/27/96 INITIAL DEPTH TO WATER 5.51 FEET (btoc) **INCHES** CASING DIAMETER 3.5 SAND DIAMETER 3.5 INCHES TOP OF OPEN INTERVAL FEET (btoc) 48 BOTTOM OF OPEN INTERVAL FEET (btoc) 58 SATURATED THICKNESS 10 FEET WATER TABLE TO BOTTOM OF SCREEN FEET 52.49 EQUIVALENT DIAMETER INCHES 3.50 OPEN INTERVAL LENGTH 10 FEET STATIC IN SCREEN? Ν FEET MAX, HEAD CHANGE 10.65 MAX. HEAD IN SCREEN? Ν

DATE	TIME	EVENT	DEPTH TO	TEST	HEAD	HEAD
		ELAPSED	WATER	ELAPSED		RATIO
		TIME	.6.4.1	TIME		
	(HR:M:S)	(MIN)	(FEET)	(MIN)	(FEET)	
8/27/96	10:30:15	0.000	16.161	0.000	10.65	1.00
8/27/96	10:30:15	0.005	16.114	0.005	10.60	1.00
8/27/96	10:30:15	0.010	16.020	0.010	10.51	0.99
8/27/96	10:30:15	0.015	15.879	0.015	10.37	0.97
8/27/96	10:30:16	0.020	15.676	0.020	10.17	0.95
8/27/96	10:30:16	0.025	15.591	0.025	10.08	0.95
8/27/96	10:30:16	0.030	15.316	0.030	9.81	0.92
8/27/96	10:30:17	0.035	15.072	0.035	9.56	0.90
8/27/96	10:30:17	0.040	14.850	0.040	9.34	0.88
8/27/96	10:30:17	0.045	14.454	0.045	8.94	0.84
8/27/96	10:30:18	0.050	14.165	0.050	8.66	0.81
8/27/96	10:30:18	0.055	13.835	0.055	8.33	0.78
8/27/96	10:30:18	0.060	13.429	0.060	7.92	0.74
8/27/96	10:30:18	0.065	13.185	0.065	7.68	0.72
8/27/96	10:30:19	0.070	12.950	0.070	7.44	0.70
8/27/96	10:30:19	0.075	12.816	0.075	7.31	0.69
8/27/96	10:30:19	0.080	12.594	0.080	7.08	0.67
8/27/96	10:30:20	0.085	12.463	0.085	6.95	0.65
8/27/96	10:30:20	0.090	12.373	0.090	6.86	0.64
8/27/96	10:30:20	0.095	12.177	0.095	6.67	0.63
8/27/96	10:30:21	0.100	11.979	0.100	6.47	0.61
8/27/96	10:30:21	0.106	11.865	0.106	6.36	0.60
8/27/96	10:30:21	0.112	11.568	0.112	6.06	0.57
8/27/96	10:30:22	0.119	11.672	0.119	6.16	0.58
8/27/96	10:30:22	0.126	11.549	0.126	6.04	0.57
8/27/96	10:30:22	0.133	11.379	0.133	5.87	0.55
8/27/96	10:30:23	0.141	11.247	0.141	5.74	0.54
8/27/96	10:30:23	0.149	10.922	0.149	5.41	0.51
8/27/96	10:30:24	0.158	10.673	0.158	5.16	0.48
8/27/96	10:30:25	0.167	10.484	0.167	4.97	0.47
8/27/96	10:30:25	0.177	10.276	0.177	4.77	0.45
8/27/96	10:30:26	0.188	10.064	0.188	4.55	0.43
8/27/96	10:30:26	0.199	9.852	0.199	4.34	0.41
8/27/96	10:30:27	0.210	9.626	0.210	4.12	0.39
8/27/96	10:30:28	0.223	9.409	0.223	3.90	0.37
8/27/96	10:30:29	0.236	9.183	0.236	3.67	0.34
8/27/96	10:30:29	0.250	8.915	0.250	3.41	0.32
8/27/96	10:30:30	0.265	8.685	0.265	3.18	0.30
8/27/96	10:30:31	0.280	8.431	0.280	2.92	0.27

DATE	TIME	EVENT	DEPTH TO	TEST	HEAD	HEAD
		ELAPSED	WATER	ELAPSED		RATIO
		TIME	,	TIME		
	(HR:M:S)	(MIN)	(FEET)	(MIN)	(FEET)	
8/27/96	10:30:32	0.297	8.200	0.297	2.69	0.25
8/27/96	10:30:33	0.315	7.946	0.315	2.44	0.23
8/27/96	10:30:35	0.333	7.695	0.333	2.19	0.21
8/27/96	10:30:36	0.353	7.478	0.353	1.97	0.18
8/27/96	10:30:37	0.374	7.238	0:374	1.73	0.16
8/27/96	10:30:38	0.396	7.012	0.396	1.50	0.14
8/27/96	10:30:40	0.420	6.816	0.420	1.31	0.12
8/27/96	10:30:41	0.445	6.632	0.445	1.12	0.11
8/27/96	10:30:43	0.470	6.472	0.470	0.96	0.09
8/27/96	10:30:44	0.496	6.336	0.496	0.83	0.08
8/27/96	10:30:46	0.525	6.223	0.525	0.71	0.07
8/27/96	10:30:48	0.555	6.138	0.555	0.63	0.06
8/27/96	10:30:50	0.586	6.073	0.586	0.56	0.05
8/27/96	10:30:52	0.621	6.034	0.621	0.52	0.05
8/27/96	10:30:54	0.658	6.016	0.658	0.51	0.05
8/27/96	10:30:56	0.696	6.007	0.696	0.50	0.05
8/27/96	10:30:59	0.738	5.993	0.738	0.48	0.05
8/27/96	10:31:01	0.781	5.988	0.781	0.48	0.04
8/27/96	10:31:04	0.828	5.983	0.828	0.47	0.04
8/27/96	10:31:07	0.876	5.983	0.876	0.47	0.04
8/27/96	10:31:10	0.928	5.979	0.928	0.47	0.04
8/27/96	10:31:13	0.983	5.974	0.983	0.46	0.04
8/27/96	10:31:17	1.041	5.974	1.041	0.46	0.04
8/27/96	10:31:21	1.103	5.970	1.103	0.46	0.04
8/27/96	10:31:25	1.168	5.970	1.168	0.46	0.04
8/27/96	10:31:29	1.238	5.970	1.238	0.46	0.04

# HVORSLEV SLUG TEST ANALYSIS RISING HEAD TEST MW-11R-TEST 2

$$K = \frac{r_c^3}{2L_e} \ln \frac{L_e}{R_e} \left[ \frac{\ln \left( \frac{h_t}{h_2} \right)}{(t2 - t1)} \right] 30.48$$

where:

 $r_c$  = casing radius (feet)

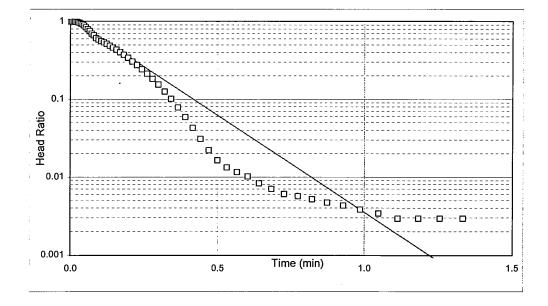
 $R_e$  = equivalent radius (feet)

L<sub>e</sub> = length of screened interval (feet)

t = time (minutes)

 $h_t$  = head at time t (feet)

INPUT PARAN	METERS		RESULTS	
r <sub>c</sub> =	0.15			
$R_e =$	0.15			
L <sub>e</sub> =	10	K=	1.31E-02 cm/sec	
$t_1 =$	0	K=	3.72E+01 ft/day	
t <sub>2</sub> =	1.5	•		
$h_1/h_0 =$	1.10			
$h_2/h_0 = 0$	0.0002			



Project Name: 216 Paterson Plank Road Site, New Jersey

Project No.: 943-6222

Analysis By:

SDM

Test Date: 08/27/96

Checked By: Analysis Date: FG 1/17/97

# RISING HEAD TEST MW-11R-TEST 2 WELL NO. MW-11R

DATE	8/27/96	
INITIAL DEPTH TO WATER	5.97	FEET (btoc)
CASING DIAMETER	3.5	INCHES
SAND DIAMETER	3.5	INCHES
TOP OF OPEN INTERVAL	48	FEET (btoc)
BOTTOM OF OPEN INTERVAL	58	FEET (btoc)
SATURATED THICKNESS	10	FEET
WATER TABLE TO BOTTOM OF SCREEN	52.03	FEET
EQUIVALENT DIAMETER	3.50	INCHES
OPEN INTERVAL LENGTH	10	FEET
STATIC IN SCREEN?	N	
MAX. HEAD CHANGE	10.18	FEET
MAX. HEAD IN SCREEN?	N	

DATE	TIME	EVENT	DEPTH TO	TEST	HEAD	HEAD
		ELAPSED	WATER	ELAPSED		RATIO
1 1		TIME		TIME	l	100
	(HR:M:S)	(MIN)	(FEET)	(MIN)	(FEET)	. ***
		0.000	40.45		40.40	
8/27/96	10:47:14	0.000	16.15	· '	10.18	:
8/27/96	10:47:14	0.005	16.16		10.19	
8/27/96	10:47:14	0.010	16.16		10.19	
8/27/96	10:47:14	0.015	16.16		10.19	
8/27/96	10:47:15	0.020	16.16		10.19	ì
8/27/96	10:47:15	0.025	16.16		10.19	
8/27/96	10:47:15	0.030	16.16		10.19	
8/27/96	10:47:16	0.035	16.16		10.19	
8/27/96	10:47:16	0.040	16.16		10.19	]
8/27/96	10:47:16	0.045	16.16		10.19	
8/27/96	10:47:17	0.050	16.16		10.19	
8/27/96	10:47:17	0.055	16.16	0.000	10.19	1.00
8/27/96	10:47:17	0.060	16.15	0.005	10.18	1.00
8/27/96	10:47:17	0.065	16.15	0.010	10.18	1.00
8/27/96	10:47:18	0.070	16.12	0.015	10.15	1.00
8/27/96	10:47:18	0.075	16.05	0.020	10.08	0.99
8/27/96	10:47:18	0.080	15.96	0.025	9.99	0.98
8/27/96	10:47:19	0.085	15.80	0.030	9.83	0.97
8/27/96	10:47:19	0.090	15.58	0.035	9.61	0.94
8/27/96	10:47:19	0.095	15.37	0.040	9.40	0.92
8/27/96	10:47:20	0.100	15.02	0.045	9.05	0.89
8/27/96	10:47:20	0.106	14.60	0.051	8.63	0.85
8/27/96	10:47:20	0.112	14.09	0.057	8.12	0.80
8/27/96	10:47:21	0.119	13.65	0.064	7.68	0.75
8/27/96	10:47:21	0.126	13.08	0.071	7.11	0.70
8/27/96	10:47:21	0.133	12.77	0.078	6.80	0.67
8/27/96	10:47:22	0.141	12.21	0.086	6.24	0.61
8/27/96	10:47:22	0.149	11.93	0.094	5.96	0.59
8/27/96	10:47:23	0.158	11.68	0.103	5.71	0.56
8/27/96	10:47:24	0.167	11.47	0.112	5.50	0.54
8/27/96	10:47:24	0.177	11.25	0.122	5.28	0.52
8/27/96	10:47:25	0.188	10.96	0.133	4.99	0.49
8/27/96	10:47:25	0.199	10.67	0.144	4.70	0.46
8/27/96	10:47:26	0.210	10.41	0.155	4.44	0.44
8/27/96	10:47:27	0.223	10.08	0.168	4.11	0.40
8/27/96	10:47:28	0.236	9.79	0.181	3.82	0.38
8/27/96	10:47:28	0.250	9.45	0.195	3.48	0.34
8/27/96	10:47:29	0.265	9.08	0.210	3.11	0.31

DATE	TIME	EL (EL IT	DEDTH TO	TEOT	LIEAD	HEAD
DATE	TIME	EVENT	DEPTH TO	TEST	HEAD	1
ļ		ELAPSED	WATER	ELAPSED		RATIO
		TIME	/·	TIME	(FFFF	
	(HR:M:S)	(MIN)	(FEET)	(MIN)	(FEET)	
8/27/96	10:47:30	0.280	8.78	0.225	2.81	0.28
8/27/96	10:47:31	0.297	8.45	0.242	2.48	0.24
8/27/96	10:47:32	0.207	8.15	0.260	2.18	0.21
8/27/96	10:47:34	0.333	7.83	0.278	1.86	0.18
8/27/96	10:47:35	0.353	7.55	0.298	1.58	0.15
8/27/96	10:47:36	0.374	7.25	0.319	1.28	0.13
8/27/96	10:47:37	0.396	7.00	0.341	1.03	0.10
8/27/96	10:47:39	0.420	6.77	0.365	0.80	0.08
8/27/96	10:47:40	0.445	6.57	0.390	0.60	0.06
8/27/96	10:47:42	0.470	6.41	0.415	0.44	0.04
8/27/96	10:47:43	0.496	6.29	0.441	0.32	0.03
8/27/96	10:47:45	0.525	6.20	0.470	0.23	0.02
8/27/96	10:47:47	0.555	6.14	0.500	0.17	0.02
8/27/96	10:47:49	0.586	6.11	0.531	0.14	0.01
8/27/96	10:47:51	0.621	6.09	0.566	0.12	0.01
8/27/96	10:47:53	0.658	6.07	0.603	0.10	0.01
8/27/96	10:47:55	0.696	6.06	0.641	0.09	0.01
8/27/96	10:47:58	0.738	6.04	0.683	0.07	0.01
8/27/96	10:48:00	0.781	6.03	0.726	0.06	0.01
8/27/96	10:48:03	0.828	6.03	0.773	0.06	0.01
8/27/96	10:48:06	0.876	6.02	0.821	0.05	0.01
8/27/96	10:48:09	0.928	6.02	0.873	0.05	0.00
8/27/96	10:48:12	0.983	6.01	0.928	0.04	0.00
8/27/96	10:48:16	1.041	6.01	0.986	0.04	0.00
8/27/96	10:48:20	1.103	6.01	1.048	0.04	0.00
8/27/96	10:48:24	1.168	6.00	1.113	0.03	0.00
8/27/96	10:48:28	1.238	6.00	1.183	0.03	0.00
8/27/96	10:48:32	1.311	6.00	1.256	0.03	0.00
8/27/96	10:48:37	1.390	6.00	1.335	0.03	0.00

### HVORSLEV SLUG TEST ANALYSIS RISING HEAD TEST MW-14D

$$K = \frac{r_c^{-1}}{2L_e} \ln \frac{L_e}{R_e} \left[ \frac{\ln \left( \frac{h_1}{h_2} \right)}{(t2 - t1)} \right] 30.48$$

where:

 $r_c$  = casing radius (feet)

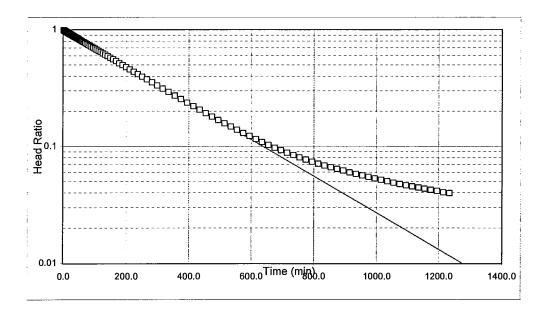
 $R_e$  = equivalent radius (feet)

 $L_e$  = length of screened interval (feet)

t = time (minutes)

 $h_t$  = head at time t (feet)

INPUT PARAMETERS	RESULTS
$r_c = 0.17$	
$R_e = 0.33$	
$L_{e} = 14$	K= 6.80E-06 cm/sec
$t_1 = 0$	K= 1.93E-02 ft/day
$t_2 = 1276$	
$h_1/h_0 = 1.00$	
$h_2/h_0 = 0.01$	



Project Name: 216 Pateson Plank Road Site, New Jersey

Project No.: 943-6222

Test Date: 08/29/96

Analysis By:

SDM

Checked By:

Analysis Date:

FG 1/17/97

#### **RISING HEAD TEST MW-14D**

WELL NO. MW-14D

DATE 8/29/96 INITIAL DEPTH TO WATER 0.92 FEET (btoc) **INCHES** CASING DIAMETER **INCHES** SAND DIAMETER 8 TOP OF OPEN INTERVAL 27 FEET (btoc) BOTTOM OF OPEN INTERVAL 41 FEET (btoc) **FEET** SATURATED THICKNESS 13 WATER TABLE TO BOTTOM OF SCREEN 40.08 FEET **INCHES** EQUIVALENT DIAMETER 5.51 OPEN INTERVAL LENGTH 14 FEET STATIC IN SCREEN? Ν FEET MAX. HEAD CHANGE 17.04 MAX. HEAD IN SCREEN? Ν

DATE	TIME	EVENT	DEPTH TO	TEST	HEAD	HEAD
		ELAPSED	WATER	ELAPSED		RATIO
]		TIME		TIME	1.0	
	(HR:M:S)	(MIN)	(FEET)	(MIN)	(FEET)	
8/27/96	15:27:39	0.000	17.961	0.000	17.04	1.00
8/27/96	15:27:39	0.005	17.963	0.005	17.04	1.00
8/27/96	15:27:39	0.010	17.961	0.010	17.04	1.00
8/27/96	15:27:39	0.015	17.961	0.015	17.04	1.00
8/27/96	15:27:40	0.020	17.961	0.020	17.04	1.00
8/27/96	15:27:40	0.025	17.961	0.025	17.04	1.00
8/27/96	15:27:40	0.030	17.959	0.030	17.04	1.00
8/27/96	15:27:41	0.035	17.956	0.035	17.04	1.00
8/27/96	15:27:41	0.040	17.956	0.040	17.04	1.00
8/27/96	15:27:41	0.045	17.956	0.045	17.04	1.00
8/27/96	15:27:42	0.050	17.954	0.050	17.03	1.00
8/27/96	15:27:42	0.055	17.954	0.055	17.03	1.00
8/27/96	15:27:42	0.060	17.954	0.060	17.03	1.00
8/27/96	15:27:42	0.065	17.954	0.065	17.03	1.00
8/27/96	15:27:43	0.070	17.954	0.070	17.03	1.00
8/27/96	15:27:43	0.075	17.956	0.075	17.04	1.00
8/27/96	15:27:43	0.080	17.952	0.080	17.03	1.00
8/27/96	15:27:44	0.085	17.952	0.085	17.03	1.00
8/27/96	15:27:44	0.090	17.950	0.090	17.03	1.00
8/27/96	15:27:44	0.095	17.950	0.095	17.03	1.00
8/27/96	15:27:45	0.100	17.950	0.100	17.03	1.00
8/27/96	15:27:45	0.106	17.950	0.106	17.03	1.00
8/27/96	15:27:45	0.112	17.947	0.112	17.03	1.00
8/27/96	15:27:46	0.119	17.947	0.119	17.03	1.00
8/27/96	15:27:46	0.126	17.947	0.126	17.03	1.00
8/27/96	15:27:46	0.133	17.945	0.133	17.03	1.00
8/27/96	15:27:47	0.141	17.943	0.141	17.02	1.00
8/27/96	15:27:47	0.149	17.943	0.149	17.02	1.00
8/27/96	15:27:48	0.158	17.940	0.158	17.02	1.00
8/27/96	15:27:49	0.167	17.940	0.167	17.02	1.00
8/27/96	15:27:49	0.177	17.938	0.177	17.02	1.00
8/27/96	15:27:50	0.188	17.938	0.188	17.02	1.00
8/27/96	15:27:50	0.199	17.938	0.199	17.02	1.00
8/27/96	15:27:51	0.210	17.936	0.210	17.02	1.00
8/27/96	15:27:52	0.223	17.936	0.223	17.02	1.00
8/27/96	15:27:53	0.236	17.933	0.236	17.01	1.00
8/27/96	15:27:53	0.250	17.931	0.250	17.01	1.00
8/27/96	15:27:54	0.265	17.931	0.265	17.01	1.00
8/27/96	15:27:55	0.280	17.929	0.280	17.01	1.00

RATIO   RATI	DATE	TIME	EVENT	DEPTH TO	TEST	HEAD	HEAD
B/Z7/96   15:27:56   0.297   17.927   0.297   17.01   1.00			1				
8/27/96	.		TIME		TIME		
8/27/96 15:27:56 0.297 17.927 0.297 17.01 1.00 8/27/96 15:27:57 0.315 17.924 0.315 17.00 1.00 8/27/96 15:27:59 0.333 17.924 0.333 17.00 1.00 8/27/96 15:28:00 0.353 17.922 0.353 17.00 1.00 8/27/96 15:28:01 0.374 17.920 0.374 17.00 8/27/96 15:28:02 0.396 17.917 0.396 17.00 1.00 8/27/96 15:28:04 0.420 17.915 0.420 17.00 1.00 8/27/96 15:28:05 0.445 17.913 0.445 16.99 1.00 8/27/96 15:28:08 0.496 17.901 0.470 16.99 8/27/96 15:28:08 0.496 17.900 0.525 16.99 8/27/96 15:28:10 0.525 17.906 0.525 16.99 8/27/96 15:28:14 0.586 17.901 0.586 16.98 8/27/96 15:28:14 0.586 17.901 0.586 16.98 8/27/96 15:28:16 0.6521 17.897 0.621 16.98 8/27/96 15:28:18 0.668 17.894 0.658 16.97 8/27/96 15:28:20 0.696 17.892 0.696 16.97 1.00 8/27/96 15:28:20 0.696 17.892 0.696 16.97 1.00 8/27/96 15:28:28 0.828 17.880 0.828 16.97 8/27/96 15:28:28 0.828 17.880 0.828 16.96 8/27/96 15:28:31 0.876 17.878 0.828 16.99 8/27/96 15:28:32 0.781 17.883 0.781 16.96 10.99 8/27/96 15:28:28 0.828 17.880 0.828 16.96 8/27/96 15:28:31 0.876 17.883 0.781 16.96 1.00 8/27/96 15:28:32 0.783 17.890 0.738 16.97 1.00 8/27/96 15:28:33 0.783 17.890 0.738 16.97 1.00 8/27/96 15:28:34 0.876 17.878 0.876 16.98 1.00 8/27/96 15:28:34 0.928 17.871 0.928 16.95 0.99 8/27/96 15:28:41 1.041 17.864 1.041 16.94 0.99 8/27/96 15:28:45 1.103 17.880 0.828 16.96 1.00 8/27/96 15:28:45 1.103 17.880 0.828 16.99 0.93 8/27/96 15:28:45 1.103 17.880 0.828 16.99 0.93 8/27/96 15:28:45 1.103 17.880 0.806 1.00 8/27/96 15:28:45 1.103 17.880 0.828 16.99 0.99 8/27/96 15:28:45 1.103 17.880 0.806 1.00 8/27/96 15:28:45 1.103 17.880 0.806 1.00 8/27/96 15:28:45 1.103 17.880 0.806 1.00 8/27/96 15:28:45 1.103 17.880 0.90 8/27/96 15:28:45 1.103 17.880 0.90 8/27/96 15:28:57 0.983 17.890 0.983 16.95 0.99 8/27/96 15:28:57 0.983 17.890 0.983 16.99 0.99 8/27/96 15:28:59 1.238 17.890 0.983 16.99 0.99 8/27/96 15:28:59 1.238 17.890 0.938 16.99 0.99 8/27/96 15:29:10 1.665 17.820 1.038 1.09 8/27/96 15:29:10 1.665 17.820 1.038 1.09 8/27/96 15:29:10 1.666 17.820 1.038 1.09 8/27/96 15:29:10 1.666 17.820 1.038 1.09 8/27/96 15:30:		(HR:M:S)		(FEET)		(FEET)	
8/27/96 15:27:57 0.315 17.924 0.315 17.00 1.00 8/27/96 15:27:59 0.333 17.924 0.333 17.00 1.00 8/27/96 15:28:00 0.353 17.922 0.353 17.00 1.00 8/27/96 15:28:01 0.374 17.920 0.374 17.00 1.00 8/27/96 15:28:04 0.420 17.915 0.420 17.00 1.00 8/27/96 15:28:05 0.445 17.915 0.420 17.00 1.00 8/27/96 15:28:05 0.445 17.913 0.445 16.99 1.00 8/27/96 15:28:08 0.496 17.900 0.470 16.99 1.00 8/27/96 15:28:08 0.496 17.900 0.470 16.99 1.00 8/27/96 15:28:10 0.525 17.906 0.525 16.99 1.00 8/27/96 15:28:10 0.525 17.906 0.525 16.99 1.00 8/27/96 15:28:14 0.586 17.901 0.586 16.98 1.00 8/27/96 15:28:18 0.658 17.901 0.586 16.98 1.00 8/27/96 15:28:18 0.658 17.897 0.621 16.98 1.00 8/27/96 15:28:20 0.586 17.892 0.696 16.97 1.00 8/27/96 15:28:20 0.586 17.892 0.696 16.97 1.00 8/27/96 15:28:23 0.733 17.890 0.738 16.97 1.00 8/27/96 15:28:23 0.738 17.890 0.738 16.97 1.00 8/27/96 15:28:23 0.738 17.890 0.738 16.97 1.00 8/27/96 15:28:23 0.738 17.890 0.738 16.97 1.00 8/27/96 15:28:24 0.828 17.880 0.828 16.96 10.97 1.00 8/27/96 15:28:24 0.828 17.880 0.828 16.96 1.00 8/27/96 15:28:24 0.828 17.880 0.828 16.96 1.00 8/27/96 15:28:34 0.928 17.871 0.928 16.95 0.98 8/27/96 15:28:34 0.928 17.871 0.928 16.95 0.98 8/27/96 15:28:34 0.928 17.871 0.928 16.95 0.98 8/27/96 15:28:34 0.928 17.871 0.928 16.95 0.98 8/27/96 15:28:45 1.103 17.860 1.103 16.94 0.99 8/27/96 15:28:45 1.103 17.860 1.103 16.94 0.99 8/27/96 15:28:45 1.103 17.860 1.103 16.94 0.99 8/27/96 15:28:45 1.103 17.860 1.103 16.94 0.99 8/27/96 15:28:59 1.238 17.871 0.928 16.95 0.99 8/27/96 15:29:24 1.551 1.787 1.884 1.473 16.91 0.99 8/27/96 15:29:29 1.551 1.238 17.871 0.928 16.95 0.99 8/27/96 15:29:29 1.551 1.238 17.890 1.339 1.695 0.99 8/27/96 15:29:29 1.551 1.238 17.890 1.339 1.695 0.99 8/27/96 15:29:37 1.886 17.907 1.886 1.041 16.94 0.99 8/27/96 15:29:40 1.529:51 1.238 17.890 1.339 1.695 0.99 8/27/96 15:29:40 1.529:51 1.238 17.890 1.339 1.695 0.99 8/27/96 15:29:40 1.529:51 1.238 17.890 1.339 1.695 0.99 8/27/96 15:29:40 1.529:51 1.238 17.790 1.665 16.89 0.99 8/27/96 15:29:51 1.240 1.753 17.890 1.895 1.895		, , , , , , , , , , , , , , , , , , ,		,	, , , , ,	, , , , , , , , , , , , , , , , , , , ,	
8/27/96 15:28:00 0.333 17.924 0.333 17.00 1.00 8/27/96 15:28:01 0.374 17.920 0.374 17.00 8/27/96 15:28:02 0.396 17.917 0.396 17.00 1.00 8/27/96 15:28:02 0.396 17.917 0.396 17.00 1.00 8/27/96 15:28:05 0.445 17.913 0.445 16.99 1.00 8/27/96 15:28:05 0.445 17.913 0.445 16.99 1.00 8/27/96 15:28:07 0.470 17.910 0.470 16.99 1.00 8/27/96 15:28:08 0.496 17.908 0.496 16.99 1.00 8/27/96 15:28:10 0.525 17.906 0.525 16.99 1.00 8/27/96 15:28:10 0.525 17.903 0.555 16.98 1.00 8/27/96 15:28:14 0.586 17.901 0.586 16.99 1.00 8/27/96 15:28:14 0.586 17.901 0.586 16.99 1.00 8/27/96 15:28:18 0.6621 17.897 0.621 16.98 1.00 8/27/96 15:28:20 0.696 17.892 0.696 16.97 1.00 8/27/96 15:28:23 0.738 17.890 0.738 16.97 1.00 8/27/96 15:28:23 0.738 17.890 0.738 16.97 1.00 8/27/96 15:28:23 0.738 17.880 0.828 16.96 10.97 8/27/96 15:28:24 0.928 17.880 0.828 16.96 1.00 8/27/96 15:28:31 0.876 17.883 0.781 16.96 1.00 8/27/96 15:28:31 0.876 17.883 0.781 16.96 1.00 8/27/96 15:28:34 0.928 17.880 0.828 16.96 1.00 8/27/96 15:28:34 0.928 17.880 0.828 16.96 1.00 8/27/96 15:28:34 0.928 17.880 0.828 16.96 1.00 8/27/96 15:28:34 0.928 17.880 0.828 16.96 1.00 8/27/96 15:28:34 0.928 17.871 0.928 16.95 0.99 8/27/96 15:28:41 1.041 17.864 1.041 16.94 0.99 8/27/96 15:28:45 1.103 17.860 1.103 16.94 0.99 8/27/96 15:28:45 1.103 17.860 1.103 16.94 0.99 8/27/96 15:29:02 1.390 17.839 1.390 16.92 0.99 8/27/96 15:29:02 1.390 17.839 1.390 16.92 0.99 8/27/96 15:29:02 1.390 17.839 1.390 16.92 0.99 8/27/96 15:29:03 1.856 17.802 1.655 16.90 0.99 8/27/96 15:29:04 1.655 17.820 1.655 16.90 0.99 8/27/96 15:29:07 1.473 17.844 1.473 16.91 0.99 8/27/96 15:29:07 1.473 17.846 1.311 16.93 0.99 8/27/96 15:29:07 1.473 17.846 1.311 16.93 0.99 8/27/96 15:29:07 1.473 17.846 1.311 16.93 0.99 8/27/96 15:29:07 1.473 17.846 1.311 16.93 0.99 8/27/96 15:29:07 1.473 17.846 1.311 16.93 0.99 8/27/96 15:29:07 1.473 17.846 1.311 16.93 0.99 8/27/96 15:29:07 1.473 17.846 1.311 16.93 0.99 8/27/96 15:29:07 1.473 17.846 1.311 16.95 0.99 8/27/96 15:29:07 1.473 17.662 1.665 16.90 0.99 8/27/96 15:29:07 1.473 17.66	8/27/96	15:27:56	0.297	17.927	0.297	17.01	1.00
8/27/96 15:28:00 0.333 17.924 0.333 17.00 1.00 8/27/96 15:28:01 0.374 17.920 0.374 17.00 8/27/96 15:28:02 0.396 17.917 0.396 17.00 1.00 8/27/96 15:28:02 0.396 17.917 0.396 17.00 1.00 8/27/96 15:28:05 0.445 17.913 0.445 16.99 1.00 8/27/96 15:28:05 0.445 17.913 0.445 16.99 1.00 8/27/96 15:28:07 0.470 17.910 0.470 16.99 1.00 8/27/96 15:28:08 0.496 17.908 0.496 16.99 1.00 8/27/96 15:28:10 0.525 17.906 0.525 16.99 1.00 8/27/96 15:28:10 0.525 17.903 0.555 16.98 1.00 8/27/96 15:28:14 0.586 17.901 0.586 16.99 1.00 8/27/96 15:28:14 0.586 17.901 0.586 16.99 1.00 8/27/96 15:28:18 0.6621 17.897 0.621 16.98 1.00 8/27/96 15:28:20 0.696 17.892 0.696 16.97 1.00 8/27/96 15:28:23 0.738 17.890 0.738 16.97 1.00 8/27/96 15:28:23 0.738 17.890 0.738 16.97 1.00 8/27/96 15:28:23 0.738 17.880 0.828 16.96 10.97 8/27/96 15:28:24 0.928 17.880 0.828 16.96 1.00 8/27/96 15:28:31 0.876 17.883 0.781 16.96 1.00 8/27/96 15:28:31 0.876 17.883 0.781 16.96 1.00 8/27/96 15:28:34 0.928 17.880 0.828 16.96 1.00 8/27/96 15:28:34 0.928 17.880 0.828 16.96 1.00 8/27/96 15:28:34 0.928 17.880 0.828 16.96 1.00 8/27/96 15:28:34 0.928 17.880 0.828 16.96 1.00 8/27/96 15:28:34 0.928 17.871 0.928 16.95 0.99 8/27/96 15:28:41 1.041 17.864 1.041 16.94 0.99 8/27/96 15:28:45 1.103 17.860 1.103 16.94 0.99 8/27/96 15:28:45 1.103 17.860 1.103 16.94 0.99 8/27/96 15:29:02 1.390 17.839 1.390 16.92 0.99 8/27/96 15:29:02 1.390 17.839 1.390 16.92 0.99 8/27/96 15:29:02 1.390 17.839 1.390 16.92 0.99 8/27/96 15:29:03 1.856 17.802 1.655 16.90 0.99 8/27/96 15:29:04 1.655 17.820 1.655 16.90 0.99 8/27/96 15:29:07 1.473 17.844 1.473 16.91 0.99 8/27/96 15:29:07 1.473 17.846 1.311 16.93 0.99 8/27/96 15:29:07 1.473 17.846 1.311 16.93 0.99 8/27/96 15:29:07 1.473 17.846 1.311 16.93 0.99 8/27/96 15:29:07 1.473 17.846 1.311 16.93 0.99 8/27/96 15:29:07 1.473 17.846 1.311 16.93 0.99 8/27/96 15:29:07 1.473 17.846 1.311 16.93 0.99 8/27/96 15:29:07 1.473 17.846 1.311 16.93 0.99 8/27/96 15:29:07 1.473 17.846 1.311 16.95 0.99 8/27/96 15:29:07 1.473 17.662 1.665 16.90 0.99 8/27/96 15:29:07 1.473 17.66					0.315	17.00	1.00
8/27/96         15:28:00         0.353         17.922         0.353         17.00         1.00           8/27/96         15:28:01         0.396         17.917         0.396         17.00         1.00           8/27/96         15:28:04         0.420         17.915         0.420         17.00         1.00           8/27/96         15:28:05         0.445         17.913         0.445         16:99         1.00           8/27/96         15:28:08         0.445         17.910         0.470         16:99         1.00           8/27/96         15:28:08         0.496         17.908         0.496         18.99         1.00           8/27/96         15:28:10         0.525         17.906         0.525         16:99         1.00           8/27/96         15:28:14         0.586         17.901         0.586         16:99         1.00           8/27/96         15:28:16         0.621         17.897         0.621         16:98         1.0           8/27/96         15:28:23         0.686         17.897         0.621         16:98         1.0           8/27/96         15:28:23         0.738         17.890         0.738         16:97         1.0			0.333	17.924		17.00	1.00
8/27/96         15:28:02         0.396         17.917         0.396         17.00         1.00           8/27/96         15:28:05         0.445         17.913         0.420         17.00         1.00           8/27/96         15:28:05         0.445         17.913         0.445         16:99         1.00           8/27/96         15:28:08         0.496         17.908         0.496         16:99         1.00           8/27/96         15:28:10         0.525         17.906         0.525         16:99         1.00           8/27/96         15:28:14         0.566         17.901         0.586         16:99         1.00           8/27/96         15:28:18         0.668         17.897         0.621         16:98         1.0           8/27/96         15:28:18         0.668         17.894         0.658         16.97         1.0           8/27/96         15:28:20         0.696         17.892         0.696         16.97         1.0           8/27/96         15:28:23         0.738         17.880         0.781         16.96         1.0           8/27/96         15:28:28         0.828         17.880         0.828         16.97         1.0	8/27/96	15:28:00	0.353	17.922	0.353	17.00	1.00
8/27/96         15:28:04         0.420         17:915         0.420         17:00         1.00           8/27/96         15:28:05         0.445         17:913         0.445         16:99         1.00           8/27/96         15:28:08         0.496         17:908         0.496         16:99         1.00           8/27/96         15:28:10         0.525         17:906         0.525         16:99         1.00           8/27/96         15:28:14         0.566         17:901         0.555         16:98         1.00           8/27/96         15:28:16         0.586         17:901         0.586         16:98         1.00           8/27/96         15:28:18         0.586         17:901         0.586         16:98         1.00           8/27/96         15:28:18         0.688         17:897         0.621         16:98         1.00           8/27/96         15:28:23         0.738         17:890         0.738         16:97         1.0           8/27/96         15:28:23         0.781         17:883         0.781         16:98         1.0           8/27/96         15:28:24         0.828         17:890         0.738         16:97         1.0	8/27/96	15:28:01	0.374	17.920	0.374	17.00	1.00
8/27/96         15:28:05         0.445         17.913         0.445         16.99         1.00           8/27/96         15:28:07         0.470         17.910         0.470         16.99         1.00           8/27/96         15:28:10         0.525         17.906         0.525         16.99         1.00           8/27/96         15:28:12         0.555         17.903         0.555         16.98         1.00           8/27/96         15:28:14         0.586         17.901         0.586         16.98         1.00           8/27/96         15:28:18         0.651         17.897         0.621         16.98         1.00           8/27/96         15:28:20         0.696         17.892         0.696         16.97         1.0           8/27/96         15:28:23         0.738         17.890         0.738         16.97         1.0           8/27/96         15:28:25         0.781         17.883         0.781         16.96         1.0           8/27/96         15:28:31         0.876         17.878         0.876         16.96         1.0           8/27/96         15:28:33         0.983         17.860         0.898         16.96         1.0	8/27/96	15:28:02	0.396	17.917	0.396	17.00	1.00
8/27/96         15:28:07         0.470         17.910         0.470         16.99         1.00           8/27/96         15:28:08         0.496         17.908         0.496         16.99         1.00           8/27/96         15:28:10         0.525         17.906         0.525         16.99         1.00           8/27/96         15:28:12         0.555         17.901         0.586         16.98         1.00           8/27/96         15:28:16         0.621         17.897         0.621         16.98         1.00           8/27/96         15:28:18         0.658         17.894         0.658         16.97         1.0           8/27/96         15:28:23         0.738         17.892         0.696         16.97         1.0           8/27/96         15:28:23         0.738         17.892         0.696         16.97         1.0           8/27/96         15:28:23         0.781         17.883         0.781         16.96         1.0           8/27/96         15:28:24         0.828         17.878         0.876         16.96         1.0           8/27/96         15:28:31         0.876         17.878         0.876         16.96         1.0	8/27/96	15:28:04	0.420	17.915	0.420	17.00	1.00
8/27/96         15:28:08         0.496         17.908         0.496         16:99         1.00           8/27/96         15:28:10         0.525         17:906         0.525         16:99         1.00           8/27/96         15:28:14         0.586         17:901         0.555         16:98         1.00           8/27/96         15:28:16         0.621         17:897         0.621         16:98         1.00           8/27/96         15:28:18         0.658         17:897         0.621         16:98         1.00           8/27/96         15:28:20         0.696         17:892         0.696         16:97         1.00           8/27/96         15:28:23         0.738         17:890         0.738         16:97         1.00           8/27/96         15:28:25         0.781         17:883         0.781         16:96         1.0           8/27/96         15:28:25         0.781         17:883         0.781         16:96         1.0           8/27/96         15:28:34         0.928         17:878         0.876         16:96         1.0           8/27/96         15:28:41         1.041         17:869         0.983         16:95         0.9	8/27/96	15:28:05	0.445	17.913	0.445	16.99	1.00
8/27/96         15:28:10         0.525         17.906         0.525         16.99         1.00           8/27/96         15:28:12         0.555         17.903         0.555         16.98         1.00           8/27/96         15:28:16         0.586         17.901         0.586         16.98         1.00           8/27/96         15:28:18         0.658         17.897         0.621         16.98         1.00           8/27/96         15:28:20         0.896         17.892         0.696         16.97         1.00           8/27/96         15:28:23         0.738         17.890         0.738         16.97         1.00           8/27/96         15:28:25         0.781         17.880         0.781         16.96         1.00           8/27/96         15:28:28         0.828         17.878         0.876         16.96         1.0           8/27/96         15:28:34         0.928         17.871         0.928         16.95         0.9           8/27/96         15:28:37         0.983         17.869         0.983         16.95         0.9           8/27/96         15:28:41         1.041         17.864         1.041         16.94         0.9	8/27/96	15:28:07	0.470	17.910	0.470	16.99	1.00
8/27/96	8/27/96	15:28:08	0.496	17.908	0.496	16.99	1.00
8/27/96         15:28:14         0.586         17:901         0.586         16.98         1.00           8/27/96         15:28:16         0.621         17.897         0.621         16:98         1.00           8/27/96         15:28:18         0.658         17.894         0.658         16:97         1.00           8/27/96         15:28:20         0.696         17.892         0.696         16:97         1.00           8/27/96         15:28:25         0.781         17.883         0.781         16:96         1.00           8/27/96         15:28:28         0.828         17.880         0.828         16:96         1.00           8/27/96         15:28:31         0.876         17.878         0.876         16:96         1.00           8/27/96         15:28:34         0.928         17.871         0.928         16:95         0.99           8/27/96         15:28:37         0.983         17.869         0.983         16:95         0.99           8/27/96         15:28:41         1.041         17.864         1.041         16:94         0.99           8/27/96         15:28:49         1.168         17.855         1.168         16:94         0.99	8/27/96	15:28:10	0.525	17.906	0.525	16.99	1.00
8/27/96         15:28:16         0.621         17.897         0.621         16.98         1.00           8/27/96         15:28:18         0.658         17.894         0.658         16.97         1.00           8/27/96         15:28:20         0.696         17.892         0.696         16.97         1.00           8/27/96         15:28:23         0.738         17.890         0.738         16.96         1.00           8/27/96         15:28:28         0.828         17.880         0.828         16.96         1.00           8/27/96         15:28:34         0.826         17.878         0.876         16.96         1.00           8/27/96         15:28:37         0.983         17.871         0.928         16.95         0.99           8/27/96         15:28:41         1.041         17.864         1.041         16.94         0.99           8/27/96         15:28:45         1.103         17.860         1.103         16.94         0.99           8/27/96         15:28:49         1.168         17.855         1.168         16.94         0.99           8/27/96         15:28:53         1.238         17.850         1.238         16.93         0.99	8/27/96	15:28:12	0.555	17.903	0.555	16.98	1.00
8/27/96         15:28:18         0.658         17.894         0.658         16.97         1.00           8/27/96         15:28:20         0.696         17.892         0.696         16.97         1.01           8/27/96         15:28:23         0.738         17.890         0.738         16.97         1.00           8/27/96         15:28:28         0.828         17.883         0.781         16.96         1.00           8/27/96         15:28:31         0.876         17.878         0.876         16.96         1.00           8/27/96         15:28:34         0.928         17.871         0.928         16.95         0.99           8/27/96         15:28:41         1.041         17.864         1.041         16.94         0.99           8/27/96         15:28:45         1.103         17.869         1.103         16.94         0.99           8/27/96         15:28:49         1.168         17.855         1.168         16.94         0.99           8/27/96         15:29:02         1.390         17.839         1.390         16.92         0.99           8/27/96         15:29:02         1.390         17.834         1.473         16.91         0.99	8/27/96	15:28:14	0.586	17.901	0.586	16.98	1.00
8/27/96         15:28:20         0.696         17.892         0.696         16:97         1.00           8/27/96         15:28:23         0.738         17.890         0.738         16.97         1.01           8/27/96         15:28:28         0.828         17.880         0.828         16.96         1.00           8/27/96         15:28:31         0.876         17.878         0.876         16.96         1.00           8/27/96         15:28:37         0.983         17.869         0.983         16.95         0.99           8/27/96         15:28:41         1.041         17.864         1.041         16.94         0.99           8/27/96         15:28:45         1.103         17.860         1.103         16.94         0.99           8/27/96         15:28:49         1.168         17.855         1.131         16.94         0.99           8/27/96         15:28:53         1.238         17.855         1.311         16.93         0.99           8/27/96         15:29:02         1.390         17.839         1.390         16.93         0.99           8/27/96         15:29:12         1.561         17.827         1.561         16.90         0.99	8/27/96	15:28:16	0.621	17.897	0.621	16.98	1.00
8/27/96         15:28:23         0.738         17.890         0.738         16.97         1.00           8/27/96         15:28:25         0.781         17.883         0.781         16.96         1.01           8/27/96         15:28:28         0.828         17.880         0.828         16.96         1.00           8/27/96         15:28:34         0.928         17.871         0.928         16.95         0.99           8/27/96         15:28:34         0.928         17.869         0.983         16.95         0.99           8/27/96         15:28:41         1.041         17.860         1.03         16.94         0.99           8/27/96         15:28:49         1.168         17.855         1.168         16.94         0.99           8/27/96         15:28:53         1.238         17.855         1.238         16.93         0.99           8/27/96         15:28:57         1.311         17.846         1.311         16.93         0.99           8/27/96         15:29:02         1.390         17.839         1.390         16.92         0.99           8/27/96         15:29:07         1.473         17.834         1.473         16.91         0.99	8/27/96	15:28:18	0.658	17.894		16.97	1.00
8/27/96         15:28:25         0.781         17.883         0.781         16.96         1.00           8/27/96         15:28:28         0.828         17.878         0.876         16.96         1.00           8/27/96         15:28:31         0.876         17.878         0.876         16.96         1.00           8/27/96         15:28:34         0.928         17.871         0.928         16.95         0.93           8/27/96         15:28:41         1.041         17.869         0.983         16.95         0.98           8/27/96         15:28:45         1.03         17.860         1.103         16.94         0.99           8/27/96         15:28:45         1.103         17.855         1.168         16.94         0.99           8/27/96         15:28:53         1.238         17.850         1.238         16.93         0.99           8/27/96         15:28:51         1.311         17.846         1.311         16.93         0.99           8/27/96         15:29:02         1.390         17.839         1.390         16.92         0.99           8/27/96         15:29:12         1.561         17.827         1.561         16.91         0.99	8/27/96	15:28:20	0.696	17.892	0.696	16.97	1.00
8/27/96         15:28:28         0.828         17.880         0.828         16.96         1.00           8/27/96         15:28:31         0.876         17.878         0.876         16.96         1.01           8/27/96         15:28:34         0.928         17.871         0.928         16.95         0.93           8/27/96         15:28:37         0.983         17.869         0.983         16.95         0.93           8/27/96         15:28:41         1.041         17.864         1.041         16.94         0.99           8/27/96         15:28:45         1.103         17.860         1.103         16.94         0.99           8/27/96         15:28:53         1.238         17.855         1.168         16.94         0.99           8/27/96         15:28:57         1.311         17.846         1.311         16.93         0.99           8/27/96         15:29:02         1.390         17.839         1.390         16.92         0.99           8/27/96         15:29:07         1.473         17.834         1.473         16.91         0.99           8/27/96         15:29:12         1.561         17.827         1.561         16.91         0.99	8/27/96	15:28:23	0.738	17.890	0.738	16.97	1.00
8/27/96         15:28:31         0.876         17.878         0.876         16.96         1.00           8/27/96         15:28:34         0.928         17.871         0.928         16.95         0.99           8/27/96         15:28:37         0.983         17.869         0.983         16.95         0.99           8/27/96         15:28:41         1.041         17.860         1.041         16.94         0.99           8/27/96         15:28:45         1.103         17.860         1.103         16.94         0.99           8/27/96         15:28:53         1.238         17.855         1.168         16.94         0.9           8/27/96         15:28:53         1.238         17.850         1.238         16.93         0.9           8/27/96         15:29:02         1.390         17.839         1.390         16.92         0.9           8/27/96         15:29:07         1.473         17.834         1.473         16.91         0.9           8/27/96         15:29:12         1.561         17.827         1.561         16.91         0.9           8/27/96         15:29:13         1.655         17.820         1.655         16.90         0.9	8/27/96	15:28:25		17.883	0.781		1.00
8/27/96         15:28:34         0.928         17.871         0.928         16.95         0.98           8/27/96         15:28:37         0.983         17.869         0.983         16.95         0.98           8/27/96         15:28:41         1.041         17.864         1.041         16.94         0.99           8/27/96         15:28:49         1.168         17.855         1.168         16.94         0.99           8/27/96         15:28:53         1.238         17.850         1.238         16.93         0.99           8/27/96         15:28:57         1.311         17.846         1.311         16.93         0.99           8/27/96         15:28:57         1.311         17.846         1.311         16.93         0.99           8/27/96         15:29:02         1.390         17.839         1.390         16.92         0.99           8/27/96         15:29:12         1.561         17.827         1.561         16.91         0.99           8/27/96         15:29:12         1.561         17.827         1.561         16.91         0.99           8/27/96         15:29:13         1.655         17.820         1.655         16.90         0.99	8/27/96	15:28:28	0.828				1.00
8/27/96         15:28:37         0.983         17.869         0.983         16.95         0.98           8/27/96         15:28:41         1.041         17.864         1.041         16.94         0.99           8/27/96         15:28:45         1.103         17.860         1.103         16.94         0.99           8/27/96         15:28:53         1.238         17.850         1.238         16.93         0.99           8/27/96         15:28:57         1.311         17.846         1.311         16.93         0.99           8/27/96         15:29:02         1.390         17.839         1.390         16.92         0.99           8/27/96         15:29:02         1.390         17.839         1.390         16.92         0.99           8/27/96         15:29:12         1.561         17.827         1.561         16.91         0.99           8/27/96         15:29:18         1.655         17.820         1.655         16.90         0.99           8/27/96         15:29:24         1.753         17.813         1.753         16.89         0.99           8/27/96         15:29:30         1.858         17.807         1.858         16.89         0.99	8/27/96			1			1.00
8/27/96         15:28:41         1.041         17.864         1.041         16.94         0.98           8/27/96         15:28:45         1.103         17.860         1.103         16.94         0.98           8/27/96         15:28:49         1.168         17.855         1.168         16.94         0.98           8/27/96         15:28:53         1.238         17.850         1.238         16.93         0.99           8/27/96         15:28:57         1.311         17.846         1.311         16.93         0.99           8/27/96         15:29:02         1.390         17.839         1.390         16.92         0.99           8/27/96         15:29:12         1.561         17.827         1.561         16.91         0.98           8/27/96         15:29:18         1.655         17.820         1.655         16.90         0.98           8/27/96         15:29:30         1.858         17.807         1.858         16.89         0.99           8/27/96         15:29:37         1.968         17.797         1.968         16.87         0.98           8/27/96         15:29:51         2.210         17.783         2.210         16.86         0.99	8/27/96	15:28:34			1 1		0.99
8/27/96         15:28:45         1.103         17.860         1.103         16.94         0.99           8/27/96         15:28:49         1.168         17.855         1.168         16.94         0.99           8/27/96         15:28:53         1.238         17.850         1.238         16.93         0.99           8/27/96         15:28:57         1.311         17.846         1.311         16.93         0.99           8/27/96         15:29:02         1.390         17.839         1.390         16.92         0.99           8/27/96         15:29:07         1.473         17.834         1.473         16.91         0.99           8/27/96         15:29:12         1.561         17.827         1.561         16.91         0.99           8/27/96         15:29:18         1.655         17.820         1.655         16.90         0.99           8/27/96         15:29:24         1.753         17.813         1.753         16.89         0.99           8/27/96         15:29:37         1.968         17.797         1.968         16.89         0.99           8/27/96         15:29:51         2.210         17.783         2.210         16.86         0.99	8/27/96						0.99
8/27/96         15:28:49         1.168         17.855         1.168         16.94         0.99           8/27/96         15:28:53         1.238         17.850         1.238         16.93         0.99           8/27/96         15:28:57         1.311         17.846         1.311         16.93         0.99           8/27/96         15:29:02         1.390         17.839         1.390         16.92         0.99           8/27/96         15:29:12         1.561         17.827         1.561         16.91         0.99           8/27/96         15:29:18         1.655         17.820         1.655         16.90         0.99           8/27/96         15:29:18         1.655         17.820         1.655         16.90         0.99           8/27/96         15:29:30         1.858         17.807         1.858         16.89         0.99           8/27/96         15:29:37         1.968         17.797         1.968         16.88         0.99           8/27/96         15:29:51         2.210         17.783         2.210         16.86         0.99           8/27/96         15:30:07         2.481         17.765         2.481         16.85         0.99							0.99
8/27/96         15:28:53         1.238         17.850         1.238         16.93         0.98           8/27/96         15:28:57         1.311         17.846         1.311         16.93         0.98           8/27/96         15:29:02         1.390         17.839         1.390         16.92         0.98           8/27/96         15:29:07         1.473         17.834         1.473         16.91         0.98           8/27/96         15:29:12         1.561         17.827         1.561         16.91         0.98           8/27/96         15:29:18         1.655         17.820         1.655         16.90         0.98           8/27/96         15:29:30         1.858         17.807         1.858         16.89         0.98           8/27/96         15:29:37         1.968         17.797         1.968         16.88         0.99           8/27/96         15:29:37         1.968         17.790         2.085         16.87         0.98           8/27/96         15:29:51         2.210         17.783         2.210         16.86         0.99           8/27/96         15:30:07         2.481         17.765         2.481         16.85         0.98							0.99
8/27/96         15:28:57         1.311         17.846         1.311         16.93         0.98           8/27/96         15:29:02         1.390         17.839         1.390         16.92         0.98           8/27/96         15:29:07         1.473         17.834         1.473         16.91         0.98           8/27/96         15:29:12         1.561         17.827         1.561         16.91         0.98           8/27/96         15:29:18         1.655         17.820         1.655         16.90         0.98           8/27/96         15:29:24         1.753         17.813         1.753         16.89         0.98           8/27/96         15:29:30         1.858         17.807         1.968         16.89         0.98           8/27/96         15:29:37         1.968         17.797         1.968         16.89         0.99           8/27/96         15:29:51         2.210         17.783         2.210         16.86         0.99           8/27/96         15:29:59         2.341         17.774         2.341         16.85         0.99           8/27/96         15:30:16         2.630         17.754         2.630         16.83         0.99							0.99
8/27/96         15:29:02         1.390         17.839         1.390         16.92         0.98           8/27/96         15:29:07         1.473         17.834         1.473         16.91         0.98           8/27/96         15:29:12         1.561         17.827         1.561         16.91         0.98           8/27/96         15:29:18         1.655         17.820         1.655         16.90         0.98           8/27/96         15:29:24         1.753         17.813         1.753         16.89         0.98           8/27/96         15:29:30         1.858         17.807         1.858         16.89         0.98           8/27/96         15:29:37         1.968         17.797         1.968         16.88         0.99           8/27/96         15:29:37         1.968         17.790         2.085         16.87         0.98           8/27/96         15:29:51         2.210         17.783         2.210         16.86         0.99           8/27/96         15:30:55         2.341         17.774         2.341         16.85         0.98           8/27/96         15:30:16         2.630         17.754         2.630         16.83         0.98	1						
8/27/96         15:29:07         1.473         17.834         1.473         16.91         0.98           8/27/96         15:29:12         1.561         17.827         1.561         16.91         0.98           8/27/96         15:29:18         1.655         17.820         1.655         16.90         0.98           8/27/96         15:29:24         1.753         17.813         1.753         16.89         0.98           8/27/96         15:29:37         1.968         17.807         1.858         16.89         0.98           8/27/96         15:29:37         1.968         17.797         1.968         16.88         0.98           8/27/96         15:29:37         1.968         17.790         2.085         16.87         0.98           8/27/96         15:29:51         2.210         17.783         2.210         16.86         0.99           8/27/96         15:29:59         2.341         17.774         2.341         16.85         0.99           8/27/96         15:30:16         2.630         17.754         2.481         16.85         0.99           8/27/96         15:30:26         2.786         17.744         2.786         16.82         0.99							
8/27/96         15:29:12         1.561         17.827         1.561         16.91         0.98           8/27/96         15:29:18         1.655         17.820         1.655         16.90         0.98           8/27/96         15:29:24         1.753         17.813         1.753         16.89         0.98           8/27/96         15:29:30         1.858         17.807         1.858         16.89         0.98           8/27/96         15:29:37         1.968         17.797         1.968         16.88         0.98           8/27/96         15:29:44         2.085         17.790         2.085         16.87         0.98           8/27/96         15:29:51         2.210         17.783         2.210         16.86         0.99           8/27/96         15:30:07         2.481         17.774         2.341         16.85         0.98           8/27/96         15:30:16         2.630         17.754         2.630         16.83         0.98           8/27/96         15:30:26         2.786         17.744         2.786         16.82         0.98           8/27/96         15:30:36         2.953         17.730         2.953         16.81         0.98					1 1		
8/27/96         15:29:18         1.655         17.820         1.655         16.90         0.98           8/27/96         15:29:24         1.753         17.813         1.753         16.89         0.98           8/27/96         15:29:30         1.858         17.807         1.858         16.89         0.98           8/27/96         15:29:37         1.968         17.797         1.968         16.88         0.98           8/27/96         15:29:44         2.085         17.790         2.085         16.87         0.98           8/27/96         15:29:51         2.210         17.783         2.210         16.86         0.99           8/27/96         15:29:59         2.341         17.774         2.341         16.85         0.99           8/27/96         15:30:07         2.481         17.765         2.481         16.85         0.99           8/27/96         15:30:26         2.786         17.744         2.786         16.83         0.99           8/27/96         15:30:36         2.953         17.730         2.953         16.81         0.99           8/27/96         15:30:46         3.130         17.721         3.130         16.70         0.99							
8/27/96         15:29:24         1.753         17.813         1.753         16.89         0.98           8/27/96         15:29:30         1.858         17.807         1.858         16.89         0.98           8/27/96         15:29:37         1.968         17.797         1.968         16.88         0.98           8/27/96         15:29:44         2.085         17.790         2.085         16.87         0.98           8/27/96         15:29:51         2.210         17.783         2.210         16.86         0.98           8/27/96         15:29:59         2.341         17.774         2.341         16.85         0.98           8/27/96         15:30:07         2.481         17.765         2.481         16.85         0.98           8/27/96         15:30:16         2.630         17.754         2.630         16.83         0.98           8/27/96         15:30:26         2.786         17.744         2.786         16.82         0.98           8/27/96         15:30:36         2.953         17.730         2.953         16.81         0.98           8/27/96         15:31:09         3.515         17.696         3.515         16.78         0.98							
8/27/96         15:29:30         1.858         17.807         1.858         16.89         0.98           8/27/96         15:29:37         1.968         17.797         1.968         16.88         0.98           8/27/96         15:29:44         2.085         17.790         2.085         16.87         0.98           8/27/96         15:29:51         2.210         17.783         2.210         16.86         0.98           8/27/96         15:29:59         2.341         17.774         2.341         16.85         0.98           8/27/96         15:30:07         2.481         17.765         2.481         16.85         0.98           8/27/96         15:30:16         2.630         17.754         2.630         16.83         0.98           8/27/96         15:30:26         2.786         17.744         2.786         16.82         0.98           8/27/96         15:30:36         2.953         17.730         2.953         16.81         0.98           8/27/96         15:30:57         3.316         17.707         3.316         16.79         0.98           8/27/96         15:31:22         3.725         17.682         3.725         16.76         0.98			i I				
8/27/96         15:29:37         1.968         17.797         1.968         16.88         0.98           8/27/96         15:29:44         2.085         17.790         2.085         16.87         0.98           8/27/96         15:29:51         2.210         17.783         2.210         16.86         0.98           8/27/96         15:29:59         2.341         17.774         2.341         16.85         0.98           8/27/96         15:30:07         2.481         17.765         2.481         16.85         0.98           8/27/96         15:30:16         2.630         17.754         2.630         16.83         0.98           8/27/96         15:30:26         2.786         17.744         2.786         16.82         0.98           8/27/96         15:30:36         2.953         17.730         2.953         16.81         0.98           8/27/96         15:30:46         3.130         17.721         3.130         16.80         0.98           8/27/96         15:31:09         3.515         17.696         3.515         16.78         0.98           8/27/96         15:31:35         3.946         17.668         3.946         16.75         0.98							
8/27/96         15:29:44         2.085         17.790         2.085         16.87         0.98           8/27/96         15:29:51         2.210         17.783         2.210         16.86         0.98           8/27/96         15:29:59         2.341         17.774         2.341         16.85         0.98           8/27/96         15:30:07         2.481         17.765         2.481         16.85         0.98           8/27/96         15:30:16         2.630         17.754         2.630         16.83         0.98           8/27/96         15:30:26         2.786         17.744         2.786         16.82         0.98           8/27/96         15:30:36         2.953         17.730         2.953         16.81         0.98           8/27/96         15:30:46         3.130         17.721         3.130         16.80         0.98           8/27/96         15:31:09         3.515         17.696         3.515         16.78         0.98           8/27/96         15:31:35         3.946         17.668         3.946         16.75         0.98           8/27/96         15:31:49         4.181         17.652         4.181         16.72         0.98							
8/27/96         15:29:51         2.210         17.783         2.210         16.86         0.99           8/27/96         15:29:59         2.341         17.774         2.341         16.85         0.99           8/27/96         15:30:07         2.481         17.765         2.481         16.85         0.99           8/27/96         15:30:16         2.630         17.754         2.630         16.83         0.99           8/27/96         15:30:26         2.786         17.744         2.786         16.82         0.99           8/27/96         15:30:36         2.953         17.730         2.953         16.81         0.99           8/27/96         15:30:46         3.130         17.721         3.130         16.80         0.99           8/27/96         15:31:09         3.515         17.696         3.515         16.78         0.99           8/27/96         15:31:35         3.946         17.668         3.946         16.75         0.99           8/27/96         15:31:49         4.181         17.652         4.181         16.73         0.99           8/27/96         15:32:20         4.693         17.620         4.693         16.70         0.99							
8/27/96         15:29:59         2.341         17.774         2.341         16.85         0.98           8/27/96         15:30:07         2.481         17.765         2.481         16.85         0.98           8/27/96         15:30:16         2.630         17.754         2.630         16.83         0.98           8/27/96         15:30:26         2.786         17.744         2.786         16.82         0.98           8/27/96         15:30:36         2.953         17.730         2.953         16.81         0.98           8/27/96         15:30:46         3.130         17.721         3.130         16.80         0.98           8/27/96         15:31:09         3.515         17.696         3.515         16.78         0.98           8/27/96         15:31:22         3.725         17.682         3.725         16.76         0.98           8/27/96         15:31:49         4.181         17.652         4.181         16.73         0.98           8/27/96         15:32:20         4.693         17.620         4.693         16.70         0.98							
8/27/96         15:30:07         2.481         17.765         2.481         16.85         0.98           8/27/96         15:30:16         2.630         17.754         2.630         16.83         0.98           8/27/96         15:30:26         2.786         17.744         2.786         16.82         0.98           8/27/96         15:30:36         2.953         17.730         2.953         16.81         0.98           8/27/96         15:30:46         3.130         17.721         3.130         16.80         0.98           8/27/96         15:30:57         3.316         17.707         3.316         16.79         0.98           8/27/96         15:31:09         3.515         17.696         3.515         16.78         0.98           8/27/96         15:31:35         3.946         17.668         3.946         16.75         0.98           8/27/96         15:31:49         4.181         17.652         4.181         16.72         0.98           8/27/96         15:32:20         4.693         17.620         4.693         16.70         0.98							
8/27/96         15:30:16         2.630         17.754         2.630         16.83         0.98           8/27/96         15:30:26         2.786         17.744         2.786         16.82         0.98           8/27/96         15:30:36         2.953         17.730         2.953         16.81         0.98           8/27/96         15:30:46         3.130         17.721         3.130         16.80         0.98           8/27/96         15:30:57         3.316         17.707         3.316         16.79         0.98           8/27/96         15:31:09         3.515         17.696         3.515         16.78         0.98           8/27/96         15:31:22         3.725         17.682         3.725         16.76         0.98           8/27/96         15:31:49         4.181         17.652         4.181         16.73         0.98           8/27/96         15:32:04         4.430         17.638         4.430         16.72         0.98           8/27/96         15:32:20         4.693         17.620         4.693         16.70         0.98							
8/27/96         15:30:26         2.786         17.744         2.786         16.82         0.98           8/27/96         15:30:36         2.953         17.730         2.953         16.81         0.98           8/27/96         15:30:46         3.130         17.721         3.130         16.80         0.98           8/27/96         15:30:57         3.316         17.707         3.316         16.79         0.98           8/27/96         15:31:09         3.515         17.696         3.515         16.78         0.98           8/27/96         15:31:22         3.725         17.682         3.725         16.76         0.98           8/27/96         15:31:35         3.946         17.668         3.946         16.75         0.98           8/27/96         15:31:49         4.181         17.652         4.181         16.73         0.98           8/27/96         15:32:04         4.430         17.638         4.430         16.72         0.98           8/27/96         15:32:20         4.693         17.620         4.693         16.70         0.98							0.99
8/27/96         15:30:36         2.953         17.730         2.953         16.81         0.98           8/27/96         15:30:46         3.130         17.721         3.130         16.80         0.98           8/27/96         15:30:57         3.316         17.707         3.316         16.79         0.98           8/27/96         15:31:09         3.515         17.696         3.515         16.78         0.98           8/27/96         15:31:22         3.725         17.682         3.725         16.76         0.98           8/27/96         15:31:35         3.946         17.668         3.946         16.75         0.98           8/27/96         15:31:49         4.181         17.652         4.181         16.73         0.98           8/27/96         15:32:04         4.430         17.638         4.430         16.72         0.98           8/27/96         15:32:20         4.693         17.620         4.693         16.70         0.98							
8/27/96         15:30:46         3.130         17.721         3.130         16.80         0.98           8/27/96         15:30:57         3.316         17.707         3.316         16.79         0.98           8/27/96         15:31:09         3.515         17.696         3.515         16.78         0.98           8/27/96         15:31:22         3.725         17.682         3.725         16.76         0.98           8/27/96         15:31:35         3.946         17.668         3.946         16.75         0.98           8/27/96         15:31:49         4.181         17.652         4.181         16.73         0.98           8/27/96         15:32:04         4.430         17.638         4.430         16.72         0.98           8/27/96         15:32:20         4.693         17.620         4.693         16.70         0.98							0.99
8/27/96         15:30:57         3.316         17.707         3.316         16.79         0.98           8/27/96         15:31:09         3.515         17.696         3.515         16.78         0.98           8/27/96         15:31:22         3.725         17.682         3.725         16.76         0.98           8/27/96         15:31:35         3.946         17.668         3.946         16.75         0.98           8/27/96         15:31:49         4.181         17.652         4.181         16.73         0.98           8/27/96         15:32:04         4.430         17.638         4.430         16.72         0.98           8/27/96         15:32:20         4.693         17.620         4.693         16.70         0.98					1 1		0.99
8/27/96         15:31:09         3.515         17.696         3.515         16.78         0.98           8/27/96         15:31:22         3.725         17.682         3.725         16.76         0.98           8/27/96         15:31:35         3.946         17.668         3.946         16.75         0.98           8/27/96         15:31:49         4.181         17.652         4.181         16.73         0.98           8/27/96         15:32:04         4.430         17.638         4.430         16.72         0.98           8/27/96         15:32:20         4.693         17.620         4.693         16.70         0.98							0.99
8/27/96     15:31:22     3.725     17.682     3.725     16.76     0.96       8/27/96     15:31:35     3.946     17.668     3.946     16.75     0.96       8/27/96     15:31:49     4.181     17.652     4.181     16.73     0.96       8/27/96     15:32:04     4.430     17.638     4.430     16.72     0.96       8/27/96     15:32:20     4.693     17.620     4.693     16.70     0.96							0.98
8/27/96     15;31:35     3.946     17.668     3.946     16.75     0.98       8/27/96     15;31:49     4.181     17.652     4.181     16.73     0.98       8/27/96     15;32:04     4.430     17.638     4.430     16.72     0.98       8/27/96     15;32:20     4.693     17.620     4.693     16.70     0.98							0.98
8/27/96     15:31:49     4.181     17.652     4.181     16.73     0.98       8/27/96     15:32:04     4.430     17.638     4.430     16.72     0.98       8/27/96     15:32:20     4.693     17.620     4.693     16.70     0.98							0.98
8/27/96     15:32:04     4.430     17.638     4.430     16.72     0.90       8/27/96     15:32:20     4.693     17.620     4.693     16.70     0.90							0.98
8/27/96 15:32:20 4.693 17.620 4.693 16.70 0.9			1				0.98
							0.98
						16.68	0.98
					5.270		0.98
					5.583		0.98
		15:33:33	5.915			16.62	0.98
8/27/96 15:33:54 6.266 17.521 6.266 16.60 0.9	8/27/96	15:33:54	6.266			16.60	0.97
		15:34:17	6.640	17.497	6.640	16.58	0.97
8/27/96 15:34:41 7.035 17.474 7.035 16.55 0.9	8/27/96		7.035	17.474			0.97
8/27/96 15:35:06 7.453 17.447 7.453 16.53 0.9	8/27/96	15:35:06	7.453	17.447	7.453	16.53	0.97

DATE	TIME	EVENT	DEPTH TO	TEST	HEAD	HEAD
		ELAPSED	WATER	ELAPSED		RATIO
		TIME		TIME	*	
	(HR:M:S)	(MIN)	(FEET)	(MIN)	(FEET)	
8/27/96	15:35:32	7.896	17.419		16.50	0.97
8/27/96	15:36:00	8.366	17.391	8.366	16.47	0.97
8/27/96	15:36:30	8.865	17.361	8.865	16.44	0.96
8/27/96	15:37:02	9.391	17.329	9.391	16.41	0.96
8/27/96	15:37:35	9.950	17.290	9.950	16.37	0.96
8/27/96	15:38:11	10.541	17.255	10.541	16.34	0.96
8/27/96	15:38:49	11.168	17.216	11.168	16.30	0.96
8/27/96	15:39:28	11.831	17.179		16.26	0.95
8/27/96	15:40:11	12.535	17.135	12.535	16.22	0.95
8/27/96	15:40:55	13.280	17.091	13.280	16.17	0.95
8/27/96	15:41:43	14.070	17.045	14.070	16.13	0.95
8/27/96	15:42:33	14.906	16.995	14.906	16.08	0.94
8/27/96	15:43:26	15.791	16.942	15.791	16.02	0.94
8/27/96	15:44:22	16.730	16.889	16.730	15.97	0.94
8/27/96	15:45:22	17.723	16.831	17.723	15.91	0.93
8/27/96	15:46:25	18.776	16.769	18.776	15.85	0.93 0.93
8/27/96	15:47:32	19.891	16.704	19.891	15.78 15.72	0.93
8/27/96	15:48:43	21.073 22.325	16.637 16.563	21.073 22.325	15.72	0.92
8/27/96 8/27/96	15:49:58 15:51:17	22.325	16.363	22.325	15.57	0.92
8/27/96	15:51:17	25.055	16.406	25.050 25.055	15.37	0.91
8/27/96	15:52:42	26.543	16.323	26.543	15.49	0.90
8/27/96	15:55:46	28.118	16.229	28.118	15.31	0.90
8/27/96	15:57:26	29.786	16.139	29.786	15.22	0.89
8/27/96	15:59:12	31.555	16.040	31.555	15.12	0.89
8/27/96	16:01:04	33.428	15.936	33.428	15.02	0.88
8/27/96	16:03:03	35.411	15.827	35.411	14.91	0.87
8/27/96	16:05:09	37.513	15.714	37.513	14.79	0.87
8/27/96	16:07:23	39.740	15.594	39.740	14.67	0.86
8/27/96	16:09:44	42.098	15.470	42.098	14.55	0.85
8/27/96	16:12:14	44.596	15.338	44.596	14.42	0.85
8/27/96	16:14:53	47.243	15.200	47.243	14.28	0.84
8/27/96	16:17:41	50.046	15.055	50.046	14.14	0.83
8/27/96	16:20:39	53.015	14.902	53.015	13.98	0.82
8/27/96	16:23:48	56.160	14.741	56.160	13.82	0.81
8/27/96	16:27:08	59.491	14.575	59.491	13.66	0.80
8/27/96	16:30:40	63.020	14.402	63.020	13.48	0.79
8/27/96	16:34:24	66.758	14.222	66.758	13.30	0.78
8/27/96	16:38:22	70.718	14.028	70.718	13.11	0.77
8/27/96			13.830		1,2.91	0.76
8/27/96	16:47:00	79.355	13.622	79.355	12.70	0.75
8/27/96	16:51:42	84.061	13.410	84.061	12.49	0.73
8/27/96	16:56:41	89.046	13.186	89.046	12.27	0.72
8/27/96	17:01:58	94.326	12.951	94.326	12.03	0.71
8/27/96	17:07:34	99.920	12.707	99.920	11.79	0.69
8/27/96	17:13:29	105.845	12.457	105.845 112.120	11.54	0.68
8/27/96	17:19:46	112.120 118.768	12.199 11.929	112.120	11.28 11.01	0.66 0.65
8/27/96	17:26:25 17:33:27	125,810	11.650	125.810	10.73	0.63
8/27/96 8/27/96	17:33:27	133.268	11.362	133.268	10.73	0.63
8/27/96	17:40:55	141.168	11.066	141.168	10.44	0.60
8/27/96	17:46:49	141.166	10.762	141.100	9.84	0.58
8/27/96	18:06:03	158.401	10.762	158,401	9.53	0.56
8/27/96	18:15:26	167.791	10.431	167.791	9.21	0.54
8/27/96	18:25:23	177.738	9.756	177.738	8.84	0.52
8/27/96	18:35:55	188.275	9.422	188.275	8.50	0.50
8/27/96	18:47:05	199.435	9.085	199.435	8.17	0.48
5,21,00	10.77.00	.50.700	0.000			

DATE	TIME	EVENT	DEPTH TO	TEST	HEAD	HEAD
		ELAPSED	WATER	ELAPSED		RATIO
		TIME		TIME		
	(HR:M:S)	(MIN)	(FEET)	(MIN)	(FEET)	
0/07/00	40.50.54	044.050	0.744	044.050	7.00	0.40
8/27/96	18:58:54	211.256	8.741	211.256	7.82	0.46
8/27/96	19:11:25	223.778	8.395	223.778	7.48	0.44
8/27/96	19:24:41	237.043 251.093	8.045	237.043 251.093	7.13 6.77	0.42 0.40
8/27/96 8/27/96	19:38:44 19:53:37	265.976	7.690 7.337	265,976	6.42	0.40
8/27/96	20:09:23	281.741	6.981	281.741	6.06	0.36
8/27/96	20:26:05	298.440	6.626	298,440	5.71	0.33
8/27/96	20:43:46	316.128	6.276	316,128	5.36	0.31
8/27/96	21:02:30	334.865	5.927	334.865	5.01	0.29
8/27/96	21:22:21	354.711	5.586	354.711	4.67	0.27
8/27/96	21:42:21	374.711	5.268	374.711	4.35	0.26
8/27/96	22:02:21	394.711	4.972	394.711	4.05	0.24
8/27/96	22:22:21	414.711	4.700	414.711	3.78	0.22
8/27/96	22:42:21	434.711	4.446	434.711	3.53	0.21
8/27/96	23:02:21	454.711	4.211	454.711	3.29	0.19
8/27/96	23:22:21	474.711	3.997	474.711	3.08	0.18
8/27/96	23:42:21	494.711	3.800	494.711	2.88	0.17
8/28/96	0:02:21	514.711	3.616	514.711	2.70	0.16
8/28/96	0:22:21	534.711	3.448	534.711	2.53	0.15
8/28/96	0:42:21	554.711	3.293	554.711	2.37	0.14
8/28/96	1:02:21	574.711 504.711	3.145	574.711	2.23 2.10	0.13 0.12
8/28/96 8/28/96	1:22:21 1:42:21	594.711 614.711	3.016 2.894	594.711 614.711	1.97	0.12
8/28/96	2:02:21	634.711	2.094	634,711	1.86	0.12
8/28/96	2:02:21	654.711	2.679	654.711	1.76	0.10
8/28/96	2:42:21	674.711	2.585	674.711	1.67	0.10
8/28/96	3:02:21	694.711	2.502	694.711	1.58	0.09
8/28/96	3:22:21	714.711	2.426	714.711	1.51	0.09
8/28/96	3:42:21	734.711	2.356	734.711	1.44	0.08
8/28/96	4:02:21	754.711	2.292	754.711	1.37	0.08
8/28/96	4:22:21	774.711	2.234	774.711	1.31	0.08
8/28/96	4:42:21	794.711	2.181	794.711	1.26	0.07
8/28/96	5:02:21	814.711	2.133	814.711	1.21	0.07
8/28/96	5:22:21	834.711	2.089	834.711	1.17	0.07
8/28/96	5:42:21	854.711	2.050	854.711	1.13	0.07
8/28/96	6:02:21	874.711	2.013	874.711	1.09	0.06
8/28/96	6:22:21	894.711	1.978	894.711	1.06	0.06
8/28/96	6:42:21	914.711	1.941	914.711 934.711	1.02	0.06 0.06
8/28/96 8/28/96	7:02:21 7:22:21	934.711 954.711	1.911 1.881	934.711	0.99 0.96	0.06
8/28/96	7:42:21	974.711	1.856	974.711	0.96	0.05
8/28/96	8:02:21	994.711	1.828	994,711	0.94	0.05
8/28/96	8:22:21	1014.711	1.803	1014,711	0.88	0.05
8/28/96	8:42:21	1034.711	1.778	1034.711	0.86	0.05
8/28/96	9:02:21	1054.711	1.754	1054.711	0.83	0.05
8/28/96	9:22:21	1074.711	1.734	1074.711	0.81	0.05
8/28/96	9:42:21	1094.711	1.713	1094.711	0.79	0.05
8/28/96	10:02:21	1114.711	1.697	1114.711	0.78	0.05
8/28/96	10:22:21	1134.711	1.678	1134.711	0.76	0.04
8/28/96	10:42:21	1154.711	1.662	1154.711	0.74	0.04
8/28/96	11:02:21	1174.711	1.646	1174.711	0.73	0.04
8/28/96	11:22:21	1194.711	1.630	1194.711	0.71	0.04
8/28/96	11:42:21	1214.711	1.611	1214.711	0.69	0.04
8/28/96	12:02:21	1234.711	1.600	1234.711	0.68	0.04

### HVORSLEV SLUG TEST ANALYSIS RISING HEAD TEST MW-14R

$$K = \frac{r_e^2}{2L_e} ln \frac{L_e}{R_e} \left[ \frac{ln \left( \frac{h_1}{h_2} \right)}{(t2 - t1)} \right] 30.48$$

where:

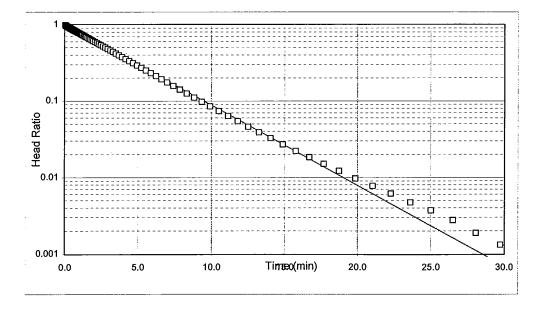
 $r_c$  = casing radius (feet)

 $R_e$  = equivalent radius (feet)

 $L_e$  = length of screened interval (feet)

t = time (minutes) $h_t = \text{head at time } t \text{ (feet)}$ 

INPUT PARAMETERS	RESULTS
$r_c = 0.15$	
$R_{\rm e} = 0.15$	
$L_{e} = 10$	K= 5.53E-04 cm/sec
$t_1 = 0$	K= 1.57E+00 ft/day
$t_2 = 30$	
$h_1/h_0 = 1.00$	
$h_2/h_0 = 0.00$	



Project Name: 216 Paterson Plank Road Site, New Jersey

Project No.: 943-6222

Test Date: 08/27/96

Analysis By:

SDM

Checked By: Analysis Date: FG 1/17/97

Page 1 of 4

#### RISING HEAD TEST MW-14R WELL NO. MW-14R

DATE 8/27/96 INITIAL DEPTH TO WATER FEET (btoc) 2.175 **INCHES** 3.5 CASING DIAMETER **INCHES** SAND DIAMETER 3.5 TOP OF OPEN INTERVAL 64 FEET (btoc) BOTTOM OF OPEN INTERVAL 74 FEET (btoc) SATURATED THICKNESS 10 FEET WATER TABLE TO BOTTOM OF SCREEN 71.825 FEET **EQUIVALENT DIAMETER** 3.50 INCHES OPEN INTERVAL LENGTH 10 FEET. STATIC IN SCREEN? Ν MAX. HEAD CHANGE 31.67 FEET MAX. HEAD IN SCREEN? Ν

Γ	DATE	TIME	EVENT	DEPTH TO	TEST	HEAD	HEAD
	j		ELAPSED	WATER	ELAPSED		RATIO
			TIME	1.	TIME		
		(HR:M:S)	(MIN)	(FEET)	(MIN)	(FEET)	
		,					
	8/27/96	13:59:35	0.000	33.848		31.67	
	8/27/96	13:59:35	0.005	33.862	l	31.69	
	8/27/96	13:59:35	0.010	33.929		31.75	
ı	8/27/96	13:59:35	0.015	33.844		31.67	
	8/27/96	13:59:36	0.020	33.922		31.75	
ţ	8/27/96	13:59:36	0.025	33.772		31.60	
-	8/27/96	13:59:36	0.030	33.791		31.62	
ı	8/27/96	13:59:37	0.035	33.885	0.000	31.71	1.000
	8/27/96	13:59:37	0.040	33.823	0.005	31.65	0.998
	8/27/96	13:59:37	0.045	33.823	0.010	31.65	0.998
	8/27/96	13:59:38	0.050	33.848	0.015	31.67	0.999
	8/27/96	13:59:38	0.055	33.710	0.020	31.54	0.994
	8/27/96	13:59:38	0.060	33.701	0.025	31.53	0.994
	8/27/96	13:59:38	0.065	33.654	0.030	31.48	0.993
	8/27/96	13:59:39	0.070	33.541	0.035	31.37	0.989
ı	8/27/96	13:59:39	0.075	33.403	0.040	31.23	0.985
	8/27/96	13:59:39	0.080	33.235	0.045	31.06	0.980
1	8/27/96	13:59:40	0.085	33.225	0.050	31.05	0.979
	8/27/96	13:59:40	0.090	33.135	0.055	30.96	0.976
	8/27/96	13:59:40	0.095	33.027	0.060	30.85	0.973
-	8/27/96	13:59:41	0.100	32.995	0.065	30.82	0.972
	8/27/96	13:59:41	0.106	32.937	0.071	30.76	0.970
-	8/27/96	13:59:41	0.112	32.870	0.077	30.70	0.968
- 1	8/27/96	13:59:42	0.119	32.815	0.084	30.64	0.966
	8/27/96	13:59:42	0.126	32.757	0.091	30.58	0.964
	8/27/96	13:59:42	0.133	32.683	0.098	30.51	0.962
	8/27/96	13:59:43	0.141	32.621	0.106	30.45	0.960
	8/27/96	13:59:43	0.149	32.508	0.114	30.33	0.957
1	8/27/96	13:59:44	0.158	32.448	0.123	30.27	0.955
	8/27/96	13:59:45	0.167	32.377	0.132	30.20	0.952
	8/27/96	13:59:45	0.177	32.300	0.142	30.13	0.950
	8/27/96	13:59:46	0.188	32.227	0.153	30.05	0.948
	8/27/96	13:59:46	0.199	32.151	0.164	29.98	0.945
-	8/27/96	13:59:47	0.210	32.061	0.175	29.89	0.942
	8/27/96	13:59:48	0.223	31.966	0.188	29.79	0.939
-	8/27/96	13:59:49	0.236	31.876	0.201	29.70	0.937
	8/27/96	13:59:49	0.250	31.777	0.215	29.60	0.934
	8/27/96	13:59:50	0.265	31.664	0.230	29.49	0.930
L	8/27/96	13:59:51	0.280	31.542	0.245	29.37	0.926

	DATE	TIME	EVENT	DEPTH TO	TEST	HEAD	HEAD
	D,		ELAPSED	WATER	ELAPSED	,	RATIO
			TIME	******	TIME	-	
		(HR:M:S)	(MIN)	(FEET)	(MIN)	(FEET)	
		<u> </u>		· · · · · · · · · · · · · · · · · · ·	(,7	( === /	
1	8/27/96	13:59:52	0.297	31.433	0.262	29.26	0.923
	8/27/96	13:59:53	0.315	31.302	0.280	29.13	0.919
	8/27/96	13:59:55	0.333	31,170	0.298	29.00	0.914
	8/27/96	13:59:56	0.353	31.030	0.318	28.86	0.910
	8/27/96	13:59:57	0.374	30.877	0.339	28.70	0.905
	8/27/96	13:59:58	0.396	30.718	0.361	28.54	0.900
	8/27/96	14:00:00	0.420	30.559	0.385	28.38	0.895
1	8/27/96	14:00:01	0.445	30.384	0.410	28.21	0.890
	8/27/96	14:00:03	0.470	30.208	0.435	28.03	0.884
	8/27/96	14:00:04	0.496	30.021	0.461	27.85	0.878
	8/27/96	14:00:06	0.525	29.828	0.490	27.65	0.872
1	8/27/96	14:00:08	0.555	29.639	0.520	27.46	0.866
	8/27/96	14:00:10	0.586	29.424	0.551	27.25	0.859
	8/27/96	14:00:12	0.621	29.186	0.586	27.01	0.852
	8/27/96	14:00:14	0.658	28.947	0.623	26.77	0.844
	8/27/96	14:00:16	0.696	28.697	0.661	26.52	0.836
	8/27/96	14:00:19	0.738	28.425	0.703	26.25	0.828
	8/27/96	14:00:21	0.781	28.146	0.746	25.97	0.819
	8/27/96	14:00:24	0.828	27.851	0.793	25.68	0.810
	8/27/96	14:00:27	0.876	27.549	0.841	25.37	0.800
	8/27/96	14:00:30	0.928	27.228	0.893	25.05	0.790
	8/27/96	14:00:33	0.983	26.896	0.948	24.72	0.780
1	8/27/96	14:00:37	1.041	26.548	1.006	24.37	0.769
	8/27/96	14:00:41	1.103	26.176	1.068	24.00	0.757
	8/27/96	14:00:45	1.168	25.798	1.133	23.62	0.745
Ì	8/27/96	14:00:49	1.238	25.394	1.203	23.22	0.732
	8/27/96	14:00:53	1.311	24.981	1.276	22.81	0.719
	8/27/96	14:00:58	1.390	24.548	1.355	22.37	0.706
	8/27/96	14:01:03	1.473	24.096	1.438	21.92	0.691
	8/27/96	14:01:08	1.561	23.630	1.526	21.46	0.677
	8/27/96	14:01:14	1.655	23.145	1.620	20.97	0.661
1	8/27/96	14:01:20	1.753	22.638	1.718	20.46	0.645
	8/27/96	14:01:26	1.858	22.121	1.823	19.95	0.629
	8/27/96	14:01:33	1.968	21.586	1.933	19.41	0.612
	8/27/96	14:01:40	2.085	21.042	2.050	18.87	0.595
	8/27/96	14:01:47	2.210	20.476	2.175	18.30	0.577
	8/27/96	14:01:55	2.341	19.886	2.306	17.71	0.559
	8/27/96	14:02:03	2.481	19.307	2.446	17.13	0.540
	8/27/96	14:02:12	2.630	18.700	2.595	16.53	0.521
	8/27/96	14:02:22	2.786	18.078	2.751	15.90	0.502
	8/27/96	14:02:32	2.953	17.443	2.918	15.27	0.481
	8/27/96	14:02:42	3.130	16.800	3.095	14.63	0.461
	8/27/96	14:02:53	3.316	16.142	3.281	13.97	0.440
	8/27/96	14:03:05	3.515	15.480	3.480	13.31	0.420
	8/27/96	14:03:18	3.725	14.811	3.690	12.64	0.398
]	8/27/96	14:03:31	3.946	14.140	3.911	11.97	0.377
	8/27/96	14:03:45	4.181	13.469	4.146	11.29	0.356
	8/27/96	14:04:00	4.430	12.793	4.395	10.62	0.335
	8/27/96	14:04:16	4.693	12.126	4.658	9.95	0.314
1	8/27/96	14:04:33	4.973	11.467	4.938	9.29	0.293
	8/27/96	14:04:51	5.270	10.809	5.235	8.63	0.272
	8/27/96	14:05:09	5.583	10.163	5.548	7.99	0.252
1	8/27/96	14:05:29	5.915	9.541	5.880	7.37	0.232
1	8/27/96	14:05:50	6.266	8.918	6.231	6.74	0.213
1	8/27/96	14:06:13	6.640	8.313	6.605	6.14	0.194
L	8/27/96	14:06:37	7.035	7.732	7.000	5.56	0.1 <u>75</u>

DATE	TIME	EVENT	DEPTH TO	TEST	HEAD	HEAD
		ELAPSED	WATER	ELAPSED		RATIO
		TIME	İ	TIME		
	(HR:M:S)	(MIN)	(FEET)	(MIN)	(FEET)	
					_	
8/27/96	14:07:02	7.453	7.179	7.418	5.00	0.158
8/27/96	14:07:28	7.896	6.660	7.861	4.49	0.141
8/27/96	14:07:56	8.366	6.164	8.331	3.99	0.126
8/27/96	14:08:26	8.865	5.705	8.830	3.53	0.111
8/27/96	14:08:58	9.391	5.278	9.356	3.10	0.098
8/27/96	14:09:31	9.950	4.883	9.915	2.71	0.085
8/27/96	14:10:07	10.541	4.524	10.506	2.35	0.074
8/27/96	14:10:45	11.168	4.196	11.133	2.02	0.064
8/27/96	14:11:24	11.831	3.905	11.796	1.73	0.055
8/27/96	14:12:07	12.535	3.645	12.500	1.47	0.046
8/27/96	14:12:51	13.280	3.414	13.245	1.24	0.039
8/27/96	14:13:39	14.070	3.213	14.035	1.04	0.033
8/27/96	14:14:29	14.906	3.036	14.871	0.86	0.027
8/27/96	14:15:22	15.791	2.881	15.756	0.71	0.022
8/27/96	14:16:18	16.730	2.759	16.695	0.58	0.018
8/27/96	14:17:18	17.723	2.653	17.688	0.48	0.015
8/27/96	14:18:21	18.776	2.563	18.741	0.39	0.012
8/27/96	14:19:28	19.891	2.484	19.856	0.31	0.010
8/27/96	14:20:39	21.073	2.422	21.038	0.25	0.008
8/27/96	14:21:54	22.325	2.371	22.290	0.20	0.006
8/27/96	14:23:13	23.650	2.325	23.615	0.15	0.005
8/27/96	14:24:38	25.055	2.293	25.020	0.12	0.004
8/27/96	14:26:07	26.543	2.263	26.508	0.09	0.003
8/27/96	14:27:42	28.118	2.235	28.083	0.06	0.002
8/27/96	14:29:22	29.786	2.217	29.751	0.04	0.001
8/27/96	14:31:08	31.555	2.198	31.520	0.02	0.001
8/27/96	14:33:00	33.428	2.185	33.393	0.01	0.000
8/27/96	14:34:59	35.411	2.175	35.376	0.00	0.000

#### **HVORSLEV SLUG TEST ANALYSIS RISING HEAD TEST MW-15D**

$$K = \frac{r_c^{1}}{2L_e} \ln \frac{L_e}{R_e} \left[ \frac{\ln \left( \frac{h_1}{h_2} \right)}{(t2 - t1)} \right] 30.48$$

where:

 $r_c$  = casing radius (feet)

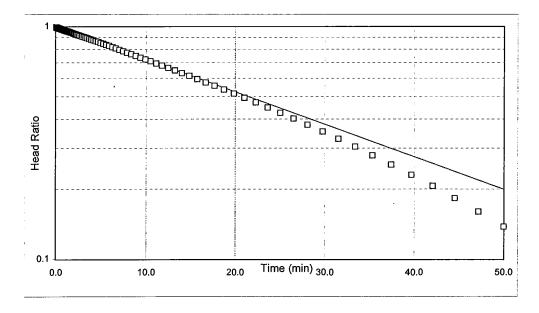
 $R_e$  = equivalent radius (feet)

L<sub>e</sub> = length of screened interval (feet)

t = time (minutes)

 $h_t$  = head at time t (feet)

INPUT PARAME	TERS		RESULTS
$r_c = 0$	.17		
$R_e = 0$	.33		
L <sub>e</sub> = 3	3.5	K=	1.53E-04 cm/sec
t <sub>1</sub> =	0	K=	4.33E-01 ft/day
$t_2 = 5$	50	•	_
$h_1/h_0 = 1.$	.00		
$h_2/h_0 = 0.$	.20		



Project Name: 216 Paterson Plank Road Site, New Jersey

Project No.: 943-6222

Test Date: 08/28/96

Analysis By:

Checked By:

Analysis Date:

SDM FG

### RISING HEAD TEST MW-15D MW-15D

DATE INITIAL DEPTH TO WATER CASING DIAMETER SAND DIAMETER SAND DIAMETER TOP OF OPEN INTERVAL BOTTOM OF OPEN INTERVAL SATURATED THICKNESS WATER TABLE TO BOTTOM OF SCREEN EQUIVALENT DIAMETER OPEN INTERVAL LENGTH	8/28/96 9.4 4 8 48.5 52 4 42.6 5.51 3.5	FEET (btoc) INCHES INCHES FEET (btoc) FEET (btoc) FEET FEET INCHES FEET
***************************************	5.51	INCHES
MAX. HEAD IN SCREEN?	N	

DATE	TIME	EVENT ELAPSED	DEPTH TO WATER	TEST ELAPSED	HEAD	HEAD RATIO
	(1)5 14 6	TIME	(CCCT)	TIME	(CCCT)	
	(HR:M:S)	(MIN)	(FEET)	(MIN)	(FEET)	
8/28/96	15:39:11	0.000	21.281		11.88	
8/28/96	15:39:11	0.005	21.657		12.26	
8/28/96	15:39:11	0.010	21.650		12.25	
8/28/96	15:39:11	0.015	21.871		12.47	
8/28/96	15:39:12	0.020	21.659		12.26	
8/28/96	15:39:12	0.025	21.694	Ì	12.29	
8/28/96	15:39:12	0.030	21.519		12.12	
8/28/96	15:39:13	0.035	21.881	0.000	12.48	1.00
8/28/96	15:39:13	0.040	21.848	0.005	12.45	1.00
8/28/96	15:39:13	0.045	21.848	0.010	12.45	1.00
8/28/96	15:39:14	0.050	21.844	0.015	12.44	1.00
8/28/96	15:39:14	0.055	21.825	0.020	12.43	1.00
8/28/96	15:39:14	0.060	21.848	0.025	12.45	1.00
8/28/96	15:39:14	0.065	21.858	0.030	12.46	1.00
8/28/96	15:39:15	0.070	21.871	0.035	12.47	1.00
8/28/96	15:39:15	0.075	21.807	0.040	12.41	0.99
8/28/96	15:39:15	0.080	21.807	0.045	12.41	0.99
8/28/96	15:39:16	0.085	21.844	0.050	12.44	1.00
8/28/96	15:39:16	0.090	21.825	0.055	12.43	1.00
8/28/96	15:39:16	0.095	21.825	0.060	12.43	1.00
8/28/96	15:39:17	0.100	21.830	0.065	12.43	1.00
8/28/96	15:39:17	0.106	21.809	0.071	12.41	0.99
8/28/96	15:39:17	0.112	21.821	0.077	12.42	1.00
8/28/96	15:39:18	0.119	21.805	0.Q84	12.41	0.99
8/28/96	15:39:18	0.126	21.816	0.091	12.42	0.99
8/28/96	15:39:18	0.133	21.800	0.098	12.40	0.99
8/28/96	15:39:19	0.141	21.800	0.106	12.40	0.99
8/28/96	15:39:19	0.149	21.781	0.114	12.38	0.99
8/28/96	15:39:20	0.158	21.781	0.123	12.38	0.99
8/28/96	15:39:21	0.167	21.795	0.132	12.40	0.99
8/28/96	15:39:21	0.177	21.781	0.142	12.38	0.99
8/28/96	15:39:22	0.188	21.791	0.153	12.39	0.99
8/28/96	15:39:22	0.199	21.777	0.164	12.38	0.99
8/28/96	15:39:23	0.210	21.781	0.175	12.38	0.99
8/28/96	15:39:24	0.223	21.763	0.188	12.36	0.99
8/28/96	15:39:25	0.236	21.758	0.201	12.36	0.99
8/28/96	15:39:25	0.250	21.754	0.215	12.35	0.99
8/28/96	15:39:26	0.265	21.745	0.230	12.35	0.99

DATE	TIME	EVENT	DEPTH TO	TEST	HEAD	HEAD
	}	ELAPSED	WATER	ELAPSED	,	RATIO
		TIME		TIME		ŀ
	(HR:M:S)	(MIN)	(FEET)	(MIN)	(FEET)	
1						
8/28/96	15:39:27	0.280	21.735	0.245	12.34	0.99
8/28/96	15:39:28	0.297	21.731	0.262	12.33	0.99
8/28/96	15:39:29	0.315	21.721	0.280	12.32	0.99
8/28/96	15:39:31	0.333	21.712	0.298	12.31	0.99
8/28/96	15:39:32	0.353	21.708	0.318	12.31	0.99
8/28/96	15:39:33	0.374	21.698	0.339	12.30	0.99
8/28/96	15:39:34	0.396	21.692	0.361	12.29	0.98
8/28/96	15:39:36	0.420	21.682	0.385	12.28	0.98
8/28/96	15:39:37	0.445	21.673	0.410	12.27	0.98
8/28/96	15:39:39	0.470	21.664	0.435	12.26	0.98
8/28/96	15:39:40	0.496	21.650	0.461	12.25	0.98
8/28/96	15:39:42	0.525	21.641	0.490	12.24	0.98
8/28/96	15:39:44	0.555	21.627	0.520	12.23	0.98
8/28/96	15:39:46	0.586	21.618	0.551	12.22	0.98
8/28/96	15:39:48	0.621	21.604	0.586	12.20	0.98
8/28/96	15:39:50	0.658	21.585	0.623	12.19	0.98
8/28/96	15:39:52	0.696	21.572	0.661	12.17	0.98
8/28/96	15:39:55	0.738	21.558	0.703	12.16	0.97
8/28/96	15:39:57	0.781	21.542	0.746	12.14	0.97
8/28/96	15:40:00	0.828	21.523	0.793	12.12	0.97
8/28/96	15:40:03	0.876	21.505	0.841	12.11	0.97
8/28/96	15:40:06	0.928	21.486	0.893	12.09	0.97
8/28/96	15:40:09	0.983	21.463	0.948	12.06	0.97
8/28/96	15:40:13	1.041	21.440	1.006	12.04	0.96
8/28/96	15:40:17	1.103	21.417	1.068	12.02	0.96
8/28/96	15:40:21	1.168	21.392	1.133	11.99	0.96
8/28/96	15:40:25	1.238	21.369	1.203	11.97	0.96 0.96
8/28/96	15:40:29	1.311	21.341	1.276	11.94	0.95
8/28/96	15:40:34	1.390	21.313	1.355	11.91	0.95
8/28/96	15:40:39	1.473	21.281	1.438 1.526	11.88 11.85	0.95
8/28/96	15:40:44	1.561	21.246 21.214	1.620	11.81	0.95
8/28/96 8/28/96	15:40:50 15:40:56	1.655 1.753	21.214	1.718	11.78	0.94
8/28/96	15:40:50	1.753	21.177	1.823	11.74	0.94
8/28/96	15:41:02	1.968	21.140	1.933	11.70	0.94
8/28/96	15:41:16	2.085	21.059	2.050	11.66	0.93
8/28/96	15:41:23	2.210	21.033	2.175	11.61	0.93
8/28/96	15:41:31	2.341	20.965	2.306	11.57	0.93
8/28/96	15:41:39	2.481	20.919	2.446	11.52	0.92
8/28/96	15:41:48	2.630	20.868	2.595	11.47	0.92
8/28/96	15:41:58	2.786	20.815	2.751	11.42	0.91
8/28/96	15:42:08	2.953	20.755	2.918	11.36	0.91
8/28/96	15:42:18	3.130	20.693	3.095	11.29	0.90
8/28/96	15:42:29	3.316	20.628	3.281	11.23	0.90
8/28/96	15:42:41	3.515	20.566	3.480	11.17	0.89
8/28/96	15:42:54	3.725	20.487	3.690	11.09	0.89
8/28/96	15:43:07	3.946	20.407	3.911	11.01	0.88
8/28/96	15:43:21	4.181	20.333	4.146	10.93	0.88
8/28/96	15:43:36	4.430	20.238	4.395	10.84	0.87
8/28/96	15:43:52	4.693	20.174	4.658	10.77	0.86
8/28/96	15:44:09	4.973	20.056	4.938	10.66	0.85
8/28/96	15:44:27	5.270	19.957	5.235	10.56	0.85
8/28/96	15:44:45	5.583	19.858	5.548	10.46	0.84
8/28/96	15:45:05	5.915	19.740	5.880	10.34	0.83
8/28/96	15:45:26	6.266	19.611	6.231	10.21	0.82
8/28/96	15:45:49	6.640	19.475	6.605	10.08	0.81

DATE	TIME	EVENT	DEPTH TO	TEST	HEAD	HEAD
		ELAPSED	WATER	ELAPSED		RATIO
		TIME	· · · · · ·	TIME		
	(HR:M:S)	(MIN)	(FEET)	(MIN)	(FEET)	
8/28/96	15:46:13	7.035	19.334	7.000	9.93	0.80
8/28/96	15:46:38	7.453	19.203	7.418	9.80	0.79
8/28/96	15:47:04	7.896	19.067	7.861	9.67	0.77
8/28/96	15:47:32	8.366	18.921	8.331	9.52	0.76
8/28/96	15:48:02	8.865	18.771	8.830	9.37	0.75
8/28/96	15:48:34	9.391	18.610	9.356	9.21	0.74
8/28/96	15:49:07	9.950	18,451	9.915	9.05	0.73
8/28/96	15:49:43	10.541	18.278	10.506	8.88	0.71
8/28/96	15:50:21	11.168	18.093	11.133	8.69	0.70
8/28/96	15:51:00	11.831	17.906	11.796	8.51	0.68
8/28/96	15:51:43	12.535	17.710	12.500	8.31	0.67
8/28/96	15:52:27	13.280	17.512	13.245	8.11	0.65
8/28/96	15:53:15	14.070	17.288	14.035	7.89	0.63
8/28/96	15:54:05	14.906	17.071	14.871	7.67	0.61
8/28/96	15:54:58	15.791	16.838	15.756	7.44	0.60
8/28/96	15:55:54	16.730	16,598	16.695	7.20	0.58
8/28/96	15:56:54	17.723	16.358	17.688	6.96	0.56
8/28/96	15:57:57	18.776	16.102	18.741	6.70	0.54
8/28/96	15:59:04	19.891	15.839	19.856	6.44	0.52
8/28/96	16:00:15	21.073	15.577	21.038	6.18	0.49
8/28/96	16:01:30	22.325	15.300	22.290	5.90	0.47
8/28/96	16:02:49	23.650	15.014	23.615	5.61	0.45
8/28/96	16:04:14	25.055	14.723	25.020	5.32	0.43
8/28/96	16:05:43	26.543	14.428	26.508	5.03	0.40
8/28/96	16:07:18	28.118	14.128	28.083	4.73	0.38
8/28/96	16:08:58	29.786	13.823	29.751	4.42	0.35
8/28/96	16:10:44	31.555	13.512	31.520	4.11	0.33
8/28/96	16:12:36	33.428	13.208	33.393	3.81	0.31
8/28/96	16:14:35	35.411	12.885	35.376	3.49	0.28
8/28/96	16:16:41	37.513	12.585	37.478	3.19	0.26
8/28/96	16:18:55	39.740	12.276	39.705	2.88	0.23
8/28/96	16:21:16	42.098	11.980	42.063	2.58	0.21
8/28/96	16:23:46	44.596	11.685	44.561	2.29	0.18
8/28/96	16:26:25	47.243	11.399	47.208	2.00	0.16
8/28/96	16:29:13	50.046	11.122	50.011	1.72	0.14
8/28/96	16:32:11	53.015	10.864	52.980	1.46	0.12
8/28/96	16:35:20	56.160	10.613	56.125	1.21	0.10
8/28/96	16:38:40	59.491	10.387	59.456	0.99	0.08
8/28/96	16:42:12	63.020	10.181	62.985	0.78	0.06
8/28/96	16:45:56	66.758	9.990	66.723	0.59	0.05
8/28/96	16:49:54	70.718	9.828	70.683	0.43	0.03
8/28/96	16:54:05	74.911	9.678	74.876	0.28	0.02
8/28/96	16:58:32	79.355	9.554	79.320	0.15	0.01

#### HVORSLEV SLUG TEST ANALYSIS RISING HEAD TEST MW-16D

$$K = \frac{r_c^{\ \prime}}{2L_e} ln \frac{L_e}{R_e} \left[ \frac{ln \left( \frac{h_t}{h_2} \right)}{(t2 - t1)} \right] 30.48$$

where:

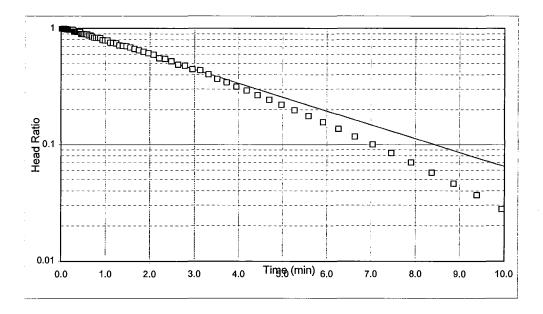
 $r_c$  = casing radius (feet)

 $R_e$  = equivalent radius (feet)

L<sub>e</sub> = length of screened interval (feet)

t = time (minutes) $h_t = \text{head at time } t \text{ (feet)}$ 

INPUT PARA	INPUT PARAMETERS		RESULTS
r <sub>c</sub> =	0.17		
$R_e =$	0.33		
$L_e = 1$	9	K=	7.09E-04 cm/sec
t <sub>1</sub> =	0	K=	2.01E+00 ft/day
$t_2 =$	10		
$h_1/h_0 =$	1.01		
$h_2/h_0 =$	0.07		



Project Name: 216 Paterson Plank Road Site, New Jersey

Analysis By:

SDM

Project No.: 943-6222

Checked By:

FG

Test Date: 08/28/96

Analysis Date:

#### **RISING HEAD TEST MW-16D**

WELL NO. MW-16D

Γ	DATE	TIME	EVENT	DEPTH TO	TEST	HEAD	HEAD
			ELAPSED	WATER	ELAPSED		RATIO
Ì	Ì		TIME		TIME		
		(HR:M:S)	(MIN)	(FEET)	(MIN)	(FEET)	
Ī							
- [	8/28/96	9:43:35	0.0000	17.5510	0.000	11.25	1.00
	8/28/96	9:43:35	0.0050	17.5510	0.005	11.25	1.00
	8/28/96	9:43:35	0.0100	17.5470	0.010	11.25	1.00
-	8/28/96	9:43:35	0.0150	17.5470	0.015	11.25	1.00
- 1	8/28/96	9:43:36	0.0200	17.5420	0.020	11.24	1.00
-	8/28/96	9:43:36	0.0250	17.5470	0.025	11.25	1.00
- 1	8/28/96	9:43:36	0.0300	17.5420	0.030	11.24	1.00
-	8/28/96	9:43:37	0.0350	17.5420	0.035	11.24	1.00
1	8/28/96	9:43:37	0.0400	17.5380	0.040	11.24	1.00
- 1	8/28/96	9:43:37	0.0450	17.5330	0.045	11.23	1.00
-1	8/28/96	9:43:38	0.0500	17.5240	0.050	11.22	1.00
ı	8/28/96	9:43:38	0.0550	17.5190	0.055	11.22	1.00
	8/28/96	9:43:38	0.0600	17.5100	0.060	11.21	1.00
	8/28/96	9:43:38	0.0650	17.5010	0.065	11.20	1.00
-	8/28/96	9:43:39	0.0700	17.4870	0.070	11.19	0.99
- {	8/28/96	9:43:39	0.0750	17.4780	0.075	11.18	0.99
	8/28/96	9:43:39	0.0800	17.4660	0.080	11.17	0.99
-	8/28/96	9:43:40	0.0850	17.4610	0.085	11.16	0.99
-	8/28/96	9:43:40	0.0900	17.4480	0.090	11.15	0.99
- 1	8/28/96	9:43:40	0.0950	17.4380	0.095	11.14	0.99
	8/28/96	9:43:41	0.1000	17.4290	0.100	11.13	0.99
	8/28/96	9:43:41	0.1058	17.4200	0.106	11.12	0.99
-	8/28/96	9:43:41	0.1120	17.4060	0.112	11.11	0.99
1	8/28/96	9:43:42	0.1185	17.3970	0.119	11.10	0.99
	8/28/96	9:43:42	0.1255	17.3880	0.126	11.09	0.99
	8/28/96	9:43:42	0.1328	17.3780	0.133	11.08	0.98
	8/28/96	9:43:43	0.1407	17.3650	0.141	11.07	0.98
	8/28/96	9:43:43	0.1490	17.3480	0.149	11.05	0.98
	8/28/96	9:43:44	0.1578	17.3390	0.158	11.04	0.98
	8/28/96	9:43:45	0.1672	17.3300	0.167	11.03	0.98
	8/28/96	9:43:45	0.1770	17.3250	0.177	11.03	0.98
	8/28/96	9:43:46	0.1875	17.3210	0.188	11.02	0.98
	8/28/96	9:43:46	0.1985	17.3120	0.199	11.01	0.98
	8/28/96	9:43:47	0.2102	17.3070	0.210	11.01	0.98
	8/28/96	9:43:48	0.2227	17.2880	0.223	10.99	0.98
	8/28/96	9:43:49	0.2358	17.2840	0.236	10.98	0.98
	8/28/96	9:43:49	0.2498	17.2790	0.250	10.98	0.98
L	8/28/96	9:43:50	0.2647	17.2750	0.265	10.98	0.98

DATE	TIME	EVENT	DEPTH TO	TEST	HEAD	HEAD
		ELAPSED	WATER	ELAPSED		RATIO
		TIME		TIME		
	(HR:M:S)	(MIN)	(FEET)	(MIN)	(FEET)	
						ļ
8/28/96	9:43:51	0.2803	16.9030	0.280	10.60	0.94
8/28/96	9:43:52	0.2970	16.8850	0.297	10.59	0.94
8/28/96	9:43:53	0.3147	16.8660	0.315	10.57	0.94
8/28/96	9:43:55	0.3333	16.8530	0.333	10.55	0.94
8/28/96	9:43:56	0.3532	16.8340	0.353	10.53	0.94
8/28/96	9:43:57	0.3742	16.8250	0.374	10.53	0.94
8/28/96	9:43:58	0.3963	16.8090	0.396	10.51	0.93
8/28/96	9:44:00	0.4198	16.7990	0.420	10.50	0.93
8/28/96	9:44:01	0.4447	16.4440	0.445	10.14	0.90
8/28/96	9:44:03	0.4697	16.4190	0.470	10.12	0.90
8/28/96	9:44:04	0.4963	16.3960	0.496	10.10	0.90
8/28/96	9:44:06	0.5247	16.3770	0.525	10.08	0.90
8/28/96	9:44:08	0.5547	16.3590	0.555	10.06	0.89
8/28/96	9:44:10	0.5863	16.3400	0.586	10.04	0.89
8/28/96	9:44:12	0.6213	16.1190	0.621	9.82	0.87
8/28/96	9:44:14	0.6580	16.1100	0.658	9.81	0.87
8/28/96	9:44:16	0.6963	15.9140	0.696	9.61	0.85
8/28/96	9:44:19	0.7380	15.7150	0.738	9.42	0.84
8/28/96	9:44:21	0.7813	15.6780	0.781	9.38	0.83
8/28/96	9:44:24	0.8280	15.6510	0.828	9.35	0.83
8/28/96	9:44:27	0.8763	15.6280	0.876	9.33	0.83
8/28/96	9:44:30	0.9280	15.2470	0.928	8.95	0.80
8/28/96	9:44:33	0.9830	15.2100	0.983	8.91	0.79
8/28/96	9:44:37	1.0413	15.1760	1.041	8.88	0.79
8/28/96	9:44:41	1.1030	14.8160	1.103	8.52	0.76
8/28/96	9:44:45	1.1680	14.7580	1.168	8.46	0.75
8/28/96	9:44:49	1.2380	14.7120	1.238	8.41	0.75
8/28/96	9:44:53	1.3113	14.3410	1.311	8.04	0.71
8/28/96	9:44:58	1.3897	14.2810	1.390	7.98	0.71
8/28/96	9:45:03	1.4730	14.2390	1.473	7.94	0.71
8/28/96	9:45:08	1.5613	14.0310	1.561	7.73	0.69
8/28/96	9:45:14	1.6547	13.8220	1.655	7.52	0.67
8/28/96	9:45:20	1.7530	13.6280	1.753	7.33	0.65
8/28/96	9:45:26	1.8580	13.4180	1.858	7.12	0.63
8/28/96	9:45:33	1.9680	13.2150	1.968	6.92	0.61
8/28/96	9:45:40	2.0847	13.0100	2.085	6.71	0.60
8/28/96	9:45:47	2.2097	12.5390	2.210	6.24	0.55
8/28/96	9:45:55	2.3413	12.4790	2.341	6.18	0.55
8/28/96	9:46:03	2.4813	12.2020	2.481	5.90	0.52
8/28/96	9:46:12	2.6297	11.8030	2.630	5.50	0.49
8/28/96	9:46:22	2.7863	11.7110	2.786	5.41	0.48
8/28/96	9:46:32	2.9530	11.3170	2.953	5.02	0.45
8/28/96	9:46:42	3.1297	11.2270	3.130	4.93	0.44
8/28/96	9:46:53	3.3163	10.8300	3.316	4.53	0.40
8/28/96	9:47:05	3.5147	10.4490	3.515	4.15	0.37
8/28/96	9:47:18	3.7247	10.1630	3.725	3.86	0.34
8/28/96	9:47:31	3.9463	9.8590	3.946	3.56	0.32
8/28/96	9:47:45	4.1813	9.5910	4.181	3.29	0.29
8/28/96	9:48:00	4.4297	9.3050	4.430	3.01	0.27
8/28/96	9:48:16	4.6930	9.0420	4.693	2.74	0.24
8/28/96	9:48:33	4.9730	8.7860	4.973	2.49	0.22
8/28/96	9:48:51	5.2697	8.5320	5.270	2.23	0.20
8/28/96	9:49:09	5.5830	8.2880	5.583	1.99	0.18
8/28/96	9:49:29	5.9147	8.0590	5.915	1.76	0.16
8/28/96	9:49:50	6.2663	7.8380	6.266	1.54	0.14
8/28/96	9:50:13	6.6397	7.6240	6.640	1.32	0.12

DATE	TIME	EVENT	DEPTH TO	TEST	HEAD	HEAD
		ELAPSED	WATER	ELAPSED		RATIO
		TIME		TIME		
	(HR:M:S)	(MIN)	(FEET)	(MIN)	(FEET)	100000000000000000000000000000000000000
-						
8/28/96	9:50:37	7.0347	7.4270	7.035	1.13	0.10
8/28/96	9:51:02	7.4530	7.2520	7.453	0.95	0.08
8/28/96	9:51:28	7.8963	7.0880	7.896	0.79	0.07
8/28/96	9:51:56	8.3663	6.9450	8.366	0.65	0.06
8/28/96	9:52:26	8.8647	6.8190	8.865	0.52	0.05
8/28/96	9:52:58	9.3913	6.7150	9.391	0.42	0.04
8/28/96	9:53:31	9.9497	6.6130	9.950	0.31	0.03
8/28/96	9:54:07	10.5413	6.5370	10.541	0.24	0.02
8/28/96	9:54:45	11.1680	6.4820	11.168	0.18	0.02
8/28/96	9:55:24	11.8313	6.4360	11.831	0.14	0.01
8/28/96	9:56:07	12.5347	6.4060	12.535	0.11	0.01
8/28/96	9:56:51	13.2797	6.3780	13.280	0.08	0.01
8/28/96	9:57:39	14.0697	6.3640	14.070	0.06	0.01

#### HVORSLEV SLUG TEST ANALYSIS RISING HEAD TEST MW-17D

$$K = \frac{r_c^2}{2L_e} ln \frac{L_e}{R_e} \left[ \frac{ln \left( \frac{h_1}{h_2} \right)}{(t2 - t1)} \right] 30.48$$

where:

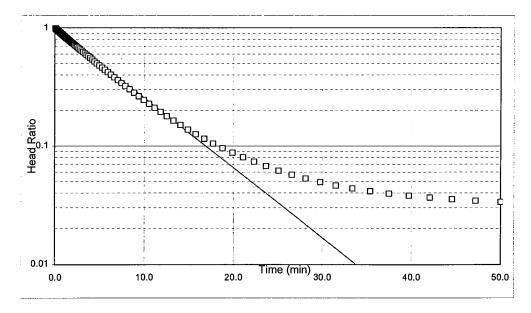
 $r_c$  = casing radius (feet)

R<sub>e</sub> = equivalent radius (feet)

 $L_e$  = length of screened interval (feet)

t = time (minutes) $h_t = \text{head at time } t \text{ (feet)}$ 

INPUT PARAMETERS	RESULTS		
$r_c = 0.17$			
$R_e = 0.33$			
$L_e = 13$	K= 2.71E-04 cm/sec		
$t_1 = 0$	K= 7.68E-01 ft/day		
$t_2 = 33.8$			
$h_1/h_0 = 1.00$			
$h_2/h_0 = 0.01$			



Project Name: 216 Paterson Plank Road Site, New Jersey

Analysis By:

SDM

Project No.: 943-6222

Checked By:

FG

Test Date: 08/28/96

Analysis Date:

# RISING HEAD TEST MW-17D

WELL NO. MW-17D

DATE INITIAL DEPTH TO WATER CASING DIAMETER SAND DIAMETER TOP OF OPEN INTERVAL BOTTOM OF OPEN INTERVAL SATURATED THICKNESS WATER TABLE TO BOTTOM OF SCREEN EQUIVALENT DIAMETER OPEN INTERVAL I FNGTH	8/28/96 4.23 4 8 42 55 16 50.77 5.51	FEET (btoc) INCHES INCHES FEET (btoc) FEET (btoc) FEET FEET INCHES FFET
MAX. HEAD IN SCREEN?	N	

	DATE	TIME	EVENT	DEPTH TO	TEST	HEAD	HEAD
			ELAPSED	WATER	ELAPSED		RATIO
			TIME		TIME		
-		(HR:M:S)	(MIN)	(FEET)	(MIN)	(FEET)	
	8/28/96	12:54:13	0.000	16.802	0.000	12.57	1.00
	8/28/96	12:54:13	0.005	16.796	0.005	12.57	1.00
	8/28/96	12:54:13	0.010	16.786	0.010	12.56	1.00
	8/28/96	12:54:13	0.015	16.775	0.015	12.55	1.00
	8/28/96	12:54:14	0.020	16.761	0.020	12.53	1.00
	8/28/96	12:54:14	0.025	16.752	0.025	12.52	1.00
	8/28/96	12:54:14	0.030	16.742	0.030	12.51	1.00
	8/28/96	12:54:15	0.035	16.731	0.035	12.50	0.99
	8/28/96	12:54:15	0.040	16.719	0.040	12.49	0.99
	8/28/96	12:54:15	0.045	16.712	0.045	12.48	0.99
	8/28/96	12:54:16	0.050	16.701	0.050	12.47	0.99
	8/28/96	12:54:16	0.055	16.689	0.055	12.46	0.99
1	8/28/96	12:54:16	0.060	16.680	0.060	12.45	0.99
	8/28/96	12:54:16	0.065	16.669	0.065	12.44	0.99
	8/28/96	12:54:17	0.070	16.659	0.070	12.43	0.99
	8/28/96	12:54:17	0.075	16.648	0.075	12.42	0.99
-	8/28/96	12:54:17	0.080	16.639	0.080	12.41	0.99
	8/28/96	12:54:18	0.085	16.629	0.085	12.40	0.99
1	8/28/96	12:54:18	0.090	16.620	0.090	12.39	0.99
İ	8/28/96	12:54:18	0.095	16.611	0.095	12.38	0.98
	8/28/96	12:54:19	0.100	16.602	0.100	12.37	0.98
	8/28/96	12:54:19	0.106	16.588	0.106	12.36	0.98
	8/28/96	12:54:19	0.112	16.576	0.112	12.35	0.98
	8/28/96	12:54:20	0.119	16.565	0.119	12.34	0.98
	8/28/96	12:54:20	0.126	16.551	0.126	12.32	0.98
	8/28/96	12:54:20	0.133	16.537	0.133	12.31	0.98
	8/28/96	12:54:21	0.141	16.521	0.141	12.29	0.98
-	8/28/96	12:54:21	0.149	16.493	0.149	12.26	0.98
	8/28/96	12:54:22	0.158	16.477	0.158	12.25	0.97
	8/28/96	12:54:23	0.167	16.459	0.167	12.23	0.97
	8/28/96	12:54:23	0.177	16.440	0.177	12.21	0.97
	8/28/96	12:54:24	0.188	16.420	0.188	12.19	0.97
	8/28/96	12:54:24	0.199	16.399	0.199	12.17	0.97
	8/28/96	12:54:25	0.210	16.378	0.210	12.15	0.97
	8/28/96	12:54:26	0.223	16.355	0.223	12.13	0.96
	8/28/96	12:54:27	0.236	16.330	0.236	12.10	0.96
	8/28/96	12:54:27	0.250	16.304	0.250	12.07	0.96
	8/28/96	12:54:28	0.265	16.277	0.265	12.05	0.96
<u> </u>	8/28/96	12:54:29	0.280	16.249	0.280	12.02	0.96

File:Mw17dslg.xls/DATA

DATE	TIME	EVENT	DEPTH TO	TEST	HEAD	HEAD
DATE	1 RVIC	ELAPSED	WATER	ELAPSED	HLAD	RATIO
		TIME	VVAILI	TIME		10,1110
	(HR:M:S)	(MIN)	(FEET)	(MIN)	(FEET)	
	(1111.141.0)	(14111.4)	(1 == 1)	(4)(1)	(1 == 17 -	
8/28/96	12:54:30	0.297	16.219	0.297	11.99	0.95
8/28/96	12:54:31	0.315	16.187	0.315	11.96	0.95
8/28/96	12:54:33	0.333	16.152	0.333	11.92	0.95
8/28/96	12:54:34	0.353	16.115	0.353	11.89	0.95
8/28/96	12:54:35	0.374	16.078	0.374	11.85	0.94
8/28/96	12:54:36	0.396	16.039	0.396	11.81	0.94
8/28/96	12:54:38	0.420	15.997	0.420	11.77	0.94
8/28/96	12:54:39	0.445	15.954	0.445	11.72	0.93
8/28/96	12:54:41	0.470	15.910	0.470	11.68	0.93
8/28/96	12:54:42	0.496	15.864	0.496	11.63	0.93
8/28/96	12:54:44	0.525	15.815	0.525	11.59	0.92
8/28/96	12:54:46	0.555	15.762	0.555	11.53	0.92
8/28/96	12:54:48	0.586	15.709	0.586	11.48	0.91
8/28/96	12:54:50	0.621	15.649	0.621	11.42	0.91
8/28/96	12:54:52	0.658	15.587	0.658	11.36	0.90
8/28/96	12:54:54	0.696	15.522	0.696	11.29	0.90
8/28/96	12:54:57	0.738	15.451	0.738	11.22	0.89
8/28/96	12:54:59	0.781	15.382	0.781	11,15	0.89
8/28/96	12:55:02	0.828	15.303	0.828	11.07	0.88
8/28/96	12:55:05	0.876	15.222	0.876	10.99	0.87
8/28/96	12:55:08	0.928	15.142	0.928	10.91	0.87
8/28/96	12:55:11	0.983	15.049	0.983	10.82	0.86
8/28/96	12:55:15	1.041	14.943	1.041	10.71	0.85
8/28/96	12:55:19	1.103	14.833	1.103	10.60	0.84
8/28/96	12:55:23	1.168	14.717	1.168	10.49	0.83
8/28/96	12:55:27	1.238	14.604	1.238	10.37	0.83
8/28/96	12:55:31	1.311	14.493	1.311	10.26	0.82
8/28/96	12:55:36	1.390	14.380	1.390	10.15	0.81
8/28/96	12:55:41	1.473	14.256	1.473	10.03	0.80
8/28/96	12:55:46	1.561	14.127	1.561	9.90	0.79
8/28/96	12:55:52	1.655	13.991	1.655	9.76	0.78
8/28/96	12:55:58	1.753	13.852	1.753	9.62	0.77
8/28/96	12:56:04	1.858	13.705	1.858	9.48	0.75
8/28/96	12:56:11	1.968	13.552	1.968	9.32	0.74
8/28/96	12:56:18	2.085	13.398	2.085	9.17	0.73
8/28/96	12:56:25	2.210	13.232	2.210	9.00	0.72
8/28/96	12:56:33	2.341	13.063	2.341	8.83	0.70
8/28/96	12:56:41	2.481	12.886	2.481	8.66	0.69
8/28/96	12:56:50	2.630	12.701	2.630	8.47	0.67
8/28/96	12:57:00	2.786	12.512	2.786	8.28	0.66
8/28/96	12:57:10	2.953	12.316	2.953	8.09	0.64
8/28/96	12:57:20	3.130	12.113	3.130	7.88	0.63
8/28/96	12:57:31	3.316	11.905		7.68	0.61
8/28/96	12:57:43	3.515	11.689	3.515	7.46	0.59
8/28/96	12:57:56	3.725	11.469	3.725	7.24	0.58
8/28/96	12:58:09	3.946	11.246	3.946	7.02	0.56
8/28/96	12:58:23	4.181	11.013	4.181	6.78	0.54
8/28/96	12:58:38	4.430	10.777	4.430	6.55	0.52
8/28/96	12:58:54	4.693	10.535	4.693	6.31	0.50
8/28/96	12:59:11	4.973	10.291	4.973	6.06	0.48
8/28/96	12:59:29	5.270	10.044	5.270	5.81	0.46
8/28/96	12:59:47	5.583	9.792	5.583	5.56	0.44
8/28/96	13:00:07	5.915	9.543	5.915	5.31	0.42
8/28/96	13:00:28	6.266	9.290	6.266	5.06	0.40
8/28/96	13:00:51	6.640	9.036	6.640	4.81	0.38
8/28/96	13:01:15	7.035	8.780	7.035	4.55	0.36

R2-0000488

DATE	TIME	EVENT	DEPTH TO	TEST	HEAD	HEAD
		ELAPSED	WATER	ELAPSED		RATIO
		TIME		TIME		
Ì	(HR:M:S)	(MIN)	(FEET)	(MIN)	(FEET)	
	, , , , , , , , , , , , , , , , , , , ,		( /			
8/28/96	13:01:40	7.453	8.528	7.453	4.30	0.34
8/28/96	13:02:06	7.896	8.279	7.896	4.05	0.32
8/28/96	13:02:34	8.366	8.032	8.366	3.80	0.30
8/28/96	13:03:04	8.865	7.788	8.865	3.56	0.28
8/28/96	13:03:36	9.391	7.553	9.391	3.32	0.26
8/28/96	13:04:09	9.950	7.322	9.950	3.09	0.25
8/28/96	13:04:45	10.541	7.098	10.541	2.87	0.23
8/28/96	13:05:23	11.168	6.886	11.168	2.66	0.21
8/28/96	13:06:02	11.831	6.678	11.831	2.45	0.19
8/28/96	13:06:45	12.535	6.482	12.535	2.25	0.18
8/28/96	13:07:29	13.280	6.298	13.280	2.07	0.16
8/28/96	13:08:17	14.070	6.125	14.070	1.90	0.15
8/28/96	13:09:07	14.906	5.963	14.906	1.73	0.14
8/28/96	13:10:00	15.791	5.813	15.791	1.58	0.13
8/28/96	13:10:56	16.730	5.677	16.730	1.45	0.12
8/28/96	13:11:56	17.723	5.551	17.723	1.32	0.11
8/28/96	13:12:59	18.776	5.435	18.776	1.21	0.10
8/28/96	13:14:06	19.891	5.334	19.891	1.10	0.09
8/28/96	13:15:17	21.073	5.239	21.073	1.01	0.08
8/28/96	13:16:32	22.325	5.156	22.325	0.93	0.07
8/28/96	13:17:51	23.650	5.080	23.650	0.85	0.07
8/28/96	13:19:16	25.055	5.008	25.055	0.78	0.06
8/28/96	13:20:45	26.543	4.948	26.543	0.72	0.06
8/28/96	13:22:20	28.118	4.898	28.118	0.67	0.05
8/28/96	13:24:00	29.786	4.852	29.786	0.62	0.05
8/28/96	13:25:46	31.555	4.810	31.555	0.58	0.05
8/28/96	13:27:38	33.428	4.780	33.428	0.55	0.04
8/28/96	13:29:37	35.411	4.752	35.411	0.52	0.04
8/28/96	13:31:43	37.513	4.727	37.513	0.50	0.04
8/28/96	13:33:57	39.740	4.709	39.740	0.48	0.04
8/28/96	13:36:18	42.098	4.690	42.098	0.46	0.04
8/28/96	13:38:48	44.596	4.676	44.596	0.45	0.04
8/28/96	13:41:27	47.243	4.662	47.243	0.43	0.03
8/28/96	13:44:15	50.046	4.653	50.046	0.42	0.03
8/28/96	13:47:13	53.015	4.642	53.015	0.41	0.03
8/28/96	13:50:22	56.160	4.632	56.160	0.40	0.03
8/28/96	13:53:42	59.491	4.623	59.491	0.39	0.03
8/28/96	13:57:14	63.020	4.619	63.020	0.39	0.03
8/28/96	14:00:58	66.758	4.609	66.758	0.38	0.03
8/28/96	14:04:56	70.718	4.605	70.718	0.38	0.03
8/28/96	14:09:07	74.911	4.600	74.911	0.37	0.03

#### HVORSLEV SLUG TEST ANALYSIS RISING HEAD TEST MW-18D

$$K = \frac{r_c^{1}}{2L_c} \ln \frac{L_c}{R_c} \left[ \frac{\ln \left( \frac{h_1}{h_2} \right)}{(t2 - t1)} \right] 30.48$$

where:

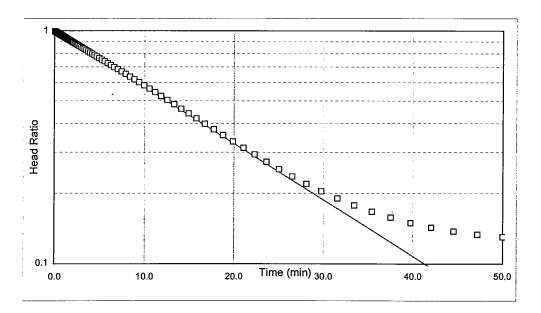
 $r_c$  = casing radius (feet)

 $R_e$  = equivalent radius (feet)

L<sub>e</sub> = length of screened interval (feet)

t = time (minutes) $h_t = \text{head at time } t \text{ (feet)}$ 

INPUT PARA	METERS	RESULTS
r <sub>c</sub> =	0.17	
R <sub>e</sub> =	0.33	
L <sub>e</sub> =	6	K= 1.90E-04 cm/sec
$t_1 =$	0	K= 5.37E-01 ft/day
$t_2 =$	85.9	
$h_1/h_0 =$	1.00	
$h_2/h_0 =$	0.01	



Project Name: 216 Paterson Plank Road Site, New Jersey

Project No.: 943-6222

Test Date: 08/28/96

Analysis By:

SDM

Checked By:

FG

Analysis Date:

1/17/97

# **RISING HEAD TEST MW-18D**

WELL NO. MW-18D

Ν

DATE 8/28/96 FEET (btoc) INITIAL DEPTH TO WATER 4.22 CASING DIAMETER 4 **INCHES** 8 **INCHES** SAND DIAMETER TOP OF OPEN INTERVAL 60 FEET (btoc) **BOTTOM OF OPEN INTERVAL** FEET (btoc) 66 SATURATED THICKNESS 7 FEET WATER TABLE TO BOTTOM OF SCREEN 61.78 **FEET EQUIVALENT DIAMETER** 5.51 **INCHES** OPEN INTERVAL LENGTH 6 **FEET** Ν STATIC IN SCREEN? MAX. HEAD CHANGE 37.06 FEET

MAX. HEAD IN SCREEN?

DEPTH TO TEST HEAD HEAD DATE TIME EVENT **ELAPSED RATIO ELAPSED** WATER TIME TIME (FEET) (HR:M:S) (MIN) (FEET) (MIN) 37.06 8/28/96 14:30:59 0.000 11.738 0.000 1.00 37.06 1.00 8/28/96 14:30:59 0.005 11.743 0.005 8/28/96 14:30:59 0.010 11.729 0.010 37.05 1.00 8/28/96 14:30:59 0.015 11.701 0.015 37.02 1.00 0.020 37.07 1.00 11.747 14:31:00 0.020 8/28/96 14:31:00 0.025 11.692 0.025 37.01 1.00 8/28/96 8/28/96 14:31:00 0.030 11.664 0.030 36.98 1.00 0.035 36.95 1.00 8/28/96 14:31:01 0.035 11.630 0.040 36.95 1.00 0.040 11.634 8/28/96 14:31:01 36.95 1.00 0.045 11.630 0.045 8/28/96 14:31:01 0.050 11.611 0.050 36.93 1.00 8/28/96 14:31:02 8/28/96 14:31:02 0.055 11.583 0.055 36.90 1.00 36.91 1.00 8/28/96 14:31:02 0.060 11.588 0.060 0.065 11.579 0.065 36.90 1.00 14:31:02 8/28/96 8/28/96 14:31:03 0.070 11.570 0.070 36.89 1.00 0.99 14:31:03 0.075 11.551 0.075 36.87 8/28/96 0.080 11.537 0.080 36.86 0.99 8/28/96 14:31:03 14:31:04 0.085 11.523 0.085 36.84 0.99 8/28/96 0.090 36.84 0.99 8/28/96 14:31:04 0.090 11.519 14:31:04 0.095 11.503 0.095 36.82 0.99 8/28/96 36.80 0.99 8/28/96 14:31:05 0.100 11.484 0.100 14:31:05 0.106 11.475 0.106 36.79 0.99 8/28/96 0.99 14:31:05 0.112 11.461 0.112 36.78 8/28/96 8/28/96 14:31:06 0.119 11.447 0.119 36.77 0.99 11.429 0.126 36.75 0.99 8/28/96 14:31:06 0.126 11.415 0.133 36.73 0.99 0.133 8/28/96 14:31:06 0.141 11.397 0.141 36.72 0.99 8/28/96 14:31:07 11.371 0.149 36.69 0.99 8/28/96 14:31:07 0.149 8/28/96 14:31:08 0.158 11.353 0.158 36.67 0.99 8/28/96 14:31:09 0.167 11.330 0.167 36.65 0.99 36.63 0.99 11.311 0.177 14:31:09 0.177 8/28/96 14:31:10 0.188 11.288 0.188 36.61 0.99 8/28/96 8/28/96 14:31:10 0.199 11.265 0.199 36.58 0.99 0.99 36.56 8/28/96 14:31:11 0.210 11.242 0.210 11.221 0.223 36.54 0.99 0.223 8/28/96 14:31:12 11.194 0.236 36.51 0.99 8/28/96 14:31:13 0.236 11.166 0.250 36.49 0.98 8/28/96 14:31:13 0.250 8/28/96 14:31:14 0.265 11.138 0.265 36.46 0.98 11.106 0.280 36.43 0.98 8/28/96 14:31:15 0.280

	DATE	TIME	EVENT	DEPTH TO	TEST	HEAD	HEAD
R/28/96	1		<b>ELAPSED</b>		ELAPSED		RATIO
8/28/96 14:31:16 0.297 11.076 0.297 36.40 0.98 8/28/96 14:31:17 0.315 11.044 0.315 36.36 0.98 8/28/96 14:31:20 0.353 10.965 0.353 36.28 0.98 8/28/96 14:31:21 0.374 10.931 0.374 36.25 0.98 8/28/96 14:31:22 0.396 10.889 0.396 36.21 0.98 8/28/96 14:31:24 0.420 10.843 0.420 36.16 0.98 8/28/96 14:31:25 0.445 10.794 0.445 36.11 0.97 8/28/96 14:31:25 0.445 10.794 0.445 36.11 0.97 8/28/96 14:31:28 0.496 10.693 0.496 36.07 0.97 8/28/96 14:31:28 0.496 10.693 0.496 36.07 0.97 8/28/96 14:31:30 0.525 10.645 0.525 35.96 0.97 8/28/96 14:31:30 0.525 10.585 0.555 35.90 0.97 8/28/96 14:31:34 0.586 10.522 0.586 35.84 0.97 8/28/96 14:31:34 0.586 10.522 0.586 35.84 0.97 8/28/96 14:31:36 0.621 10.458 0.621 35.78 0.97 8/28/96 14:31:34 0.686 10.326 0.683 35.71 0.98 8/28/96 14:31:34 0.696 10.312 0.696 35.63 0.99 8/28/96 14:31:40 0.696 10.312 0.696 35.63 0.99 8/28/96 14:31:45 0.781 10.153 0.781 35.47 0.98 8/28/96 14:31:45 0.781 10.153 0.781 35.47 0.98 8/28/96 14:31:45 0.781 10.153 0.781 35.47 0.98 8/28/96 14:31:45 0.781 10.153 0.781 35.47 0.98 8/28/96 14:31:45 0.781 10.153 0.781 35.47 0.98 8/28/96 14:31:45 0.781 10.153 0.781 35.47 0.98 8/28/96 14:31:45 0.781 10.153 0.781 35.47 0.98 8/28/96 14:31:45 0.781 10.153 0.781 35.47 0.98 8/28/96 14:31:45 0.781 10.153 0.781 35.47 0.98 8/28/96 14:31:45 0.781 10.153 0.781 35.47 0.98 8/28/96 14:31:51 0.876 9.978 0.876 0.928 35.20 0.95 8/28/96 14:32:51 1.03 9.551 1.103 9.551 1.103 34.87 0.99 8/28/96 14:32:51 1.041 9.684 1.041 34.98 0.94 8/28/96 14:32:57 1.103 9.551 1.103 34.87 0.99 8/28/96 14:32:50 1.168 9.477 1.168 34.75 0.99 8/28/96 14:32:50 1.168 9.477 1.168 34.75 0.99 8/28/96 14:32:57 1.968 7.987 1.968 33.31 0.99 8/28/96 14:32:57 1.968 7.987 1.968 33.31 0.99 8/28/96 14:32:57 1.968 7.987 1.968 33.31 0.99 8/28/96 14:32:57 1.968 7.987 1.968 33.31 0.99 8/28/96 14:32:57 1.968 7.987 1.968 33.31 0.99 8/28/96 14:32:57 1.968 7.987 1.968 33.31 0.99 8/28/96 14:32:57 1.968 7.987 1.968 33.31 0.99 8/28/96 14:32:57 1.968 7.987 1.968 33.31 0.99 8/28/96 14:33:57 1.968 7.987 1.968 33.30 0.99 8/28/96 14:33:57 1.968	1		TIME		TIME		
8/28/96 14:31:17 0.315 11.044 0.315 36.36 0.98 8/28/96 14:31:120 0.353 11.002 0.333 36.22 0.98 8/28/96 14:31:20 0.353 10.995 0.353 36.28 0.98 8/28/96 14:31:21 0.374 10.931 0.374 36.25 0.98 8/28/96 14:31:22 0.396 10.889 0.396 36.21 0.98 8/28/96 14:31:24 0.420 10.843 0.420 36.16 0.98 8/28/96 14:31:25 0.445 10.794 0.445 36.11 0.97 8/28/96 14:31:27 0.470 10.748 0.470 36.07 0.97 8/28/96 14:31:28 0.496 10.693 0.496 36.01 0.97 8/28/96 14:31:30 0.525 10.645 0.525 35.96 0.97 8/28/96 14:31:30 0.525 10.645 0.525 35.96 0.97 8/28/96 14:31:34 0.586 10.522 0.586 35.84 0.97 8/28/96 14:31:36 0.621 10.458 0.621 35.78 0.621 35.78 0.696 36.21 0.98 8/28/96 14:31:43 0.6821 10.458 0.621 35.78 0.96 8/28/96 14:31:43 0.6821 10.458 0.621 35.78 0.96 8/28/96 14:31:43 0.6826 10.386 0.585 35.50 0.96 8/28/96 14:31:43 0.6826 10.386 0.588 35.71 0.98 8/28/96 14:31:43 0.738 10.236 0.738 35.56 0.98 8/28/96 14:31:43 0.738 10.236 0.738 35.56 0.98 8/28/96 14:31:43 0.738 10.236 0.738 35.56 0.98 8/28/96 14:31:43 0.738 10.236 0.738 35.56 0.98 8/28/96 14:31:43 0.738 10.236 0.738 35.56 0.98 8/28/96 14:31:43 0.738 10.236 0.738 35.56 0.98 8/28/96 14:31:43 0.738 10.236 0.738 35.50 0.98 8/28/96 14:31:43 0.738 10.236 0.738 35.50 0.98 8/28/96 14:31:43 0.738 10.236 0.738 35.50 0.98 8/28/96 14:31:43 0.738 10.236 0.738 35.50 0.98 8/28/96 14:31:43 0.738 10.236 0.738 35.50 0.98 8/28/96 14:31:51 0.876 9.978 0.978		(HR:M:S)	(MIN)	(FEET)	(MIN)	(FEET)	
8/28/96 14:31:17 0.315 11.044 0.315 36.36 0.98 8/28/96 14:31:120 0.353 11.002 0.333 36.22 0.98 8/28/96 14:31:20 0.353 10.995 0.353 36.28 0.98 8/28/96 14:31:21 0.374 10.931 0.374 36.25 0.98 8/28/96 14:31:22 0.396 10.889 0.396 36.21 0.98 8/28/96 14:31:24 0.420 10.843 0.420 36.16 0.98 8/28/96 14:31:25 0.445 10.794 0.445 36.11 0.97 8/28/96 14:31:27 0.470 10.748 0.470 36.07 0.97 8/28/96 14:31:28 0.496 10.693 0.496 36.01 0.97 8/28/96 14:31:30 0.525 10.645 0.525 35.96 0.97 8/28/96 14:31:30 0.525 10.645 0.525 35.96 0.97 8/28/96 14:31:34 0.586 10.522 0.586 35.84 0.97 8/28/96 14:31:36 0.621 10.458 0.621 35.78 0.621 35.78 0.696 36.21 0.98 8/28/96 14:31:43 0.6821 10.458 0.621 35.78 0.96 8/28/96 14:31:43 0.6821 10.458 0.621 35.78 0.96 8/28/96 14:31:43 0.6826 10.386 0.585 35.50 0.96 8/28/96 14:31:43 0.6826 10.386 0.588 35.71 0.98 8/28/96 14:31:43 0.738 10.236 0.738 35.56 0.98 8/28/96 14:31:43 0.738 10.236 0.738 35.56 0.98 8/28/96 14:31:43 0.738 10.236 0.738 35.56 0.98 8/28/96 14:31:43 0.738 10.236 0.738 35.56 0.98 8/28/96 14:31:43 0.738 10.236 0.738 35.56 0.98 8/28/96 14:31:43 0.738 10.236 0.738 35.56 0.98 8/28/96 14:31:43 0.738 10.236 0.738 35.50 0.98 8/28/96 14:31:43 0.738 10.236 0.738 35.50 0.98 8/28/96 14:31:43 0.738 10.236 0.738 35.50 0.98 8/28/96 14:31:43 0.738 10.236 0.738 35.50 0.98 8/28/96 14:31:43 0.738 10.236 0.738 35.50 0.98 8/28/96 14:31:51 0.876 9.978 0.978							
8/28/96         14:31:17         0.315         11.044         0.315         36.36         0.98           8/28/96         14:31:20         0.333         11.002         0.333         36.32         0.98           8/28/96         14:31:21         0.374         10.991         0.374         36.25         0.98           8/28/96         14:31:24         0.420         10.843         0.420         36.16         0.98           8/28/96         14:31:25         0.445         10.794         0.445         36.11         0.97           8/28/96         14:31:27         0.470         10.748         0.470         36.07         0.97           8/28/96         14:31:32         0.496         10.693         0.496         36.01         0.97           8/28/96         14:31:33         0.555         10.585         0.555         35.96         0.97           8/28/96         14:31:34         0.586         10.522         0.586         35.84         0.97           8/28/96         14:31:33         0.658         10.522         0.586         35.71         0.96           8/28/96         14:31:43         0.621         10.458         0.621         35.76         0.97	8/28/96	14:31:16	0.297	11.076	0.297	36.40	0.98
8/28/96         14:31:20         0.353         10.965         0.353         36.28         0.98           8/28/96         14:31:21         0.374         10.981         0.396         36.21         0.98           8/28/96         14:31:24         0.420         10.843         0.420         36.16         0.98           8/28/96         14:31:25         0.445         10.794         0.445         36.11         0.97           8/28/96         14:31:27         0.470         10.748         0.470         36.07         0.97           8/28/96         14:31:30         0.525         10.645         0.525         35.96         0.97           8/28/96         14:31:30         0.525         10.645         0.525         35.96         0.97           8/28/96         14:31:34         0.566         10.522         0.586         35.84         0.97           8/28/96         14:31:34         0.566         10.522         0.586         35.51         0.97           8/28/96         14:31:34         0.768         10.522         0.586         35.51         0.98           8/28/96         14:31:43         0.738         10.236         0.738         35.59         0.97	8/28/96	14:31:17	0.315	11.044	0.315	36.36	0.98
8/28/96 14:31:21 0.374 10.931 0.374 36.25 0.98 8/28/96 14:31:22 0.396 10.889 0.396 36.21 0.98 8/28/96 14:31:25 0.445 10.794 0.445 36.11 0.97 8/28/96 14:31:25 0.445 10.794 0.445 36.11 0.97 8/28/96 14:31:27 0.470 10.748 0.470 36.07 0.97 8/28/96 14:31:28 0.496 10.693 0.496 36.01 0.97 8/28/96 14:31:30 0.525 10.645 0.525 35.96 0.97 8/28/96 14:31:30 0.525 10.645 0.525 35.96 0.97 8/28/96 14:31:34 0.566 10.522 0.586 35.84 0.97 8/28/96 14:31:36 0.621 10.458 0.621 35.78 0.97 8/28/96 14:31:36 0.621 10.458 0.621 35.78 0.97 8/28/96 14:31:34 0.566 10.522 0.586 35.84 0.97 8/28/96 14:31:34 0.566 10.322 0.586 35.84 0.97 8/28/96 14:31:34 0.566 10.322 0.586 35.84 0.97 8/28/96 14:31:34 0.586 10.322 0.586 35.84 0.97 8/28/96 14:31:34 0.689 10.342 0.696 35.63 0.98 8/28/96 14:31:43 0.738 10.236 0.738 35.56 0.98 8/28/96 14:31:44 0.696 10.312 0.696 35.63 0.98 8/28/96 14:31:45 0.781 10.153 0.781 35.47 0.96 8/28/96 14:31:45 0.781 10.153 0.781 35.47 0.96 8/28/96 14:31:45 0.828 10.088 0.828 35.39 0.95 8/28/96 14:31:45 0.928 9.876 0.928 35.20 0.95 8/28/96 14:31:57 0.983 9.773 0.983 35.09 0.95 8/28/96 14:32:01 1.041 9.664 1.041 34.98 0.94 8/28/96 14:32:01 1.041 9.664 1.041 34.98 0.94 8/28/96 14:32:01 1.041 9.664 1.041 34.98 0.94 8/28/96 14:32:01 1.041 9.664 1.041 34.98 0.94 8/28/96 14:32:01 1.041 9.684 1.041 34.98 0.94 8/28/96 14:32:02 1.390 9.023 1.390 34.44 0.93 8/28/96 14:32:02 1.390 9.023 1.390 34.94 0.93 8/28/96 14:32:02 1.390 9.023 1.390 34.94 0.93 8/28/96 14:32:03 1.655 8.548 1.655 33.67 0.91 8/28/96 14:32:07 1.656 8.784 1.655 33.67 0.99 8/28/96 14:32:07 1.565 8.548 1.655 33.67 0.99 8/28/96 14:32:07 1.565 8.548 1.655 33.67 0.99 8/28/96 14:32:07 1.565 8.548 1.655 33.67 0.99 8/28/96 14:32:07 1.565 8.548 1.655 33.67 0.99 8/28/96 14:32:07 1.565 8.548 1.655 33.67 0.99 8/28/96 14:33:04 2.056 7.784 2.055 33.10 0.99 8/28/96 14:33:04 2.056 7.784 2.055 33.90 0.95 8/28/96 14:33:04 2.056 7.784 2.055 33.10 0.99 8/28/96 14:33:04 2.056 7.784 2.055 33.10 0.99 8/28/96 14:33:04 2.056 7.784 2.055 33.10 0.99 8/28/96 14:33:04 2.056 7.784 2.055 33.10 0.99 8	8/28/96	14:31:19	0.333	11.002	0.333	36.32	0.98
8/28/96	1 1			10.965		36.28	0.98
8/28/96	8/28/96	14:31:21		10.931	0.374	36.25	0.98
8/28/96	1 1			10.889	0.396	36.21	0.98
8/28/96				10.843		36.16	0.98
8/28/96         14:31:27         0.470         10.748         0.470         36.07         0.97           8/28/96         14:31:30         0.496         10.683         0.496         36.01         0.97           8/28/96         14:31:30         0.525         10.685         0.555         35.96         0.97           8/28/96         14:31:34         0.586         10.585         0.555         35.90         0.97           8/28/96         14:31:36         0.621         10.458         0.621         55.78         0.97           8/28/96         14:31:40         0.686         10.386         0.658         35.71         0.96           8/28/96         14:31:43         0.738         10.236         0.738         35.63         0.96           8/28/96         14:31:45         0.781         10.153         0.781         35.47         0.96           8/28/96         14:31:45         0.781         10.153         0.781         35.47         0.96           8/28/96         14:31:44         0.928         9.876         0.928         35.30         0.95           8/28/96         14:31:51         0.876         9.978         0.876         0.530         0.95	8/28/96	14:31:25	0.445	10.794	0.445	36.11	0.97
8/28/96         14:31:28         0.496         10.693         0.496         36.01         0.97           8/28/96         14:31:32         0.555         10.685         0.555         35.96         0.97           8/28/96         14:31:34         0.586         10.522         0.586         35.84         0.97           8/28/96         14:31:38         0.681         10.486         0.621         35.78         0.97           8/28/96         14:31:38         0.688         10.386         0.658         35.71         0.96           8/28/96         14:31:40         0.696         10.312         0.696         35.63         0.96           8/28/96         14:31:43         0.738         10.236         0.738         35.56         0.96           8/28/96         14:31:48         0.828         10.068         0.828         35.39         0.95           8/28/96         14:31:51         0.826         9.976         0.828         35.30         0.95           8/28/96         14:32:51         0.983         9.773         0.983         35.09         0.95           8/28/96         14:32:01         1.041         9.664         1.041         34.98         0.94	8/28/96	14:31:27	0.470	10.748	0.470	36.07	0.97
8/28/96         14:31:32         0.555         10.585         0.555         35.90         0.97           8/28/96         14:31:34         0.586         10.522         0.586         35.84         0.97           8/28/96         14:31:36         0.621         10.458         0.621         35.78         0.97           8/28/96         14:31:40         0.696         10.312         0.696         35.63         0.96           8/28/96         14:31:45         0.781         10.236         0.738         35.56         0.96           8/28/96         14:31:45         0.781         10.153         0.781         35.47         0.98           8/28/96         14:31:54         0.828         10.088         0.828         35.39         0.95           8/28/96         14:31:54         0.928         9.876         0.928         35.20         0.95           8/28/96         14:32:05         1.03         9.551         1.103         34.87         0.94           8/28/96         14:32:01         1.041         9.664         1.041         34.99         0.95           8/28/96         14:32:13         1.238         9.300         1.238         34.62         0.93	8/28/96	14:31:28	0.496	10.693	0.496	36.01	0.97
8/28/96         14:31:32         0.555         10.585         0.556         35.90         0.97           8/28/96         14:31:34         0.586         10.522         0.586         35.84         0.97           8/28/96         14:31:36         0.621         10.458         0.621         35.78         0.97           8/28/96         14:31:40         0.696         10.312         0.696         35.63         0.96           8/28/96         14:31:45         0.781         10.153         0.781         35.47         0.96           8/28/96         14:31:45         0.781         10.153         0.781         35.47         0.96           8/28/96         14:31:45         0.781         10.153         0.781         35.47         0.96           8/28/96         14:31:54         0.928         9.876         0.928         35.39         0.95           8/28/96         14:31:57         0.983         9.773         0.983         35.20         0.95           8/28/96         14:32:01         1.041         9.664         1.041         34.98           8/28/96         14:32:01         1.013         9.551         1.103         34.87         0.94           8/28/96	8/28/96	14:31:30	0.525	10.645	0.525	35.96	0.97
8/28/96         14:31:34         0.586         10.522         0.586         35.84         0.97           8/28/96         14:31:36         0.621         10.458         0.621         35.78         0.97           8/28/96         14:31:40         0.696         10.312         0.696         35.63         0.96           8/28/96         14:31:43         0.738         10.236         0.738         35.56         0.96           8/28/96         14:31:45         0.781         10.153         0.781         35.47         0.96           8/28/96         14:31:45         0.781         10.153         0.781         35.30         0.95           8/28/96         14:31:54         0.828         10.068         0.828         35.30         0.95           8/28/96         14:31:54         0.928         9.876         0.928         35.20         0.95           8/28/96         14:31:54         0.928         9.876         0.928         35.20         0.95           8/28/96         14:31:54         0.928         9.876         0.928         35.20         0.95           8/28/96         14:32:20         1.041         9.664         1.041         34.98         0.94	i i		0.555	10.585	0.555	35.90	0.97
8/28/96         14:31:36         0.621         10.458         0.621         35.78         0.97           8/28/96         14:31:38         0.658         10.386         0.658         35.71         0.96           8/28/96         14:31:43         0.696         10.312         0.696         35.63         0.96           8/28/96         14:31:45         0.738         10.236         0.738         35.56         0.96           8/28/96         14:31:45         0.781         10.153         0.781         35.47         0.96           8/28/96         14:31:51         0.876         9.978         0.876         35.30         0.95           8/28/96         14:31:57         0.983         9.773         0.983         35.20         0.95           8/28/96         14:32:07         0.983         9.773         0.983         35.00         0.95           8/28/96         14:32:01         1.041         9.664         1.041         34.98         0.94           8/28/96         14:32:13         1.238         9.300         1.238         34.62         0.93           8/28/96         14:32:17         1.311         9.168         1.311         34.49         0.93	1					35.84	0.97
8/28/96         14:31:38         0.658         10.386         0.658         35.71         0.96           8/28/96         14:31:40         0.696         10.312         0.696         35.63         0.96           8/28/96         14:31:45         0.781         10.236         0.738         35.56         0.96           8/28/96         14:31:45         0.781         10.153         0.781         35.47         0.96           8/28/96         14:31:48         0.828         10.068         0.828         35.39         0.95           8/28/96         14:31:54         0.928         9.876         0.928         35.20         0.95           8/28/96         14:32:01         1.041         9.664         1.041         34.98         0.94           8/28/96         14:32:05         1.103         9.551         1.103         34.87         0.94           8/28/96         14:32:13         1.238         9.300         1.238         34.62         0.93           8/28/96         14:32:17         1.311         9.168         1.311         34.49         0.93           8/28/96         14:32:217         1.311         9.168         1.311         34.49         0.93	8/28/96			10,458	0.621	35.78	0.97
8/28/96         14:31:40         0.696         10.312         0.696         35.63         0.96           8/28/96         14:31:43         0.738         10.236         0.738         35.56         0.96           8/28/96         14:31:45         0.781         10.153         0.781         35.47         0.96           8/28/96         14:31:48         0.828         10.068         0.828         35.30         0.95           8/28/96         14:31:54         0.928         9.876         0.928         35.20         0.95           8/28/96         14:31:57         0.983         9.773         0.983         35.09         0.95           8/28/96         14:32:01         1.041         9.664         1.041         34.98         0.94           8/28/96         14:32:05         1.103         9.551         1.103         34.87         0.94           8/28/96         14:32:17         1.311         9.168         9.427         1.168         34.75         0.93           8/28/96         14:32:17         1.311         9.168         1.311         34.49         0.93           8/28/96         14:32:27         1.473         8.873         1.473         34.19         0.92	1				0.658	35.71	0.96
8/28/96         14:31:43         0.738         10.236         0.738         35.56         0.96           8/28/96         14:31:45         0.781         10.153         0.781         35.47         0.96           8/28/96         14:31:51         0.876         9.978         0.828         35.39         0.95           8/28/96         14:31:54         0.928         9.876         0.928         35.20         0.95           8/28/96         14:31:57         0.983         9.773         0.993         35.09         0.95           8/28/96         14:32:01         1.041         9.664         1.041         34.87         0.94           8/28/96         14:32:05         1.103         9.551         1.103         34.87         0.94           8/28/96         14:32:09         1.168         9.427         1.168         34.75         0.94           8/28/96         14:32:13         1.238         9.300         1.238         34.62         0.93           8/28/96         14:32:17         1.311         9.168         1.311         34.49         0.93           8/28/96         14:32:27         1.473         8.873         1.473         34.19         0.92           <					0.696	35.63	0.96
8/28/96         14:31:45         0.781         10.153         0.781         35.47         0.96           8/28/96         14:31:48         0.828         10.068         0.828         35.39         0.95           8/28/96         14:31:51         0.876         9.978         0.876         35.30         0.95           8/28/96         14:31:57         0.983         9.773         0.983         35.20         0.95           8/28/96         14:32:01         1.041         9.664         1.041         34.98         0.94           8/28/96         14:32:05         1.103         9.551         1.103         34.87         0.94           8/28/96         14:32:09         1.168         9.427         1.168         34.75         0.94           8/28/96         14:32:09         1.168         9.427         1.168         34.75         0.94           8/28/96         14:32:13         1.238         9.300         1.238         34.62         0.93           8/28/96         14:32:21         1.390         9.023         1.390         34.34         0.93           8/28/96         14:32:27         1.473         8.873         1.473         34.19         0.92           <	8/28/96			10,236	0.738	35.56	0.96
8/28/96         14:31:48         0.828         10.068         0.828         35:39         0.95           8/28/96         14:31:51         0.876         9.978         0.876         35:30         0.95           8/28/96         14:31:57         0.983         9.773         0.983         35:20         0.95           8/28/96         14:32:01         1.041         9.664         1.041         34.98         0.94           8/28/96         14:32:05         1.103         9.551         1.103         34.87         0.94           8/28/96         14:32:13         1.238         9.300         1.238         34.62         0.93           8/28/96         14:32:17         1.311         9.168         1.311         34.49         0.93           8/28/96         14:32:27         1.473         8.873         1.473         34.19         0.92           8/28/96         14:32:32         1.561         8.714         1.561         34.03         0.93           8/28/96         14:32:32         1.561         8.714         1.561         34.03         0.92           8/28/96         14:32:36         1.655         8.548         1.655         33.87         0.91 <t< td=""><td></td><td></td><td></td><td></td><td></td><td>35.47</td><td>0.96</td></t<>						35.47	0.96
8/28/96         14:31:51         0.876         9.978         0.876         35:30         0.95           8/28/96         14:31:54         0.928         9.876         0.928         35:20         0.95           8/28/96         14:31:57         0.983         9.773         0.983         35:09         0.95           8/28/96         14:32:01         1.041         9.644         1.041         34.98         0.94           8/28/96         14:32:03         1.103         9.551         1.103         34.87         0.94           8/28/96         14:32:13         1.238         9.300         1.238         34.62         0.93           8/28/96         14:32:22         1.390         9.023         1.390         34.34         0.93           8/28/96         14:32:22         1.390         9.023         1.390         34.34         0.93           8/28/96         14:32:32         1.561         8.714         1.561         34.03         0.92           8/28/96         14:32:38         1.655         8.548         1.655         33.87         0.91           8/28/96         14:32:44         1.753         8.370         1.753         33.69         0.91 <td< td=""><td></td><td></td><td></td><td>10.068</td><td>0.828</td><td>35.39</td><td>0.95</td></td<>				10.068	0.828	35.39	0.95
8/28/96         14:31:54         0.928         9.876         0.928         35.20         0.95           8/28/96         14:31:57         0.983         9.773         0.983         35.09         0.95           8/28/96         14:32:05         1.041         9.664         1.041         34.87         0.94           8/28/96         14:32:05         1.103         9.551         1.103         34.87         0.94           8/28/96         14:32:13         1.238         9.300         1.238         34.62         0.93           8/28/96         14:32:17         1.311         9.168         1.311         34.49         0.93           8/28/96         14:32:27         1.473         8.873         1.473         34.19         0.92           8/28/96         14:32:32         1.561         8.714         1.561         34.03         0.92           8/28/96         14:32:38         1.655         8.548         1.655         33.87         0.91           8/28/96         14:32:30         1.858         8.183         1.858         33.50         0.91           8/28/96         14:32:57         1.968         7.987         1.968         33.31         0.90 <td< td=""><td>1</td><td>14:31:51</td><td>0.876</td><td>9.978</td><td>0.876</td><td>35.30</td><td>0.95</td></td<>	1	14:31:51	0.876	9.978	0.876	35.30	0.95
8/28/96         14:31:57         0.983         9.773         0.983         35.09         0.95           8/28/96         14:32:01         1.041         9.664         1.041         34.98         0.94           8/28/96         14:32:05         1.103         9.551         1.103         34.87         0.94           8/28/96         14:32:09         1.168         9.427         1.168         34.75         0.94           8/28/96         14:32:17         1.311         9.168         1.311         34.49         0.93           8/28/96         14:32:22         1.390         9.023         1.390         34.34         0.93           8/28/96         14:32:32         1.561         8.714         1.561         34.03         0.92           8/28/96         14:32:32         1.561         8.714         1.561         34.03         0.92           8/28/96         14:32:32         1.561         8.714         1.561         34.03         0.92           8/28/96         14:32:34         1.753         8.370         1.753         33.69         0.91           8/28/96         14:33:04         2.085         7.871         1.968         33.31         0.90 <td< td=""><td></td><td></td><td></td><td>9.876</td><td>0.928</td><td>35.20</td><td>0.95</td></td<>				9.876	0.928	35.20	0.95
8/28/96         14:32:01         1.041         9.664         1.041         34.98         0.94           8/28/96         14:32:05         1.103         9.551         1.103         34.87         0.94           8/28/96         14:32:09         1.168         9.427         1.168         34.75         0.94           8/28/96         14:32:13         1.238         9.300         1.238         34.62         0.93           8/28/96         14:32:17         1.311         9.168         1.311         34.49         0.93           8/28/96         14:32:22         1.390         9.023         1.390         34.34         0.93           8/28/96         14:32:32         1.561         8.714         1.561         34.03         0.92           8/28/96         14:32:38         1.655         8.548         1.655         33.87         0.91           8/28/96         14:32:50         1.858         8.183         1.858         33.50         0.90           8/28/96         14:33:04         2.085         7.784         2.085         33.10         0.89           8/28/96         14:33:04         2.085         7.784         2.085         33.10         0.89 <td< td=""><td></td><td></td><td></td><td></td><td></td><td>35.09</td><td>0.95</td></td<>						35.09	0.95
8/28/96         14:32:05         1.103         9.551         1.103         34.87         0.94           8/28/96         14:32:09         1.168         9.427         1.168         34.75         0.94           8/28/96         14:32:13         1.238         9.300         1.238         34.62         0.93           8/28/96         14:32:22         1.391         9.168         1.311         34.49         0.93           8/28/96         14:32:22         1.390         9.023         1.390         34.34         0.93           8/28/96         14:32:32         1.561         8.714         1.561         34.03         0.92           8/28/96         14:32:38         1.655         8.548         1.655         33.87         0.91           8/28/96         14:32:37         1.858         8.183         1.858         33.50         0.92           8/28/96         14:32:57         1.968         7.987         1.968         33.31         0.90           8/28/96         14:33:04         2.085         7.784         2.085         33.10         0.80           8/28/96         14:33:11         2.210         7.565         2.210         32.88         0.89 <td< td=""><td></td><td>14:32:01</td><td></td><td>9.664</td><td>1.041</td><td>34.98</td><td>0.94</td></td<>		14:32:01		9.664	1.041	34.98	0.94
8/28/96         14:32:09         1.168         9.427         1.168         34.75         0.94           8/28/96         14:32:13         1.238         9.300         1.238         34.62         0.93           8/28/96         14:32:17         1.311         9.168         1.311         34.49         0.93           8/28/96         14:32:27         1.473         8.873         1.473         34.19         0.92           8/28/96         14:32:32         1.561         8.714         1.561         34.03         0.92           8/28/96         14:32:32         1.561         8.714         1.561         34.03         0.92           8/28/96         14:32:44         1.753         8.370         1.753         33.69         0.91           8/28/96         14:32:44         1.753         8.370         1.753         33.50         0.90           8/28/96         14:33:44         1.753         8.370         1.753         33.50         0.91           8/28/96         14:33:04         2.085         7.784         2.085         33.10         0.89           8/28/96         14:33:11         2.210         7.565         2.210         32.88         0.89 <td< td=""><td></td><td></td><td></td><td></td><td>1.103</td><td>34.87</td><td>0.94</td></td<>					1.103	34.87	0.94
8/28/96         14:32:13         1.238         9.300         1.238         34.62         0.93           8/28/96         14:32:17         1.311         9.168         1.311         34.49         0.93           8/28/96         14:32:27         1.373         8.873         1.473         34.19         0.93           8/28/96         14:32:32         1.561         8.714         1.561         34.03         0.92           8/28/96         14:32:38         1.655         8.548         1.655         33.87         0.91           8/28/96         14:32:44         1.753         8.370         1.753         33.69         0.91           8/28/96         14:32:50         1.858         8.183         1.858         33.50         0.90           8/28/96         14:33:04         2.085         7.784         2.085         33.10         0.90           8/28/96         14:33:04         2.085         7.784         2.085         33.10         0.89           8/28/96         14:33:11         2.210         7.565         2.210         32.88         0.89           8/28/96         14:33:36         2.630         6.848         2.630         32.17         0.87 <td< td=""><td></td><td></td><td></td><td>İ</td><td>1.168</td><td>34.75</td><td>0.94</td></td<>				İ	1.168	34.75	0.94
8/28/96         14:32:17         1.311         9.168         1.311         34.49         0.93           8/28/96         14:32:22         1.390         9.023         1.390         34.34         0.93           8/28/96         14:32:27         1.473         8.873         1.473         34.19         0.92           8/28/96         14:32:32         1.561         8.714         1.561         34.03         0.92           8/28/96         14:32:38         1.655         8.548         1.655         33.87         0.91           8/28/96         14:32:44         1.753         8.370         1.753         33.69         0.91           8/28/96         14:32:50         1.858         8.183         1.858         33.50         0.90           8/28/96         14:33:04         2.085         7.784         2.085         33.10         0.89           8/28/96         14:33:11         2.210         7.565         2.210         32.88         0.89           8/28/96         14:33:11         2.240         7.565         2.210         32.88         0.89           8/28/96         14:33:19         2.341         7.097         2.481         32.42         0.87 <td< td=""><td>1 - 1</td><td></td><td></td><td>9.300</td><td>1.238</td><td>34.62</td><td>0.93</td></td<>	1 - 1			9.300	1.238	34.62	0.93
8/28/96         14:32:22         1.390         9.023         1.390         34.34         0.93           8/28/96         14:32:27         1.473         8.873         1.473         34.19         0.92           8/28/96         14:32:32         1.561         8.714         1.561         34.03         0.92           8/28/96         14:32:38         1.655         8.548         1.655         33.87         0.91           8/28/96         14:32:44         1.753         8.370         1.753         33.69         0.91           8/28/96         14:32:50         1.858         8.183         1.858         33.50         0.90           8/28/96         14:32:57         1.968         7.987         1.968         33.31         0.90           8/28/96         14:33:04         2.085         7.784         2.085         33.10         0.89           8/28/96         14:33:11         2.210         7.565         2.210         32.88         0.89           8/28/96         14:33:42         2.87         7.987         2.481         32.42         0.87           8/28/96         14:33:46         2.630         6.848         2.630         32.17         0.87					1.311	34.49	0.93
8/28/96         14:32:27         1.473         8.873         1.473         34.19         0.92           8/28/96         14:32:32         1.561         8.714         1.561         34.03         0.92           8/28/96         14:32:38         1.655         8.548         1.655         33.87         0.91           8/28/96         14:32:44         1.753         8.370         1.753         33.69         0.91           8/28/96         14:32:50         1.858         8.183         1.858         33.50         0.90           8/28/96         14:32:57         1.968         7.987         1.968         33.31         0.90           8/28/96         14:33:04         2.085         7.784         2.085         33.10         0.89           8/28/96         14:33:11         2.210         7.565         2.210         32.88         0.89           8/28/96         14:33:19         2.341         7.339         2.341         32.66         0.88           8/28/96         14:33:36         2.630         6.848         2.630         32.17         0.87           8/28/96         14:33:46         2.786         6.580         2.786         31.90         0.86 <td< td=""><td></td><td></td><td></td><td>9.023</td><td></td><td>34.34</td><td>0.93</td></td<>				9.023		34.34	0.93
8/28/96         14:32:32         1.561         8.714         1.561         34.03         0.92           8/28/96         14:32:38         1.655         8.548         1.655         33.87         0.91           8/28/96         14:32:44         1.753         8.370         1.753         33.69         0.91           8/28/96         14:32:50         1.858         8.183         1.858         33.50         0.90           8/28/96         14:32:57         1.968         7.987         1.968         33.31         0.90           8/28/96         14:33:04         2.085         7.784         2.085         33.10         0.89           8/28/96         14:33:11         2.210         7.565         2.210         32.88         0.89           8/28/96         14:33:19         2.341         7.339         2.341         32.42         0.87           8/28/96         14:33:36         2.630         6.848         2.630         32.17         0.87           8/28/96         14:33:46         2.786         6.580         2.786         31.90         0.86           8/28/96         14:34:40         3.130         5.999         3.130         31.32         0.85 <td< td=""><td></td><td></td><td></td><td>1</td><td>1.473</td><td>34.19</td><td>0.92</td></td<>				1	1.473	34.19	0.92
8/28/96         14:32:38         1.655         8.548         1.655         33.87         0.91           8/28/96         14:32:44         1.753         8.370         1.753         33.69         0.91           8/28/96         14:32:50         1.858         8.183         1.858         33.50         0.90           8/28/96         14:32:57         1.968         7.987         1.968         33.31         0.90           8/28/96         14:33:04         2.085         7.784         2.085         33.10         0.89           8/28/96         14:33:11         2.210         7.565         2.210         32.88         0.89           8/28/96         14:33:19         2.341         7.339         2.341         32.66         0.88           8/28/96         14:33:36         2.630         6.848         2.630         32.17         0.87           8/28/96         14:33:46         2.786         6.580         2.786         31.90         0.86           8/28/96         14:33:40         3.130         5.999         3.130         31.32         0.85           8/28/96         14:34:17         3.316         5.694         3.316         31.01         0.84 <td< td=""><td></td><td></td><td></td><td></td><td>1.561</td><td>34.03</td><td>0.92</td></td<>					1.561	34.03	0.92
8/28/96         14:32:44         1.753         8.370         1.753         33.69         0.91           8/28/96         14:32:50         1.858         8.183         1.858         33.50         0.90           8/28/96         14:32:57         1.968         7.987         1.968         33.31         0.90           8/28/96         14:33:04         2.085         7.784         2.085         33.10         0.89           8/28/96         14:33:11         2.210         7.565         2.210         32.88         0.89           8/28/96         14:33:19         2.341         7.339         2.341         32.66         0.88           8/28/96         14:33:27         2.481         7.097         2.481         32.42         0.87           8/28/96         14:33:36         2.630         6.848         2.630         32.17         0.87           8/28/96         14:33:46         2.786         6.580         2.786         31.90         0.86           8/28/96         14:34:40         3.130         5.999         3.130         31.32         0.85           8/28/96         14:34:42         3.725         5.021         3.725         30.34         0.82 <td< td=""><td></td><td>14:32:38</td><td>1,655</td><td>1</td><td>1.655</td><td>33.87</td><td>0.91</td></td<>		14:32:38	1,655	1	1.655	33.87	0.91
8/28/96         14:32:50         1.858         8.183         1.858         33.50         0.90           8/28/96         14:32:57         1.968         7.987         1.968         33.31         0.90           8/28/96         14:33:04         2.085         7.784         2.085         33.10         0.89           8/28/96         14:33:11         2.210         7.565         2.210         32.88         0.89           8/28/96         14:33:19         2.341         7.339         2.341         32.66         0.88           8/28/96         14:33:27         2.481         7.097         2.481         32.42         0.87           8/28/96         14:33:36         2.630         6.848         2.630         32.17         0.87           8/28/96         14:33:46         2.786         6.580         2.786         31.90         0.86           8/28/96         14:33:56         2.953         6.299         2.953         31.62         0.85           8/28/96         14:34:17         3.316         5.694         3.316         31.01         0.84           8/28/96         14:34:42         3.725         5.021         3.725         30.34         0.82 <td< td=""><td></td><td></td><td></td><td>8.370</td><td>1.753</td><td>33.69</td><td>0.91</td></td<>				8.370	1.753	33.69	0.91
8/28/96         14:33:04         2.085         7.784         2.085         33.10         0.89           8/28/96         14:33:11         2.210         7.565         2.210         32.88         0.89           8/28/96         14:33:19         2.341         7.339         2.341         32.66         0.88           8/28/96         14:33:27         2.481         7.097         2.481         32.42         0.87           8/28/96         14:33:36         2.630         6.848         2.630         32.17         0.87           8/28/96         14:33:46         2.786         6.580         2.786         31.90         0.86           8/28/96         14:33:56         2.953         6.299         2.953         31.90         0.86           8/28/96         14:34:06         3.130         5.999         3.130         31.32         0.85           8/28/96         14:34:29         3.515         5.367         3.515         30.69         0.83           8/28/96         14:34:42         3.725         5.021         3.725         30.34         0.82           8/28/96         14:35:50         4.181         4.253         4.181         29.57         0.80 <td< td=""><td></td><td>14:32:50</td><td></td><td>8.183</td><td>1.858</td><td>33.50</td><td>0.90</td></td<>		14:32:50		8.183	1.858	33.50	0.90
8/28/96         14:33:11         2.210         7.565         2.210         32.88         0.89           8/28/96         14:33:19         2.341         7.339         2.341         32.66         0.88           8/28/96         14:33:27         2.481         7.097         2.481         32.42         0.87           8/28/96         14:33:36         2.630         6.848         2.630         32.17         0.87           8/28/96         14:33:46         2.786         6.580         2.786         31.90         0.86           8/28/96         14:33:56         2.953         6.299         2.953         31.90         0.86           8/28/96         14:34:06         3.130         5.999         3.130         31.32         0.85           8/28/96         14:34:29         3.515         5.367         3.515         30.69         0.83           8/28/96         14:34:42         3.725         5.021         3.725         30.34         0.82           8/28/96         14:34:42         3.725         5.021         3.725         30.34         0.82           8/28/96         14:35:50         4.181         4.253         4.181         29.57         0.80 <td< td=""><td>8/28/96</td><td>14:32:57</td><td>1.968</td><td>7.987</td><td>1.968</td><td>33.31</td><td>0.90</td></td<>	8/28/96	14:32:57	1.968	7.987	1.968	33.31	0.90
8/28/96         14:33:11         2.210         7.565         2.210         32.88         0.89           8/28/96         14:33:19         2.341         7.339         2.341         32.66         0.88           8/28/96         14:33:27         2.481         7.097         2.481         32.42         0.87           8/28/96         14:33:36         2.630         6.848         2.630         32.17         0.87           8/28/96         14:33:46         2.786         6.580         2.786         31.90         0.86           8/28/96         14:34:06         3.130         5.999         2.953         31.62         0.85           8/28/96         14:34:06         3.130         5.999         3.130         31.32         0.85           8/28/96         14:34:29         3.515         5.367         3.515         30.69         0.83           8/28/96         14:34:42         3.725         5.021         3.725         30.34         0.82           8/28/96         14:34:42         3.725         5.021         3.725         30.34         0.82           8/28/96         14:35:50         4.181         4.253         4.181         29.57         0.80 <td< td=""><td>8/28/96</td><td>14:33:04</td><td>2.085</td><td>7.784</td><td>2.085</td><td>33.10</td><td>0.89</td></td<>	8/28/96	14:33:04	2.085	7.784	2.085	33.10	0.89
8/28/96         14:33:27         2.481         7.097         2.481         32.42         0.87           8/28/96         14:33:36         2.630         6.848         2.630         32.17         0.87           8/28/96         14:33:46         2.786         6.580         2.786         31.90         0.86           8/28/96         14:33:56         2.953         6.299         2.953         31.62         0.85           8/28/96         14:34:06         3.130         5.999         3.130         31.32         0.85           8/28/96         14:34:17         3.316         5.694         3.316         31.01         0.84           8/28/96         14:34:29         3.515         5.367         3.515         30.69         0.83           8/28/96         14:34:42         3.725         5.021         3.725         30.34         0.82           8/28/96         14:34:42         3.725         5.021         3.725         30.34         0.82           8/28/96         14:35:50         4.181         4.253         4.181         29.57         0.80           8/28/96         14:35:40         4.693         3.452         4.693         28.77         0.78 <td< td=""><td>8/28/96</td><td>14:33:11</td><td></td><td>7.565</td><td>2.210</td><td>32.88</td><td>0.89</td></td<>	8/28/96	14:33:11		7.565	2.210	32.88	0.89
8/28/96         14:33:36         2.630         6.848         2.630         32.17         0.87           8/28/96         14:33:46         2.786         6.580         2.786         31.90         0.86           8/28/96         14:33:56         2.953         6.299         2.953         31.62         0.85           8/28/96         14:34:06         3.130         5.999         3.130         31.32         0.85           8/28/96         14:34:17         3.316         5.694         3.316         31.01         0.84           8/28/96         14:34:29         3.515         5.367         3.515         30.69         0.83           8/28/96         14:34:42         3.725         5.021         3.725         30.34         0.82           8/28/96         14:34:55         3.946         4.626         3.946         29.95         0.81           8/28/96         14:35:09         4.181         4.253         4.181         29.57         0.80           8/28/96         14:35:24         4.430         3.863         4.430         29.18         0.79           8/28/96         14:35:40         4.693         3.452         4.693         28.77         0.78 <td< td=""><td>8/28/96</td><td>14:33:19</td><td>2.341</td><td>7.339</td><td>2.341</td><td>32.66</td><td>0.88</td></td<>	8/28/96	14:33:19	2.341	7.339	2.341	32.66	0.88
8/28/96         14:33:36         2.630         6.848         2.630         32.17         0.87           8/28/96         14:33:46         2.786         6.580         2.786         31.90         0.86           8/28/96         14:33:56         2.953         6.299         2.953         31.62         0.85           8/28/96         14:34:06         3.130         5.999         3.130         31.32         0.85           8/28/96         14:34:17         3.316         5.694         3.316         31.01         0.84           8/28/96         14:34:29         3.515         5.367         3.515         30.69         0.83           8/28/96         14:34:42         3.725         5.021         3.725         30.34         0.82           8/28/96         14:34:55         3.946         4.626         3.946         29.95         0.81           8/28/96         14:35:09         4.181         4.253         4.181         29.57         0.80           8/28/96         14:35:24         4.430         3.863         4.430         29.18         0.79           8/28/96         14:35:40         4.693         3.452         4.693         28.77         0.78 <td< td=""><td></td><td></td><td>2.481</td><td>7.097</td><td>2.481</td><td>32.42</td><td>0.87</td></td<>			2.481	7.097	2.481	32.42	0.87
8/28/96         14:33:46         2.786         6.580         2.786         31.90         0.86           8/28/96         14:33:56         2.953         6.299         2.953         31.62         0.85           8/28/96         14:34:06         3.130         5.999         3.130         31.32         0.85           8/28/96         14:34:17         3.316         5.694         3.316         31.01         0.84           8/28/96         14:34:29         3.515         5.367         3.515         30.69         0.83           8/28/96         14:34:42         3.725         5.021         3.725         30.34         0.82           8/28/96         14:34:55         3.946         4.626         3.946         29.95         0.81           8/28/96         14:35:09         4.181         4.253         4.181         29.57         0.80           8/28/96         14:35:24         4.430         3.863         4.430         29.18         0.79           8/28/96         14:35:40         4.693         3.452         4.693         28.77         0.78           8/28/96         14:36:15         5.270         2.580         5.270         27.90         0.75 <td< td=""><td></td><td></td><td>2.630</td><td>6.848</td><td>2.630</td><td>32.17</td><td>0.87</td></td<>			2.630	6.848	2.630	32.17	0.87
8/28/96         14:33:56         2.953         6.299         2.953         31.62         0.85           8/28/96         14:34:06         3.130         5.999         3.130         31.32         0.85           8/28/96         14:34:17         3.316         5.694         3.316         31.01         0.84           8/28/96         14:34:29         3.515         5.367         3.515         30.69         0.83           8/28/96         14:34:42         3.725         5.021         3.725         30.34         0.82           8/28/96         14:34:55         3.946         4.626         3.946         29.95         0.81           8/28/96         14:35:09         4.181         4.253         4.181         29.57         0.80           8/28/96         14:35:24         4.430         3.863         4.430         29.18         0.79           8/28/96         14:35:40         4.693         3.452         4.693         28.77         0.78           8/28/96         14:35:57         4.973         3.030         4.973         28.35         0.77           8/28/96         14:36:15         5.270         2.580         5.270         27.90         0.75 <td< td=""><td></td><td>14:33:46</td><td></td><td>6.580</td><td>2.786</td><td>31.90</td><td>0.86</td></td<>		14:33:46		6.580	2.786	31.90	0.86
8/28/96         14:34:06         3.130         5.999         3.130         31.32         0.85           8/28/96         14:34:17         3.316         5.694         3.316         31.01         0.84           8/28/96         14:34:29         3.515         5.367         3.515         30.69         0.83           8/28/96         14:34:42         3.725         5.021         3.725         30.34         0.82           8/28/96         14:34:55         3.946         4.626         3.946         29.95         0.81           8/28/96         14:35:09         4.181         4.253         4.181         29.57         0.80           8/28/96         14:35:24         4.430         3.863         4.430         29.18         0.79           8/28/96         14:35:40         4.693         3.452         4.693         28.77         0.78           8/28/96         14:35:57         4.973         3.030         4.973         28.35         0.77           8/28/96         14:36:15         5.270         2.580         5.270         27.90         0.75           8/28/96         14:36:33         5.583         2.114         5.583         27.43         0.74 <td< td=""><td></td><td></td><td></td><td></td><td>2.953</td><td>31.62</td><td>0.85</td></td<>					2.953	31.62	0.85
8/28/96         14:34:17         3.316         5.694         3.316         31.01         0.84           8/28/96         14:34:29         3.515         5.367         3.515         30.69         0.83           8/28/96         14:34:42         3.725         5.021         3.725         30.34         0.82           8/28/96         14:34:55         3.946         4.626         3.946         29.95         0.81           8/28/96         14:35:09         4.181         4.253         4.181         29.57         0.80           8/28/96         14:35:24         4.430         3.863         4.430         29.18         0.79           8/28/96         14:35:40         4.693         3.452         4.693         28.77         0.78           8/28/96         14:35:57         4.973         3.030         4.973         28.35         0.77           8/28/96         14:36:15         5.270         2.580         5.270         27.90         0.75           8/28/96         14:36:33         5.583         2.114         5.583         27.43         0.74           8/28/96         14:36:53         5.915         1.632         5.915         26.95         0.73 <td< td=""><td></td><td></td><td></td><td></td><td></td><td>31.32</td><td>0.85</td></td<>						31.32	0.85
8/28/96         14:34:29         3.515         5.367         3.515         30.69         0.83           8/28/96         14:34:42         3.725         5.021         3.725         30.34         0.82           8/28/96         14:34:55         3.946         4.626         3.946         29.95         0.81           8/28/96         14:35:09         4.181         4.253         4.181         29.57         0.80           8/28/96         14:35:24         4.430         3.863         4.430         29.18         0.79           8/28/96         14:35:40         4.693         3.452         4.693         28.77         0.78           8/28/96         14:35:57         4.973         3.030         4.973         28.35         0.77           8/28/96         14:36:15         5.270         2.580         5.270         27.90         0.75           8/28/96         14:36:33         5.583         2.114         5.583         27.43         0.74           8/28/96         14:36:53         5.915         1.632         5.915         26.95         0.73           8/28/96         14:37:14         6.266         1.123         6.266         26.44         0.71 <td< td=""><td></td><td></td><td></td><td></td><td></td><td>31.01</td><td>0.84</td></td<>						31.01	0.84
8/28/96         14:34:42         3.725         5.021         3.725         30.34         0.82           8/28/96         14:34:55         3.946         4.626         3.946         29.95         0.81           8/28/96         14:35:09         4.181         4.253         4.181         29.57         0.80           8/28/96         14:35:24         4.430         3.863         4.430         29.18         0.79           8/28/96         14:35:40         4.693         3.452         4.693         28.77         0.78           8/28/96         14:35:57         4.973         3.030         4.973         28.35         0.77           8/28/96         14:36:15         5.270         2.580         5.270         27.90         0.75           8/28/96         14:36:33         5.583         2.114         5.583         27.43         0.74           8/28/96         14:36:53         5.915         1.632         5.915         26.95         0.73           8/28/96         14:37:14         6.266         1.123         6.266         26.44         0.71           8/28/96         14:37:37         6.640         0.594         6.640         25.91         0.70							0.83
8/28/96         14:34:55         3.946         4.626         3.946         29.95         0.81           8/28/96         14:35:09         4.181         4.253         4.181         29.57         0.80           8/28/96         14:35:24         4.430         3.863         4.430         29.18         0.79           8/28/96         14:35:40         4.693         3.452         4.693         28.77         0.78           8/28/96         14:35:57         4.973         3.030         4.973         28.35         0.77           8/28/96         14:36:15         5.270         2.580         5.270         27.90         0.75           8/28/96         14:36:33         5.583         2.114         5.583         27.43         0.74           8/28/96         14:36:53         5.915         1.632         5.915         26.95         0.73           8/28/96         14:37:14         6.266         1.123         6.266         26.44         0.71           8/28/96         14:37:37         6.640         0.594         6.640         25.91         0.70						30.34	0.82
8/28/96         14:35:09         4.181         4.253         4.181         29.57         0.80           8/28/96         14:35:24         4.430         3.863         4.430         29.18         0.79           8/28/96         14:35:40         4.693         3.452         4.693         28.77         0.78           8/28/96         14:35:57         4.973         3.030         4.973         28.35         0.77           8/28/96         14:36:15         5.270         2.580         5.270         27.90         0.75           8/28/96         14:36:33         5.583         2.114         5.583         27.43         0.74           8/28/96         14:36:53         5.915         1.632         5.915         26.95         0.73           8/28/96         14:37:14         6.266         1.123         6.266         26.44         0.71           8/28/96         14:37:37         6.640         0.594         6.640         25.91         0.70			3.946	4.626	3.946	29.95	0.81
8/28/96         14:35:24         4.430         3.863         4.430         29.18         0.79           8/28/96         14:35:40         4.693         3.452         4.693         28.77         0.78           8/28/96         14:35:57         4.973         3.030         4.973         28.35         0.77           8/28/96         14:36:15         5.270         2.580         5.270         27.90         0.75           8/28/96         14:36:33         5.583         2.114         5.583         27.43         0.74           8/28/96         14:36:53         5.915         1.632         5.915         26.95         0.73           8/28/96         14:37:14         6.266         1.123         6.266         26.44         0.71           8/28/96         14:37:37         6.640         0.594         6.640         25.91         0.70	1 -						0.80
8/28/96         14:35:40         4.693         3.452         4.693         28.77         0.78           8/28/96         14:35:57         4.973         3.030         4.973         28.35         0.77           8/28/96         14:36:15         5.270         2.580         5.270         27.90         0.75           8/28/96         14:36:33         5.583         2.114         5.583         27.43         0.74           8/28/96         14:36:53         5.915         1.632         5.915         26.95         0.73           8/28/96         14:37:14         6.266         1.123         6.266         26.44         0.71           8/28/96         14:37:37         6.640         0.594         6.640         25.91         0.70	1						0.79
8/28/96     14:35:57     4.973     3.030     4.973     28.35     0.77       8/28/96     14:36:15     5.270     2.580     5.270     27.90     0.75       8/28/96     14:36:33     5.583     2.114     5.583     27.43     0.74       8/28/96     14:36:53     5.915     1.632     5.915     26.95     0.73       8/28/96     14:37:14     6.266     1.123     6.266     26.44     0.71       8/28/96     14:37:37     6.640     0.594     6.640     25.91     0.70							0.78
8/28/96     14:36:15     5.270     2.580     5.270     27.90     0.75       8/28/96     14:36:33     5.583     2.114     5.583     27.43     0.74       8/28/96     14:36:53     5.915     1.632     5.915     26.95     0.73       8/28/96     14:37:14     6.266     1.123     6.266     26.44     0.71       8/28/96     14:37:37     6.640     0.594     6.640     25.91     0.70							0.77
8/28/96     14:36:33     5.583     2.114     5.583     27.43     0.74       8/28/96     14:36:53     5.915     1.632     5.915     26.95     0.73       8/28/96     14:37:14     6.266     1.123     6.266     26.44     0.71       8/28/96     14:37:37     6.640     0.594     6.640     25.91     0.70					:		0.75
8/28/96     14:36:53     5.915     1.632     5.915     26.95     0.73       8/28/96     14:37:14     6.266     1.123     6.266     26.44     0.71       8/28/96     14:37:37     6.640     0.594     6.640     25.91     0.70							0.74
8/28/96     14:37:14     6.266     1.123     6.266     26.44     0.71       8/28/96     14:37:37     6.640     0.594     6.640     25.91     0.70	-						0.73
8/28/96 14:37:37 6.640 0.594 6.640 25.91 0.70							0.71
1	_						
	8/28/96	14:38:01	7.035	0.050	7.035	25.37	0.68

DATE	TIME	EVENT	DEPTH TO	TEST	HEAD	HEAD
{		ELAPSED	WATER	ELAPSED		RATIO
		TIME		TIME		
	(HR:M:S)	(MIN)	(FEET)	(MIN)	(FEET)	
8/28/96	14:38:26	7.453	-0.520	7.453	24.80	0.67
8/28/96	14:38:52	7.896	-1.113	7.896	24.21	0.65
8/28/96	14:39:20	8.366	-1.721	8.366	23.60	0.64
8/28/96	14:39:50	8.865	-2.356	8.865	22.96	0.62
8/28/96	14:40:22	9.391	-3.016	9.391	22.30	0.60
8/28/96	14:40:55	9.950	-3.689	9.950	21.63	0.58
8/28/96	14:41:31	10.541	-4.388	10.541	20.93	0.56
8/28/96	14:42:09	11.168	-5.122	11.168	20.20	0.55
8/28/96	14:42:48	11.831	-5.883	11.831	19.44	0.52
8/28/96	14:43:31	12.535	-6.630	12.535	18.69	0.50
8/28/96	14:44:15	13.280	-7.391	13.280	17.93	0.48
8/28/96	14:45:03	14.070	-8.169	14.070	17.15	0.46
8/28/96	14:45:53	14.906	-8.953	14.906	16.37	0.44
8/28/96	14:46:46	15.791	-9.742	15.791	15.58	0.42
8/28/96	14:47:42	16.730	-10.538	16.730	14.78	0.40
8/28/96	14:48:42	17.723	-11.331	17.723	13.99	0.38
8/28/96	14:49:45	18.776	-12.127	18.776	13.19	0.36
8/28/96	14:50:52	19.891	-12.907	19.891	12.41	0.33
8/28/96	14:52:03	21.073	-13.679	21.073	11.64	0.31
8/28/96	14:53:18	22.325	-14.429	22.325	10.89	0.29
8/28/96	14:54:37	23.650	-15.183	23.650	10.14	0.27
8/28/96	14:56:02	25.055	-15.901	25.055	9.42	0.25
8/28/96	14:57:31	26.543	-16.560	26.543	8.76	0.24
8/28/96	14:59:06	28.118	-17.178	28.118	8.14	0.22
8/28/96	15:00:46	29.786	-17.746	29.786	7.57	0.20
8/28/96	15:02:32	31.555	-18.263	31.555	7.06	0.19
8/28/96	15:04:24	33.428	-18.733	33.428	6.59	0.18
8/28/96	15:06:23	35.411	-19.137	35.411	6.18	0.17
8/28/96	15:08:29	37.513	-19.490	37.513	5.83	0.16
8/28/96	15:10:43	39.740	-19.787	39.740	5.53	0.15
8/28/96	15:13:04	42.098	-20.030	42.098	5.29	0.14
8/28/96	15:15:34	44.596	-20.230	44.596	5.09	0.14
8/28/96	15:18:13	47.243	-20.387	47.243	4.93	0.13
8/28/96	15:21:01	50.046	-20.509	50.046	4.81	0.13
8/28/96	15:23:59	53.015	-20.611	53.015	4.71	0.13
8/28/96	15:27:08	56.160	-20.685	56.160	4.63	0.13
8/28/96	15:30:28	59.491	-20.742	59.491	4.58	0.12
8/28/96	15:34:00	63.020	-20.793	63.020	4.53	0.12
8/28/96	15:37:44	66.758	-20.835	66.758	4.48	0.12
8/28/96	15:41:42	70.718	-20.871	70.718	4.45	0.12
8/28/96	15:45:53	74.911	-20.899	74.911	4.42	0.12
8/28/96	15:50:20	79.355	-20.922	79.355	4.40	0.12
8/28/96	15:55:02	84.061	-20.941	84.061	4.38	0.12
8/28/96	16:00:01	89.046	-20.959	89.046	4.36	0.12
8/28/96	16:05:01	94.046	-20.978	94.046	4.34	0.12
8/28/96	16:10:01	99.046	-20.987	99.046	4.33	0.12
8/28/96	16:15:01	104.046	-20.996	104.046	4.32	0.12
8/28/96	16:20:01	109.046	-21.005	109.046	4.31	0.12
8/28/96	16:25:01	114.046	-21.019	114.046	4.30	0.12

## APPENDIX E

Geophysical Testing Procedures, Data, and Results

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## **LIST OF ATTACHMENTS**

Attachment E-1 - Acoustic and Gamma Logging Report

### E. Geophysical Testing

#### E.1 General

The geophysical testing program included the following downhole logging procedures: temperature logging, caliper logging, downhole flowmeter measurements, downhole camera investigation, acoustic logging and natural gamma logging. Geophysical investigations were conducted in the following boreholes/monitoring wells:

Well	Temperature Logging	Caliper Logging	Downhole Flowmeter Measurements	Downhole Camera Investigation	Acoustic Logging	Natural Gamma Logging
MW-2D				Х	Х	х
MW-2R				Х	Х	Х
MW-5D			Х	Х	Х	Х
MW-7D			Х	Х	Х	Х
MW-8R	Х	Х	Х	Х		
MW-11D				Х	Х	Х
MW-14D					Х	X
MW-18D					Х	Х

The following sections include a description of the instruments and methodology used for downhole logging and present the results of the geophysical testing.

#### **E.2** Downhole Temperature and Caliper Logging

Temperature and caliper measurements were conducted in the open corehole MW-8R. A Mt. Sopris Model MGX Digital Logger was used to performed the borehole geophysical logging. The logger consists of an interface/power supply and a hoist/cable reel. The interface/power supply contains the controls for the probe and provides the link between the probe and a portable computer. The hoist/cable reel is motorized and contains a sensor which measures the amount of cable which is unwound to determine the exact elevation of the probe in the hole. The probe was suspended in the center of the hole using a tripod-mounted pulley.

The downhole temperature and caliper logging was conducted using a CTP-2292 3-arm caliper and fluid temperature probe. The probe was attached to the Mt. Sopris Model MGX Digital Logger and the temperature of the borehole fluid was recorded while the probe was lowered into the open borehole MW-8R. The caliper logging was conducted by slowly removing the probe once the bottom of the borehole was reached. The results of temperature and caliper logging are presented in Figure E-1. This investigation method identified a zone with higher temperature gradients at a depth of about 110 feet below ground surface (bgs). The probe and cable spool were decontaminated prior to use.

#### E.3 Downhole Flowmeter Logging

The probe used for the downhole flowmeter logging was a Heat Pulse Flowmeter Model HFP-4293 provided by Colog, Inc. (Colog) of Golden, Colorado. The flowmeter emits a pulse of heat from the center of the probe when a signal is received from the operator. Sensors located above and below the emitter measure the heat pulse as it arrives. A heat pulse received by the lower sensor indicates downward gradients and a heat pulse received by the upper sensor indicates upward gradients. The time delay required for the pulse to reach the sensors indicates the magnitude of the gradients. A series of flexible discs center the instrument in the borehole and seal the space between the probe and the borehole wall. This directs all groundwater flow through the instrument. The probe was attached to the Mt. Sopris Model MGX Digital Logger. The interface/power supply was connected to a portable computer to display and record the digital data.

Since the probe is stationary for flowmeter testing, multiple runs were required for each hole. At least two tests were run at each depth. A test consisted of waiting for the water to stabilize in the borehole, "firing" the heat pulse, and then recording the heat signature. When sufficient data was obtained, the probe was moved to the next location and the procedure repeated. Testing of the hole was complete when the entire open borehole or screened interval was tested. The tests were performed approximately every 5 feet. Flowmeter measurements were conducted initially under static conditions and then in hydrodynamic conditions by pumping at a constant rate from the borehole/well using a Grundfos RediFlo-2 submersible pump located above the screened interval or open portion of the borehole. The probe, cable spool, portable logger and the pump were decontaminated prior to use at each borehole.

suspended on a sheathed cable which was marked at five foot intervals. The camera and light were manually lowered into each well as the depth was manually entered into the character generator every five feet. The camera and light were advanced into the borehole at a rate low enough as to not cause increases in the turbidity of the water. When the bottom of the borehole was reached, the procedure was repeated in the upward direction. The camera, light and cable were decontaminated prior to use at each borehole.

The downhole video investigation identified the presence of a separate phase liquid in well MW-11D. At the same well, the downhole video indicated a potential discrepancy between the installation log and the measured top of the well screen. In addition, the downhole video indicated that the casing of monitoring well MW-2R may not be fully grouted at the contact with the bedrock. To further evaluate these findings acoustic and natural gamma logging was conducted as described in Section **E.5** and Attachment E-1.

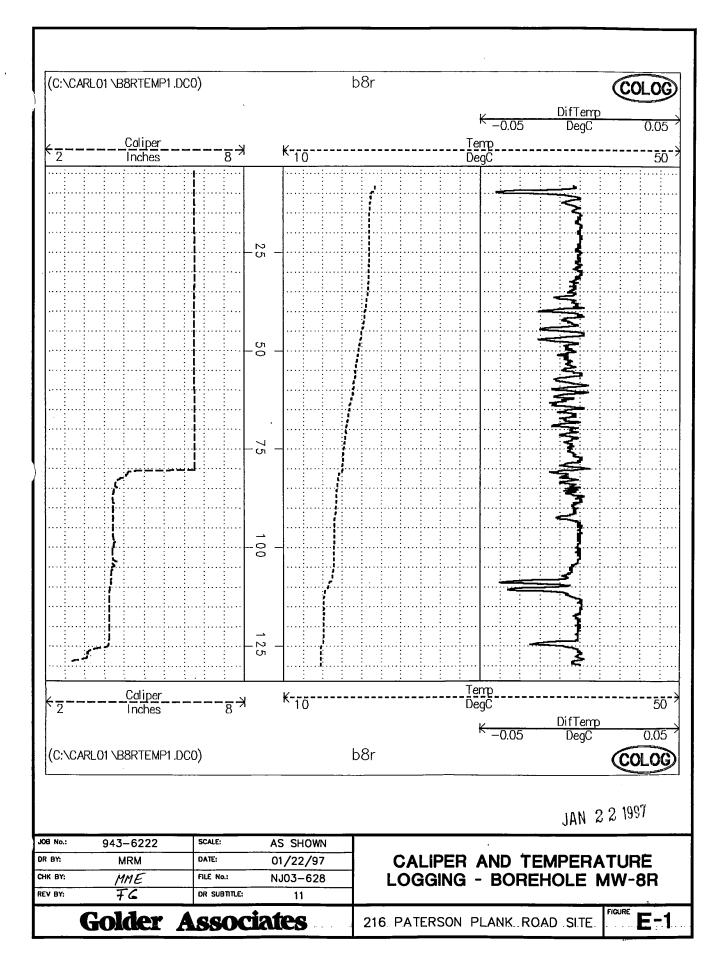
#### E.5 Acoustic and Natural Gamma Logging

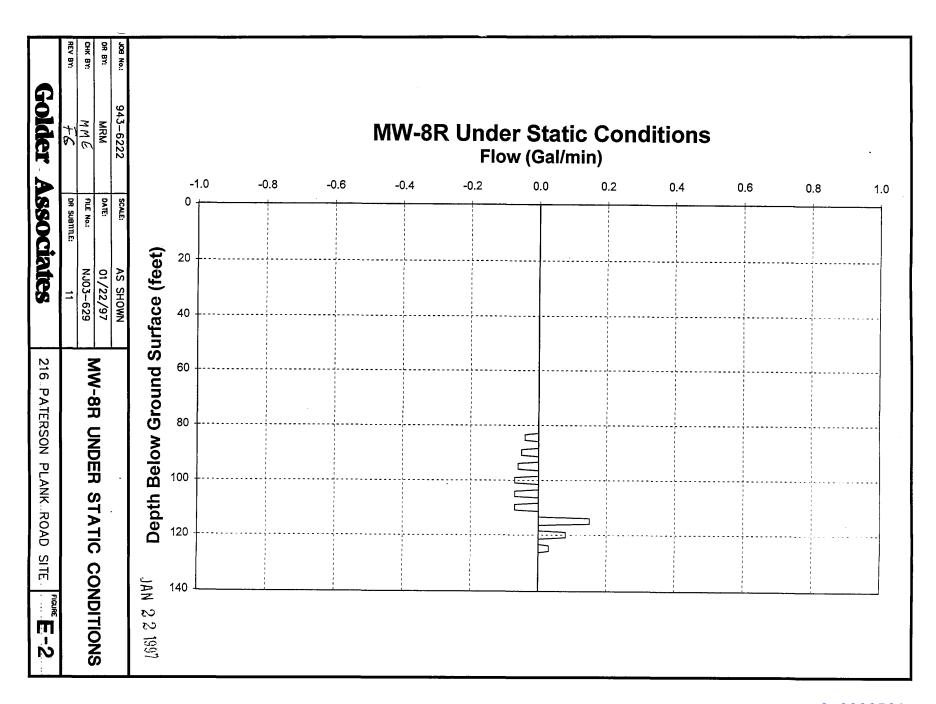
Acoustic and Natural Gamma logging was performed by Colog, Inc. of Golden, Colorado under the supervision of Golder Associates personnel. For the acoustic logging, Colog collected full waveform sonic data using a Mt. Sopris Instrument Company sonic logging probe. The probe consisted of a transmitter and a receiver with a spacing of 4 feet. The natural gamma logging was performed using a Mt. Sopris Instrument Company Model ALP-S Natural Gamma Probe. The probes were suspended in the hole via a motorized hoist/cable which measured the elevation of the probes. The hoist/cable assembly also contained an interface unit which transferred information from the probes and the hoist level sensor to a portable computer. The interface/power supply was connected to a portable computer to display and record the digital data. The computer was connected to a portable printer for review of logs in the field.

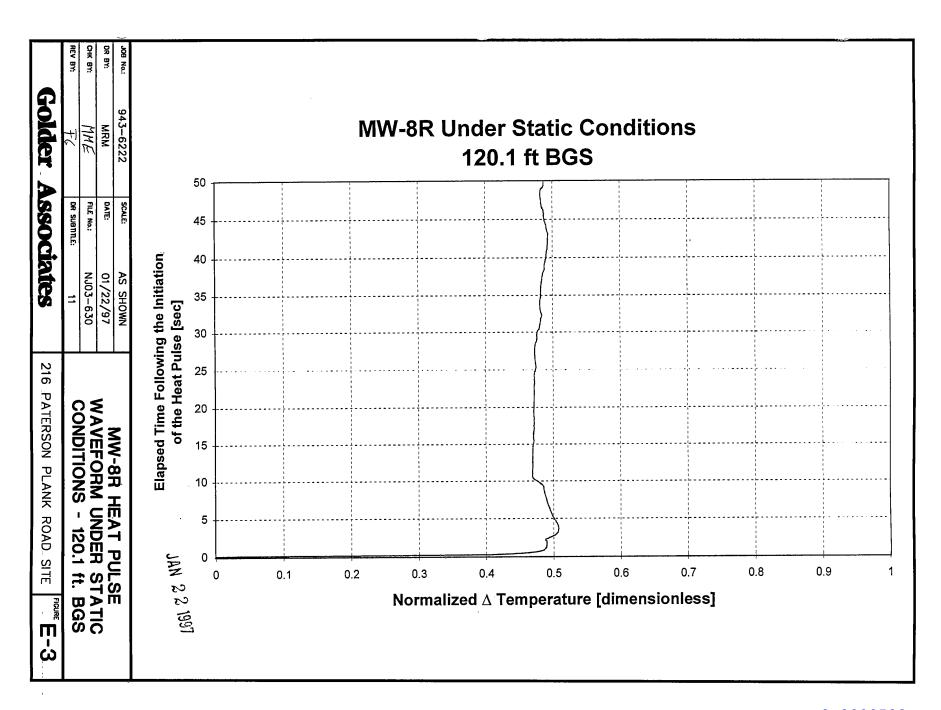
In accordance with standard logging procedures, logging runs were performed from the bottom of the boring upwards. This facilitated maintenance of a constant logging speed, since the probe is more likely to catch on uneven portions of the borehole walls while being lowered down the boring. A logging speed of approximately 1.5 feet per minute was used for the natural gamma runs and 6.0 feet per minute for the acoustic runs. The probes and the hoist/cable assembly were decontaminated prior to use at each borehole.

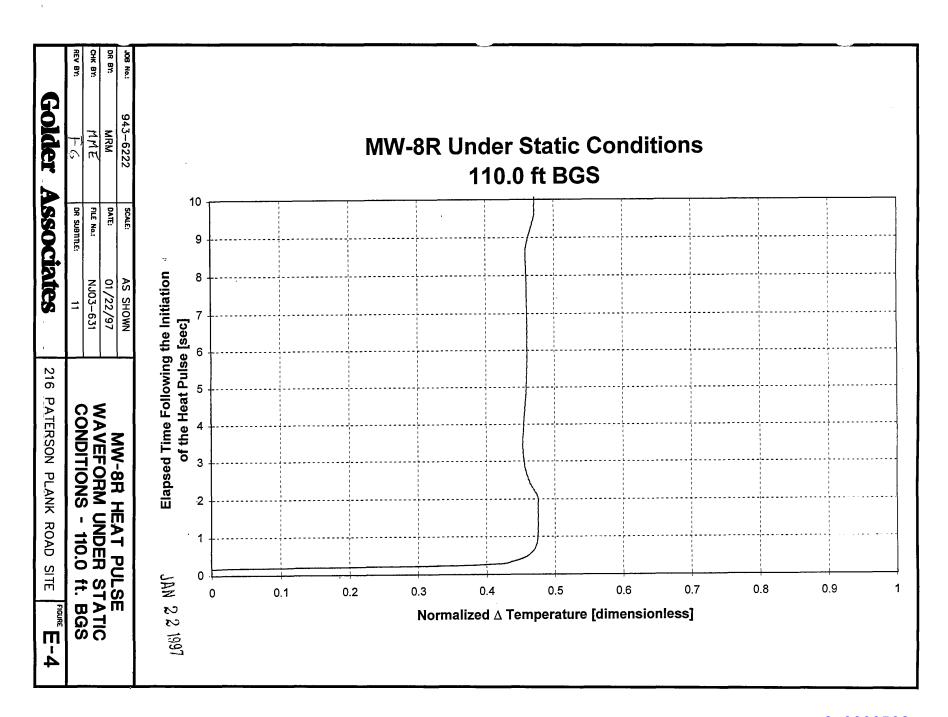
The results of the acoustic and natural gamma logging are presented as Attachment E-1 to this appendix.

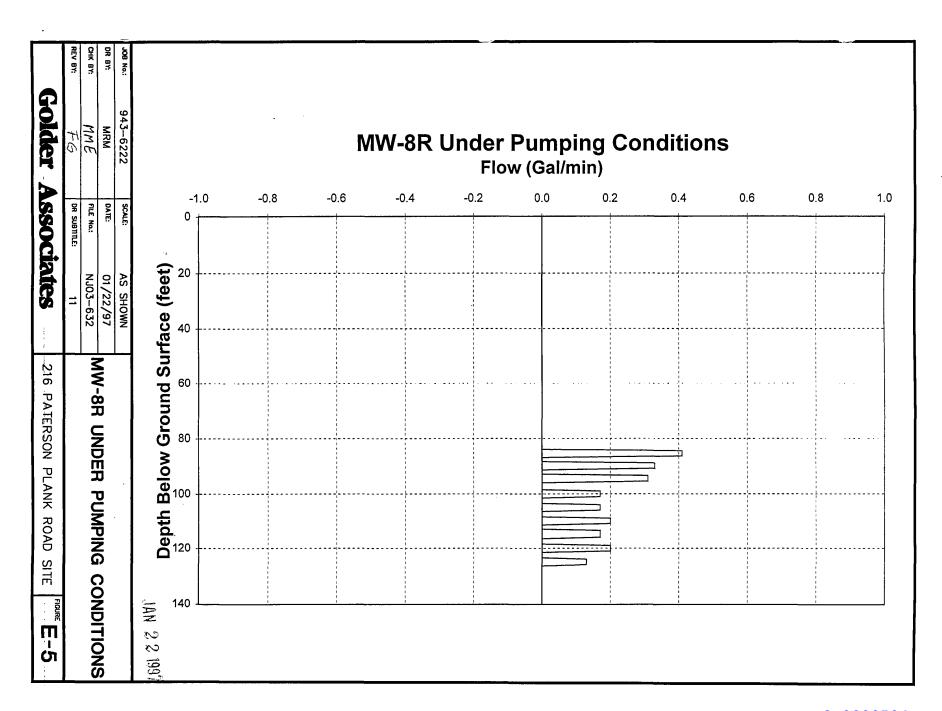
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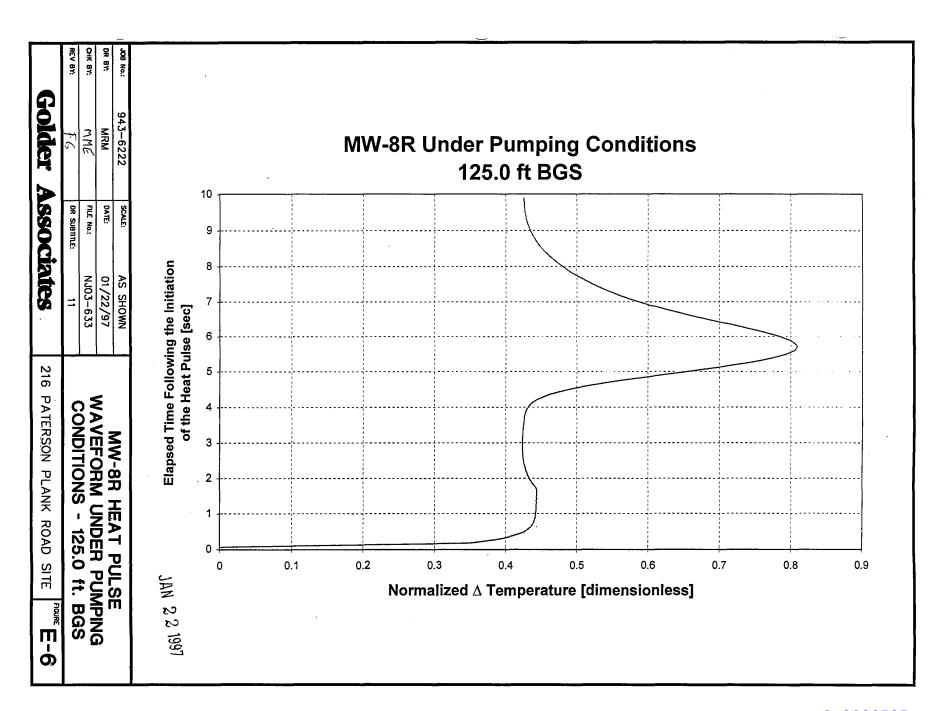


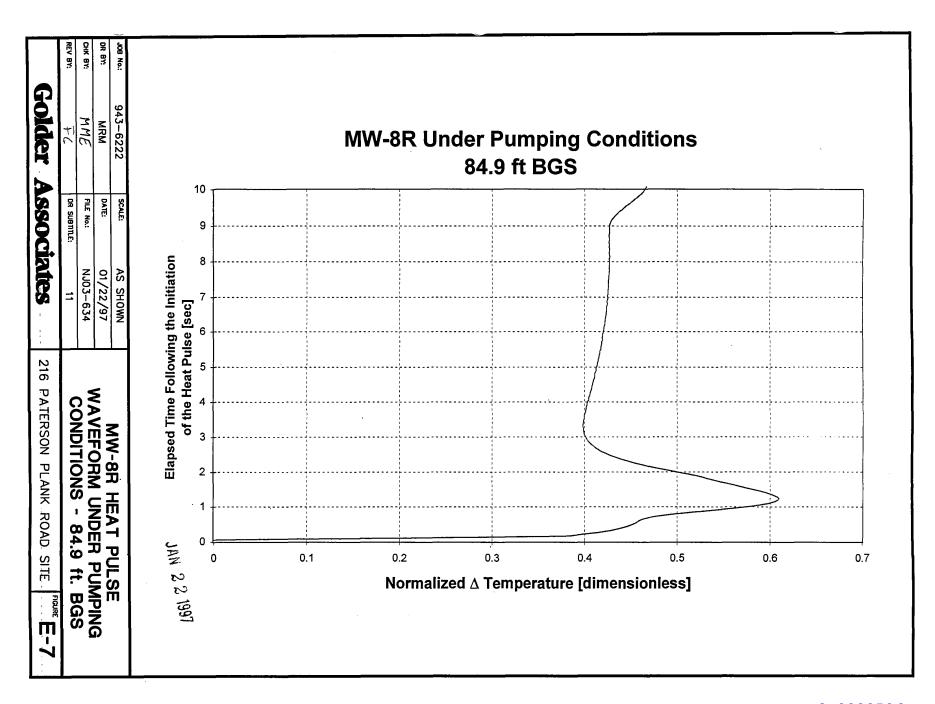


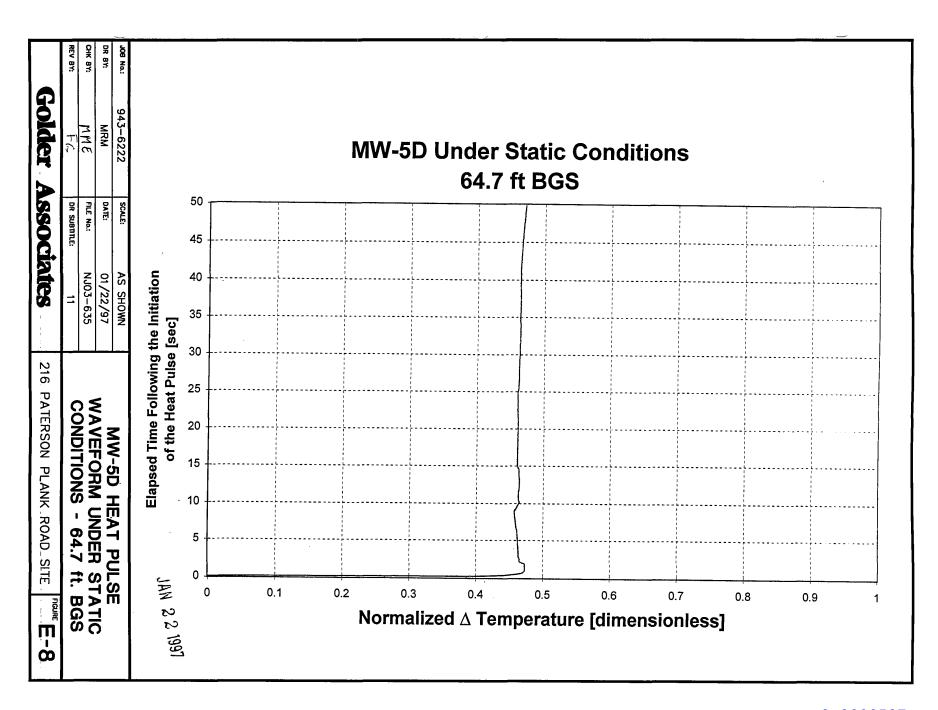


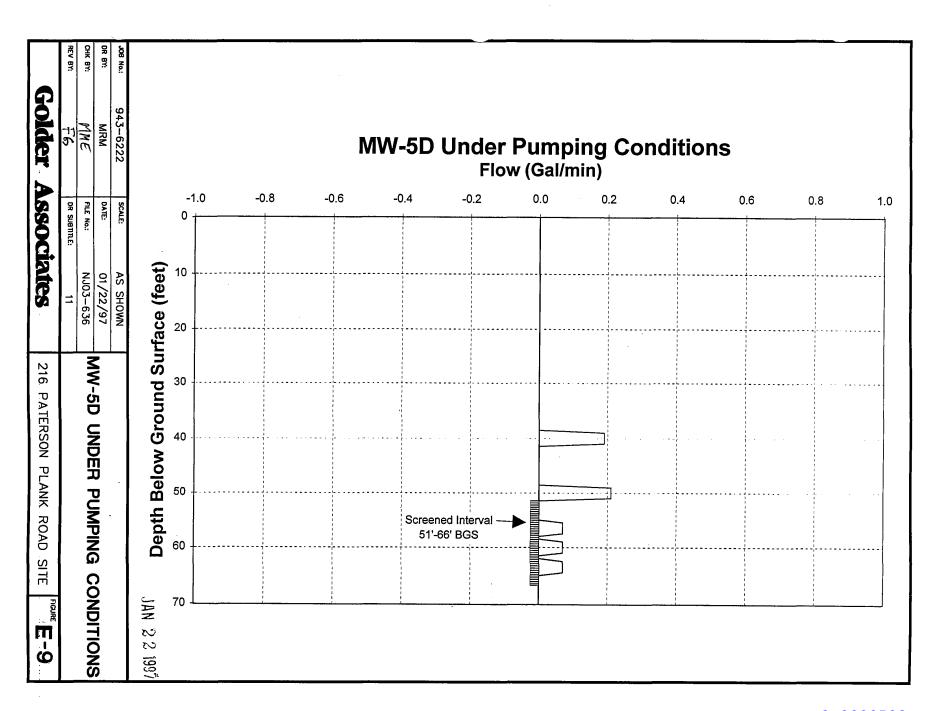


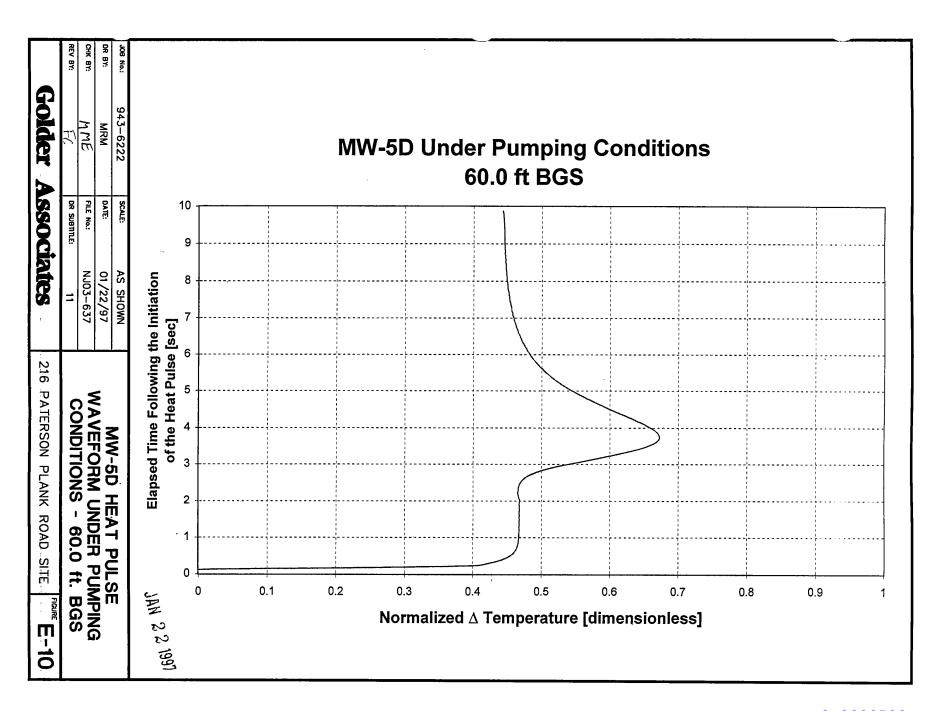


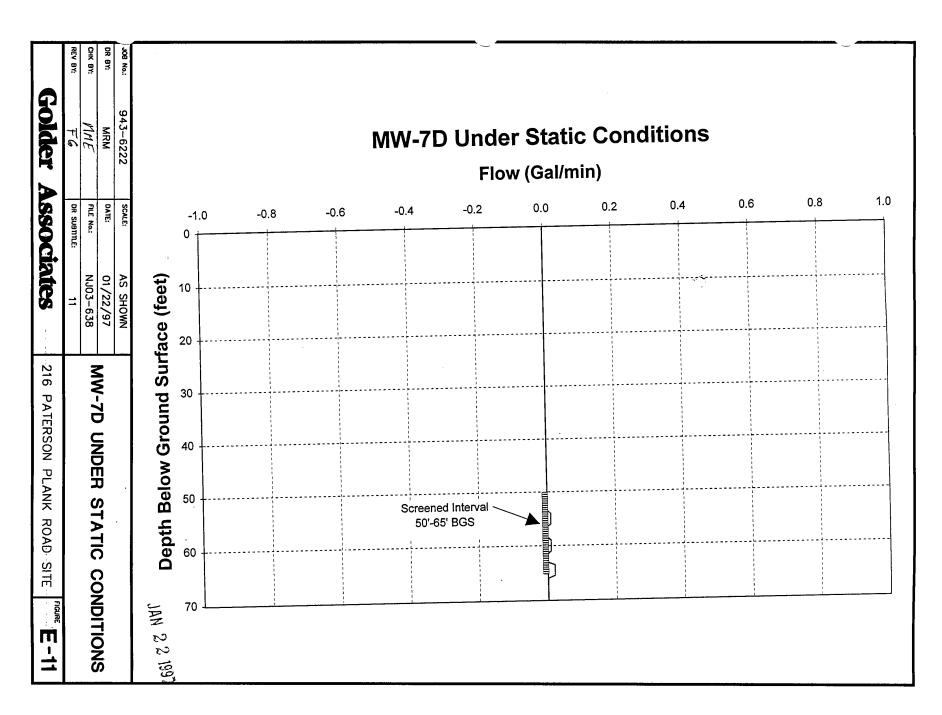


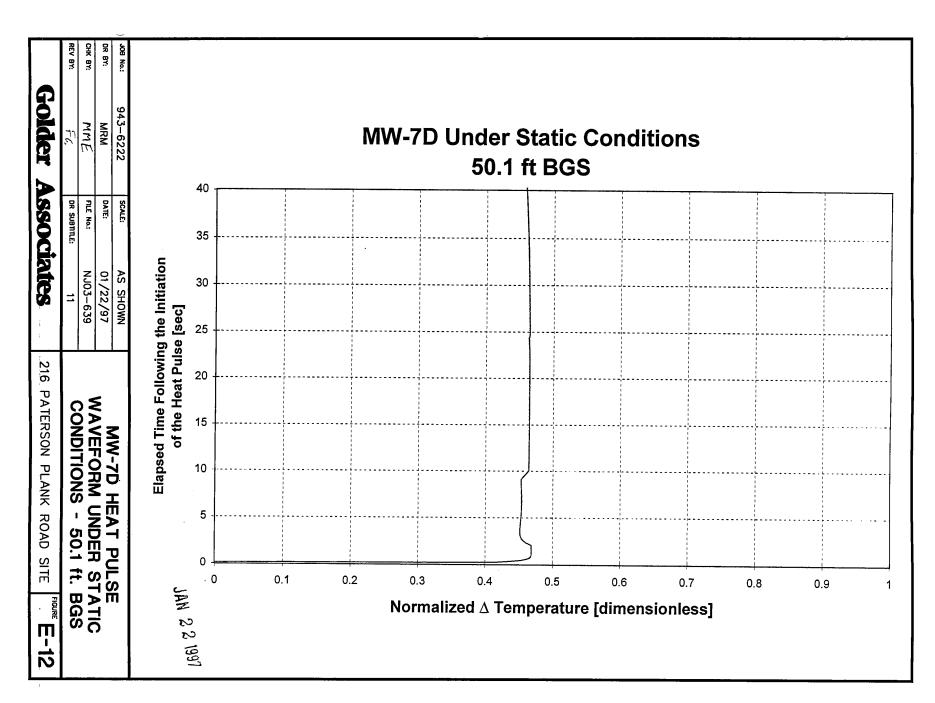


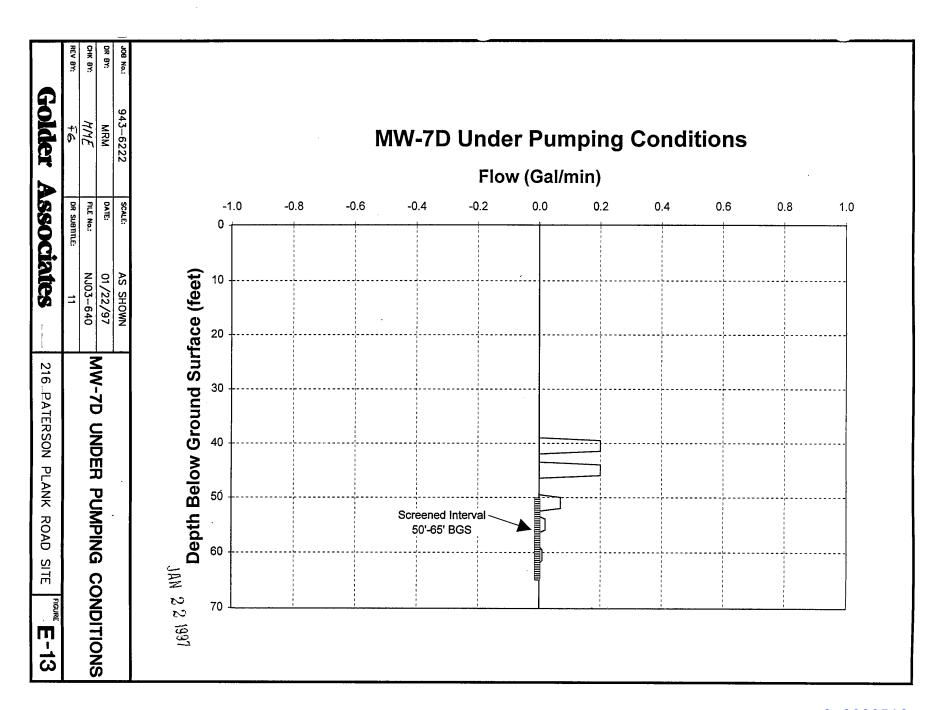


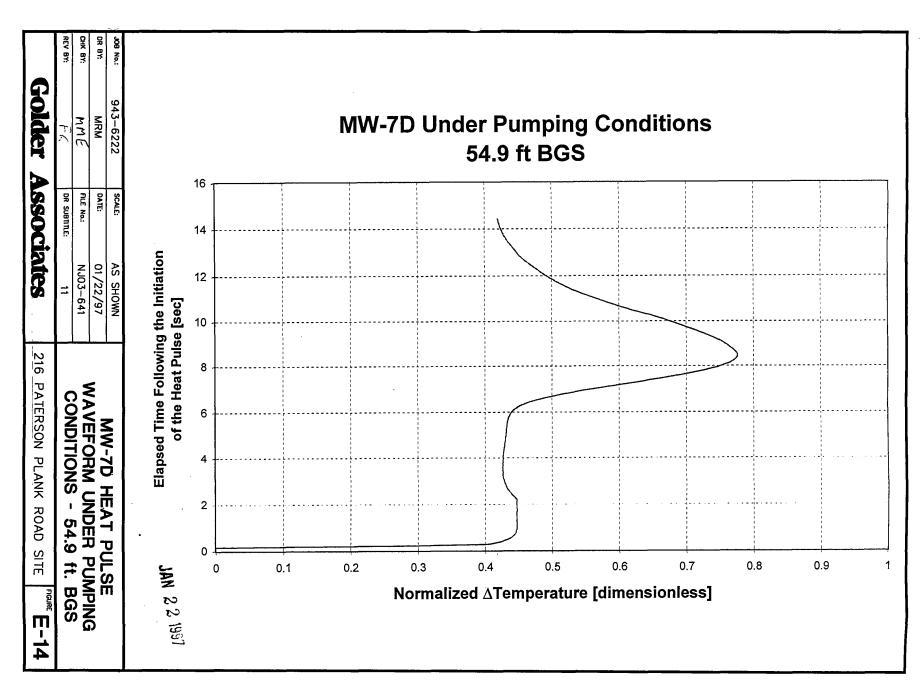












## Attachment E-1

Acoustic and Gamma Logging Report

## Scope of Work:

COLOG collected cement bond logs (CBLs) utilizing a full waveform sonic logging probe and gamma logs in seven existing steel cased wells at the 216 Paterson Plank Road project, New Jersey for Golder Associates on September 25-27, 1996. The goal of this logging program was to investigate the integrity of the bonding in the steel casing in these wells. The following wells were logged:

<u>Well</u>	Logged TD	Basic Construction
MW-2D	56 ft	4 inch Steel Casing and Screen
MW-2R	88 ft	6 inch Steel Casing and Screen
MW-5D	63 ft	4 inch Steel Casing and Screen
MW-7D	63.5 ft	4 inch Steel Casing and Screen
MW-11D	33 ft	4 inch Steel Casing and Screen
MW-14D	36 ft	4 inch Steel Casing and Screen

Post acquisition, COLOG reprocessed the full waveform sonic data and combined it with the gamma log to make final geophysical logs plotted at a scale of 1 inch to 10 ft with a log header. A reproducible original and 4 blueline copies of these logs are enclosed with this report. COLOG also generated a one page color summary plot for each well including well design based on information provided by Golder Associates, a Delta-T (transit time), a bond index determined from the CBL, a sonic waveform for the far receiver and the gamma log. Copies of these Summary Plots have been included with this report and are the basis of the CBL log interpretation

#### **Criteria for Cement Bond Log Interpretation:**

Acoustic Bond Logs have been traditionally used in the petroleum industry to evaluate the bond between steel casing and the grouted material in the annular space around it. Very simply, unbonded or "free" casing tends to "ring" with a smooth high amplitude acoustic wave response with large displacements in the peak-to-peak amplitude (lower frequency) on the variable density sonic waveform display (VDL). Furthermore, the transit time (Delta-T) for steel casing is very consistent at about 57 micro-seconds/foot (approximately 17,500 fps). Well bonded casing, on the other hand, gives a more "muffled (lower amplitude) response. Since the response of the casing is deadened by the cement or grout adhering to it, response from the grout or the formation behind it is evident as later arrivals and erratic response on the VDL with significant variation in Delta-T.

The muffling effect is further evidenced by the "Bond Index" which is reflecting the amplitude of the first arriving acoustic wave associated with the steel casing. Bond Index is scaled from zero to 1 where 1 indicates no bond and zero suggests a well bonded casing. Note that there are other causes of a high Bond Index than poor cement bond. These include, thin grout sheath, low grout strength (e.g. bentonite grout versus cement) and micro-annulus effects.

The differences between bonded and unbonded casing appear fairly obvious on the Summary Plots. The VDL through the free-casing shows very consistent parallel banding and the Delta-T is consistent at  $57 \,\mu\text{S/ft}$ . Bold color variations in the VDL are indicative of the high amplitude "ringing" effect of the acoustic wave traveling through the steel and the Bond Index is near 1. Apparent "free" or unbonded casing is demonstrated in well MW-2R from fluid level to approximately 60 feet with the classic response.

The VDL for bonded casing tends to arrive much later, be more erratic and have a lower amplitude than bonded pipe (more muted blue-green color tones) while the Delta-T is much higher and more variable. The Bond Index for bonded casing is near zero. Apparent well-cemented casing is demonstrated in well MW-7D from approximately 18 to 38 ft with the classic response.

Screened intervals often show parallel banding on the VDL although at a slower Delta-T and later arrival than unbonded casing. Screen is demonstrated in well MW-2D from approximately 46 ft to TD. A bentonite seal (if good integrity) shows a "free" pipe or unbonded casing response (Delta-T is approximately 57 µS/ft) at a slightly lower amplitude than unbonded casing. A bentonite seal is demonstrated in well MW-2D from approximately 40-43 ft. Sometimes, bentonite seals have a higher gamma value; however, this is highly variable. Note that the minimum bed resolution on the VDL is equal to the transmitter-receiver spacing (COLOG shows a 4 foot spacing on the Summary Plots). Thinner features (less than this spacing) are smeared, or show as a transition on the VDL.

COLOG collected full waveform sonic data with a 45mm Mt. Sopris Instrument Co. (MSI) 2 receiver sonic logging tool through the fluid filled section of these seven wells. The amplitude of the first arriving compressional wave associated with the casing is historically referred to as a cement bond log (CBL). The transmitter-receiver spacing for the far receiver on this tool is 4 feet. Assuming steel casing has a transit time of approximately 57 µS/ft and a fluid transit time of approximately 200 µs/ft, the steel arrival occurs at approximately 290-300 micro-seconds on the VDLs.

#### MW-7D

Fluid level

approximately 4 ft

Bentonite seal

39-43 ft (also has slightly higher gamma)

Screen

46 ft-TD

Good Bond

Fair-Poor Bond

Poor Bond

4-9 ft

9-18 ft

18-39 ft

39-43 ft

43-46 ft

#### **MW-11D**

Fluid level

approximately 3 ft

Bentonite seal

19-22 ft (also has slightly higher gamma)

23 ft -TD

Screen

Fair-Poor Bond

8-10 ft

Poor Bond

Poor Bond

4-6 ft

3-8 ft

10-19 ft

Good Bond

19-23 ft

### **MW-14D**

Fluid level

Filter Pack

approximately 2 ft possibly 28-30 ft

30 ft -TD

Screen

Good Bond

Fair-Poor Bond

2-4 ft

6-8 ft 11-13 ft

8-11 ft

13-28 ft

28-30 ft

#### **MW-18D**

Fluid level

approximately 7 ft possibly 55-60 ft?

Filter Pack

60 ft-TD

Screen

Good Bond 7-9 ft

Fair-Poor Bond 9-15 ft

Poor Bond 22-29 ft

15-22 ft

55-60 ft

29-55 ft

## **CBL Interpretation Summaries:**

#### MW-2D

Fluid level approximately 8 ft

Bentonite seal 737-41 ft (also has slightly higher gamma)

Screen 47 ft-TD

 Good Bond
 Fair-Poor Bond
 Poor Bond

 FL-10 ft
 12-20 ft
 10-12 ft

 20-28 ft
 31-34 ft
 28-31 ft

 41-44 ft
 34-41 ft

 44-47 ft

## Well MW-2R

Fluid level approximately 6 ft
Bentonite seal not indicated
Screen not indicated

Bottom of Casing approximately 60 ft

 Good Bond
 Fair-Poor Bond
 Poor Bond

 FL-9 ft
 9-12 ft
 12-22 ft

 22-30 ft
 30-60 ft

#### MW-5D

Fluid level approximately 2 ft

Bentonite seal 43-47 ft (also has slightly higher gamma)

Screen 47 ft - TD

Good Bond Fair-Poor Bond Poor Bond FL-9 ft 12-22 ft 9-12 ft 22-43 ft

#### Limitations:

COLOG's logging was performed in accordance with generally accepted industry practices involving similar studies at the same time and in the same geographical area. COLOG has observed that degree of care and skill generally exercised by others under similar circumstances and conditions. Interpretations of logs or interpretation of test or other data, and any recommendation or hydrogeologic description based upon such interpretations, are opinions based upon inferences from measurements, empirical relationships and assumptions. These inferences and assumptions require engineering judgment, and therefore are not scientific certainties. As such, other professional engineers or analysts may differ as to their interpretation. Accordingly, COLOG cannot and does not warrant the accuracy, correctness or completeness of any such interpretation, recommendation or hydrogeologic description.

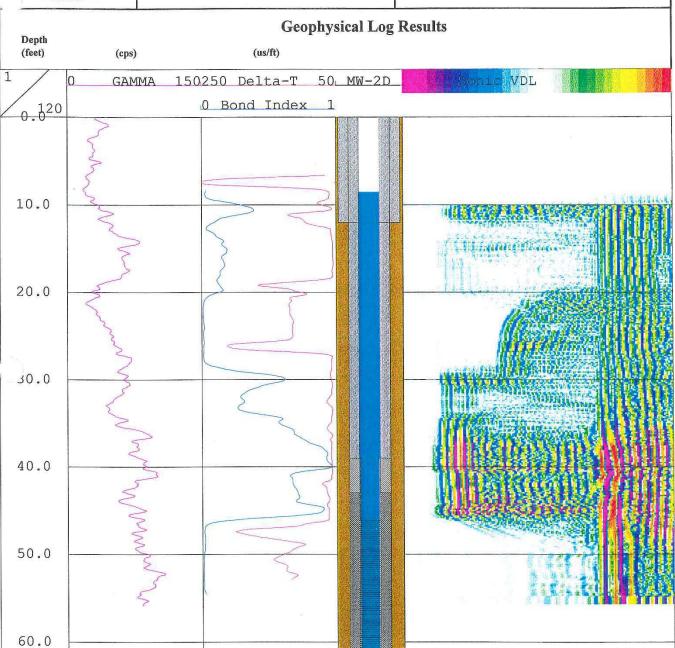
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PROJECT: CARLSTADT

DATE: October 8, 1996

WELL: MW-2D REV: 1.0 BY: NLH

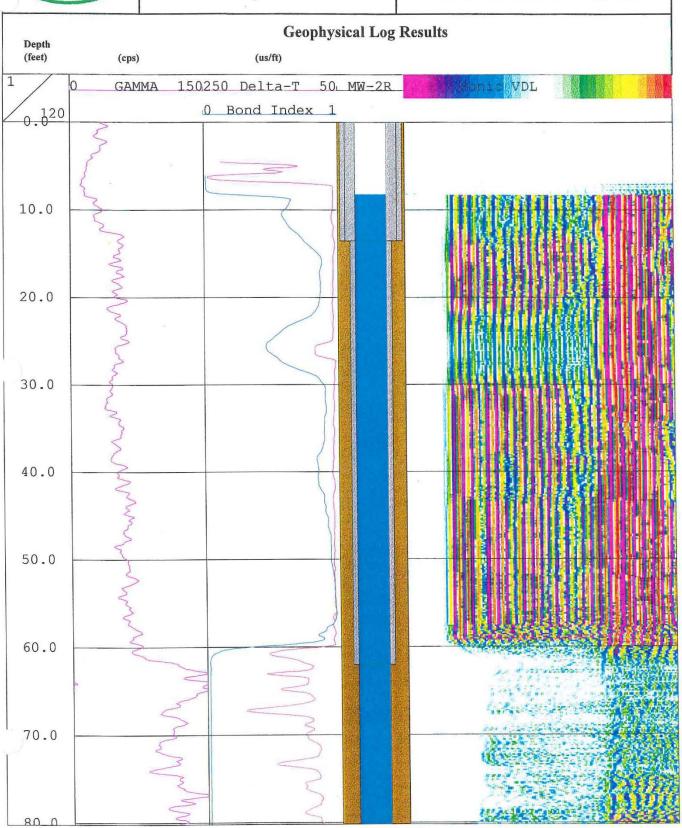




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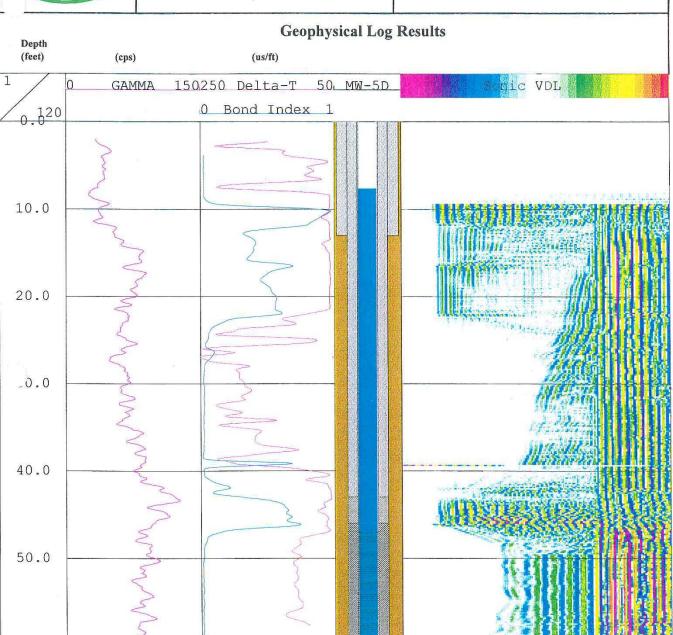


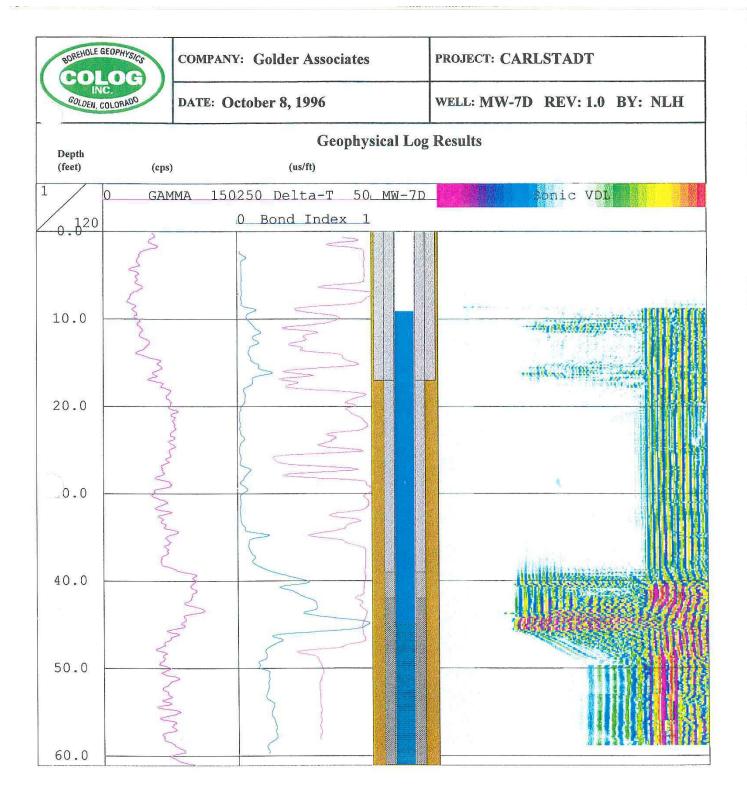


PROJECT: CARLSTADT

DATE: October 8, 1996

WELL: MW-5D REV: 1.0 BY: NLH



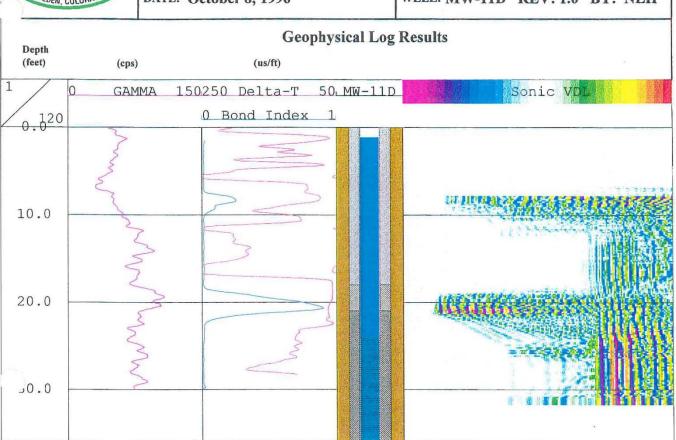


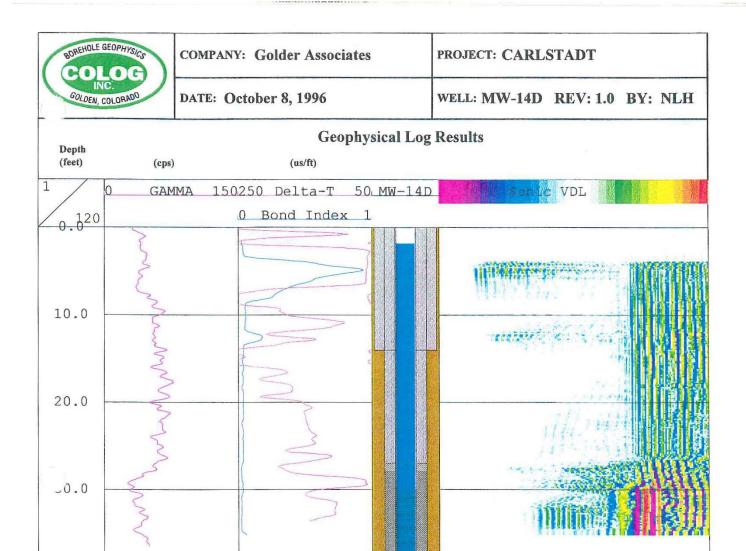


PROJECT: CARLSTADT

DATE: October 8, 1996

WELL: MW-11D REV: 1.0 BY: NLH





40.0

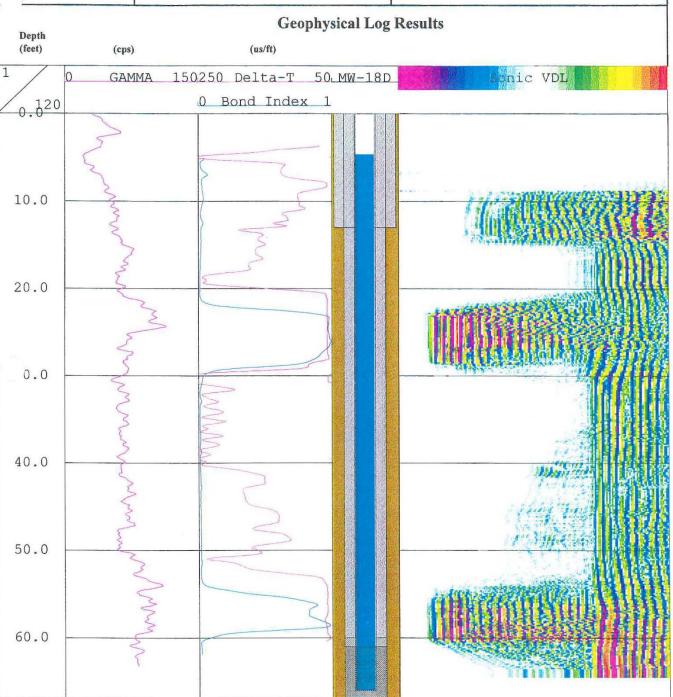


COMPANY: Golder Associates

PROJECT: CARLSTADT

DATE: October 8, 1996

WELL: MW-18D REV: 1.0 BY: NLH



#### APPENDIX F

Summary of Low Flow Purging Information

#### SUMMARY OF PURGING INFORMATION MONITORING WELL MW-02D SEPTEMBER 1996 GROUNDWATER SAMPLING EVENT 216 PATERSON PLANK ROAD SITE CARLSTADT, NEW JERSEY

	Elapsed			Specific		<b>-</b>	Dissolved	Depth To	Volume	Approximate
Time (HH:MM)	Time (HH:MM)	Temperature (oC)	pH (std)	Conductance (mS)	eH (mv)	Turbidity (NTU)	Oxygen (mg/l)	Water (ft. btc)	Purged (Liters)	Purge Rate (ml/min)
15:38	00:00			BEGIN PURC	SING			12.00		
15:39	00:01	14.9	8.23	3.29	30.3	10.0	-0.80		0.3	300
15:42	00:04	15.0	8.20	3.28	20.8	0.0	-0.85		0.6	100
15:45	00:07	15.3	8.08	3.30	18.6	0.0	-0.91	- "	0.9	100
15:47	00:09	15.6	8.04	3.24	31.7	0.0	-0.85		1.5	200
15:50	00:12	15.7	8.03	3.16	32.8	0.0	-0.78		2.5	330
15:53	00:15	15.8	8.13	3.08	58.3	0.0	-0.78		3.5	330
15:56	00:18	15.8	8.16	2.99	96.8	0.0	-0.77		4.5	330
15:59	00:21	15.8	8.16	2.96	115.0	0.0	-0.80		5.5	330
16:02	00:24	15.8	8.18	2.94	118.0	0.0	-0.84	14.00	6.5	330
16:15	00:37			BEGIN SAMP	LING					

### SUMMARY OF PURGING INFORMATION MONITORING WELL MW-02R SEPTEMBER 1996 GROUNDWATER SAMPLING EVENT 216 PATERSON PLANK ROAD SITE CARLSTADT, NEW JERSEY

	Elapsed			Specific		·	Dissolved	Depth To	Volume	Approximate
Time	Time	Temperature	pН	Conductance	eН	Turbidity	Oxygen ·	Water	Purged	Purge Rate
(HH:MM)	(HH:MM)	(°C)	(std)	(mS)	(mv)	(NTU)	(mg/l)	(ft. btc)	(Liters)	(ml/min)
08:57	00:00			BEGIN PUR	SING			11.20		
08:58	00:01	16.0	8.35	1.90	93.0	0.0	3.85		0.2	200
9:07	00:10	14.9	10.59	2.23	11.7	0.0	0.80		2.0	200
9:11	00:14	15.0	10.60	2.27	-4.1	0.0	0.55		3.5	
9:14	00:17	14.9	10.59	2.29	-3.3	0.0	0.71		4.2	
9:19	00:22	14.9	10.60	2.30	-12.0	0.0	0.43		5.2	
9:22	00:25	14.9	10.61	2.30	-13.0	0.0	0.38	11.95	5.8	
9:25	00:28	14.9	10.62	2.30	-16.3	0.0	0.37		6.4	200
9:29	00:32	14.9	10.63	2.31	-22.2	0.0	0.37	11.95	7.2	200
9:45	00:48			BEGIN SAMP	LING			11.94		

### SUMMARY OF PURGING INFORMATION MONITORING WELL MW-05D SEPTEMBER 1996 GROUNDWATER SAMPLING EVENT 216 PATERSON PLANK ROAD SITE CARLSTADT, NEW JERSEY

Time (HH:MM)	Elapsed Time (HH:MM)	Temperature (°C)	pH (std)	Specific Conductance (mS)	eH (mv)	Turbidity (NTU)	Dissolved Oxygen (mg/l)	Depth To Water (ft. btc)	Volume Purged (Liters)	Approximate Purge Rate (ml/min)
08:57	00:00			BEGIN PUR	SING			10.50		
09:06	00:09	16.0	7.19	1.64	98.5	0.0	3.28	11.00	1.4	160
9:11	00:14	15.9	7.55	1.70	66.8	0.0	2.82		2.1	155
9:16	00:19	16.0	7.63	1.69	61.2	0.0	2.70		3.0	180
9:20	00:23			BEGIN SAMP	LING					

### SUMMARY OF PURGING INFORMATION MONITORING WELL MW-07D SEPTEMBER 1996 GROUNDWATER SAMPLING EVENT 216 PATERSON PLANK ROAD SITE CARLSTADT, NEW JERSEY

Time (HH:MM)	Elapsed Time (HH:MM)	Temperature (°C)	pH (std)	Specific Conductance (mS)	eH (mv)	Turbidity (NTU)	Dissolved Oxygen (mg/l)	Depth To Water (ft. btc)	Volume Purged (Liters)	Approximate Purge Rate (ml/min)
13:07	00:00			BEGIN PUR	SING			11.03		
13:15	00:08	17.4	7.74	0.806	94.0	0.0	4.14		0.80	100
13:24	00:17	17.2	8.13	0.796	70.3	0.0	3.39	11.45	2.15	150
13:30	00:23	17.2	8.20	0.793	64.8	0.0	2.85		3.05	150
13:36	00:29	17.2	8.24	0.793	61.6	0.0	2.94	11.70	3.95	150
13:40	00:33			BEGIN SAMP	LING					

#### SUMMARY OF PURGING INFORMATION MONITORING WELL MW-08D SEPTEMBER 1996 GROUNDWATER SAMPLING EVENT 216 PATERSON PLANK ROAD SITE CARLSTADT, NEW JERSEY

	Elapsed			Specific			Dissolved	Depth To	Volume	Approximate
Time	Time	Temperature	рΗ	Conductance	eН	Turbidity	Oxygen	Water	Purged	Purge Rate
(HH:MM)	(HH:MM)	(°C)	(std)	(mS)	(mv)	(NTU)	(mg/l)	(ft. btc)	(Liters)	(ml/min)
14:17	00:00			BEGIN PURC	ING			4.40		
14:21	00:04	16.5	8.07	2.28	41.5	590.0	-0.59	5.40	0.8	200
14:25	00:08	16.7	8.09	2.28	33.0	532.0	-0.58	5.40	1.5	175
14:30	00:13	16.8	8.08	2.28	23.6	503.0	-0.57	5.40	2.2	140
14:35	00:18	18.3	8.11	2.32	88.3	511.0	0.22		2.5	60
14:42	00:25	18.3	8.09	2.32	54.4	509.0	-0.07	5.40	2.8	45
14:49	00:32	18.5	8.09	2.31	20.3	509.0	0.02	5.65	3.2	
14:55	00:38	17.9	8.14	2.32	-14.3	>999	-0.65		3.6	
15:09	00:52	17.9	8.11	2.31	7.4	>999	0.70		4.6	70
15:14	00:57	17.9	8.12	2.32	-10.4	>999	0.77	5.95	5.3	140
15:20	01:03	17.9	8.17	2.31	-30.3	>999	0.59	5.96	6.2	150
15:25	01:08	17.8	8.18	2.30	-35.2	>999	0.45	5.97	6.8	120
15:30	01:13	17.8	8.18	2.30	-47.9	>999	0.23		7.4	120
15:35	01:18	17.8	8.18	2.30	-60.3	>999	0.18		8.1	140
15:40	01:23	17.8	8.18	2.30	-60.0	900.0	0.14	5.99	8.7	120
15:45	01:28	17.8	8.18	2.30	-60.0	839.0	0.12	5.99	9.5	160
15:50	01:33	17.8	8.18	2.30	-57.2	783.0	0.03	5.99	10.1	120
15:55	01:38	17.7	8.19	2.30	-57.2	753.0	0.04	5.99	10.7	120
16:00	01:43	17.7	8.19	2.30	-52.1	717.0	-0.07		11.3	120
16:03	01:46	17.7	8.19	2.29	-60.4	608.0	-0.21		11.7	130
16:10	01:53	17.7	8.19	2.29	-72.3	622.0	-0.21	5.96	12.9	170
16:15	01:58	17.7	8.19	2.27	-73.9	542.0	-0.31	5.96	13.8	160
16:20	02:03	17.7	8.19	2.26	-77.8	507.0	-0.33		14.7	180
16:25	02:08	17.7	8.19	2.27	-69.7	527.0	-0.34		16.4	300
16:35	02:18	17.6	8.19	2.27	-71.7	429.0	-0.40	5.96	19.9	350
16:45	02:28	17.5	8.20	2.25	-70.4	393.0	-0.54	-	23.4	350
16:50	02:33	17.5	8.20	2.23	-74.1	353.0	-0.51		25.1	340
17:00	02:43	17.5	8.20	2.22	-73.1	389.0	-0.57	5.99	28.6	300
17:05	02:48			BEGIN SAMP	LING					

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## SUMMARY OF PURGING INFORMATION MONITORING WELL MW-08R SEPTEMBER 1996 GROUNDWATER SAMPLING EVENT 216 PATERSON PLANK ROAD SITE CARLSTADT, NEW JERSEY

	Elapsed			Specific			Dissolved	Depth To	Volume	Approximate
Time	Time	Temperature	pН	Conductance	eН	Turbidity	Oxygen	Water	Purged	Purge Rate
(HH:MM)	(HH:MM)	(°C)	(std)	(mS)	(mv)	(NTU)	(mg/l)	(ft. btc)	(Liters)	(ml/min)
09:05	00:00			BEGIN SAMP	LING			5.11		
09:15	00:10	16.9	10.35	2.67	-80.2	0.0	2.45	5.55	1.8	180
9:18	00:13	17.0	10.63	2.66	-88.8	14.0	2.01	5.56	2.3	180
9:25	00:20	17.0	10.75	2.67	-89.7	19.0	1.59	5.56	3.5	180
9:30	00:25	17.1	10.75	2.66	-83.0	13.0	1.46	5.65	4.4	120
9:35	00:30	17.1	10.75	2.67	-76.0	7.0	1.36	5.60	4.8	80
9:40	00:35	17.1	10.74	2.68	-77.1	8.0	1.41	5.60	5.2	80
9:43	00:38	17.1	10.73	2.67	-76.2	7.0	1.46		5.7	180
9:45	00:40			BEGIN SAMP	LING					

## SUMMARY OF PURGING INFORMATION MONITORING WELL MW-10D SEPTEMBER 1996 GROUNDWATER SAMPLING EVENT 216 PATERSON PLANK ROAD SITE CARLSTADT, NEW JERSEY

	Elapsed			Specific			Dissolved	Depth To	Volume	Approximate
Time	Time	Temperature	pН	Conductance	еН	Turbidity	Oxygen	Water	Purged	Purge Rate
(HH:MM)	(HH:MM)	(°C)	(std)	(mS)	(mv)	(NTU)	(mg/l)	(ft. btc)	(Liters)	(ml/min)
8:41	00:00			BEGIN PURC	SING			7.05		
8:45	00:04	17.6	11.08	1.01	-7.5	26.0	3.21		0.6	160
9:00	00:19	17.2	11.09	1.09	1.0	26.0	2.81	8.11	1.2	160
9:05	00:24	17.2	11.09	1.10	-0.8	18.0	3.14	8.70	2.3	220
9:10	00:29	17.6	11.08	1.11	0.1	13.0	3.10	9.38	3.3	190
9:18	00:37	17.5	11.08	1.11	1.6	11.0	3.13	10.30	5.3	250
9:26	00:45	17.9	11.07	1.10	3.7	4.0	2.65	11.10	8.6	400
9:36	00:55	17.8	11.08	1.11	6.0	0.0	2.73	12.30	12.6	400
9:41	01:00	18.0	11.07	1.10	3.0	0.0	2.68	12.52	14.6	400
9:45	01:04	17.9	11.08	1.11	3.5	0.0	2.97		16.2	400
9:50	01:09	18.1	11.07	1.11	2.3	0.0	2.62	13.48	18.2	400
10:00	01:19			BEGIN SAMP	LING				Ť	

### SUMMARY OF PURGING INFORMATION MONITORING WELL MW-10R SEPTEMBER 1996 GROUNDWATER SAMPLING EVENT 216 PATERSON PLANK ROAD SITE CARLSTADT, NEW JERSEY

	Elapsed			Specific			Dissolved	Depth To	Volume	Approximate
Time	Time	Temperature	pН	Conductance	еН	Turbidity	Oxygen	Water	Purged	Purge Rate
(HH:MM)	(HH:MM)	(°C)	(std)	(mS)	(mv)	(NTU)	(mg/l)	(ft. btc)	(Liters)	(ml/min)
11:50	00:00			BEGIN PURC	ING			7.15		
11:55	00:05	19.7	9.18	0.589		46.0	1.67	7.25	0.3	200
11:59	00:09	18.6	9.66	0.619	22.6	227.0	0.91	7.35	1.4	275
12:04	00:14	17.7	9.91	0.643	4.0	564.0	0.04	7.37	2.9	300
12:09	00:19	17.7	9.91	0.647	-8.2	409.0	-0.23	7.38	4.4	300
12:16	00:26	17.7	9.91	0.644	-14.8	343.0	-0.25	7.39	6.5	300
12:21	00:31	17.7	9.88	0.650	-21.5	327.0	-0.21	7.39	8.0	300
12:26	00:36	17.6	9.90	0.652	-25.1	300.0	-0.12	7.40	9.5	300
12:31	00:41	17.6	9.90	0.653	-28.1	277.0	-0.21	7.40	11.0	300
12:34	00:44	17.6	9.91	0.654	-32.6	270.0	-0.26	7.40	12.5	300
12:38	00:48	17.6	9.93	0.655	-35.4	248.0	-0.37	7.40	13.7	300
12:42	00:52	17.6	9.94	0.657	-36.3	178.0	-0.31	7.40	14.9	300
12:47	00:57	17.6	9.95	0.657	-37.3	148.0	-0.38	7.40	16.3	280
12:53	01:03	17.6	9.98	0.657	-39.8	150.0	-0.43	7.40	18.1	300
13:00	01:10	17.6	10.01	0.656	-42.2	92.0	-0.45	7.40	20.2	300
13:04	01:14	17.6	10.02	0.656	-45.2	77.0	-0.48	7.40	21.4	300
13:08	01:18	17.6	10.03	0.657	-47.0	63.0	-0.48	7.40	22.6	300
13:12	01:22	17.7	10.04	0.656	-49.7	64.0	-0.48	7.40	23.8	300
13:16	01:26	17.7	10.06	0.656	-51.8	60.0	-0.48	7.40	25.0	300
13:18	01:28			BEGIN SAMP	LING					

## SUMMARY OF PURGING INFORMATION MONITORING WELL MW-11D SEPTEMBER 1996 GROUNDWATER SAMPLING EVENT 216 PATERSON PLANK ROAD SITE CARLSTADT, NEW JERSEY

	Elapsed			Specific			Dissolved	Depth To	Volume	Approximate
Time	Time	Temperature	pН	Conductance	eН	Turbidity	Oxygen	Water	Purged	Purge Rate
(HH:MM)	(HH:MM)	(°C)	(std)	(mS)	(mv)	(NTU)	(mg/l)	(ft. btc)	(Liters)	(ml/min)
10:26	00:00			BEGIN SAMP	LING			5.25		
10:28	00:02	17.0	8.96	0.813		50.0	1.30	5.40	0.3	150
10:33	00:07	16.4	9.10	1.120	-0.1	42.0	0.38	5.52	1.0	200
10:38	00:12	16.6	9.30	1.160	<b>-</b> 9.6	58.0	-0.01	5.55	1.5	100
10:42	00:16	16.6	9.34	1.180	-11.5	66.0	-0.10	5.50	2.2	175
10:46	00:20	16.6	9.34	1.190	-13.2	84.0	-0.09	5.56	2.8	150
10:51	00:25	16.6	9.35	1.200	-15.5	88.0	-0.04	5.56	3.5	150
10:56	00:30	16.6	9.36	1.210	-23.5	85.0	0.04	5.57	4.3	150
11:02	00:36	16.7	9.35	1.210	-29.1	75.0	0.01	5.57	5.2	150
11:09	00:43	16.8	9.34	1.210	-37.4	66.0	-0.05	5.58	5.8	100
11:14	00:48	16.8	9.34	1.210	-38.8	65.0	-0.10	5.58	6.4	120
11:19	00:53	16.9	9.33	1.210	-38.9	55.0	-0.22	5.59	7.0	120
11:24	00:58	16.9	9.33	1.210	-39.1	49.0	-0.24	5.59	7.6	120
11:29	01:03	17.0	9.33	1.210	-40.9	49.0	-0.29	5.58	8.4	160
11:32	01:06			BEGIN SAMP	LING					

## SUMMARY OF PURGING INFORMATION MONITORING WELL MW-11R SEPTEMBER 1996 GROUNDWATER SAMPLING EVENT 216 PATERSON PLANK ROAD SITE CARLSTADT, NEW JERSEY

, , , , ,	Elapsed			Specific			Dissolved	Depth To	Volume	Approximate
Time	Time	Temperature	рН	Conductance	еН	Turbidity	Oxygen	Water	Purged	Purge Rate
(HH:MM)	(HH:MM)	(°C)	(std)	(mS)	(mv)	(NTU)	(mg/l)	(ft. btc)	(Liters)	(ml/min)
10:03	00:00			BEGIN PURC	SING			6.00		
10:07	00:04	15.7	11.24	1.33	-3.6	2.0	2.07	6.06	1.1	280
10:12	00:09	15.6	11.26	1.40	-77.7	8.0	1.86	6.07	2.5	280
10:17	00:14	15.7	11.24	1.37	-97.9	7.0	1.54	6.09	3.9	280
10:22	00:19	16.2	11.17	1.30	-111.7	7.0	1.36	6.10	5.9	400
10:27	00:24	16.3	11.12	1.24	-121.7	4.0	1.31	6.10	8.4	500
10:32	00:29	16.4	11.08	1.20	-104.9	1.0	1.23	6.11	10.8	480
10:37	00:34	16.4	11.06	1.17	-124.3	0.0	1.25	6.12	13.2	480
10:42	00:39	16.5	11.05	1.16	-131.4	0.0	1.21	6.12	15.6	480
10:45	00:42			BEGIN SAMP	LING					

### SUMMARY OF PURGING INFORMATION MONITORING WELL MW-12D SEPTEMBER 1996 GROUNDWATER SAMPLING EVENT 216 PATERSON PLANK ROAD SITE CARLSTADT, NEW JERSEY

	Elapsed			Specific			Dissolved	Depth To	Volume	Approximate
Time	Time	Temperature	рН	Conductance	eН	Turbidity	Oxygen	Water	Purged	Purge Rate
(HH:MM)	(HH:MM)	(°C)	(std)	(mS)	(mv)	(NTU)	(mg/l)	(ft. btc)	(Liters)	(ml/min)
11:12	00:00			BEGIN PURC	ING			5.62		
11:15	00:03	10.6	6.68	1.16		65.0	1.43	5.85	0.40	130
11:19	00:07	16.1	6.94	1.66	-118.2	68.0	1.17	5.93	0.80	100
11:24	00:12	16.1	6.93	1.94	-115.0	62.0	0.59	5.90	1.80	200
11:28	00:16	16.1	6.94	1.98	-115.3	59.0	0.43	5.90	2.80	250
11:32	00:20	16.1	6.95	2.00	-118.5	58.0	0.44	5.90	3.80	250
11:36	00:24	16.1	6.95	2.01	-119.6	59.0	0.44	5.90	4.60	200
11:41	00:29	16.1	6.96	2.02	-121.2	59.0	0.44	5.90	5.60	200
11:42	00:30			BEGIN SAMP	LING					

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### SUMMARY OF PURGING INFORMATION MONITORING WELL RMW-13D SEPTEMBER 1996 GROUNDWATER SAMPLING EVENT 216 PATERSON PLANK ROAD SITE CARLSTADT, NEW JERSEY

	Elapsed			Specific			Dissolved	Depth To	Volume	Approximate
Time	Time	Temperature	pН	Conductance	eН	Turbidity	Oxygen	Water	Purged	Purge Rate
(HH:MM)	(HH:MM)	(°C)	(std)	(mS)	(mv)	(NTU)	(mg/l)	(ft. btc)	(Liters)	(ml/min)
10:54	00:00			BEGIN PURG	ING			4.51		
10:55	00:01	16.9	10.73	1.49	88.9	8.0	2.70	4.58	0.54	540
11:00	00:06	17.0	10.27	1.44	95.8	10.0	1.59	4.56	2.90	470
11:05	00:11	17.3	9.99	1.43	102.1	6.0	1.36	4.50	4.50	320
11:10	00:16	17.7	9.80	1.42	106.5	5.0	1.34	4.50	5.70	240
11:15	00:21	17.7	9.73	1.42	101.7	4.0	1.28	4.50	6.90	240
11:20	00:26	17.8	9.70	1.41	97.1	4.0	1.26	4.50	8.10	240
11:25	00:31			BEGIN SAMP	LING					

## SUMMARY OF PURGING INFORMATION MONITORING WELL MW-14D SEPTEMBER 1996 GROUNDWATER SAMPLING EVENT 216 PATERSON PLANK ROAD SITE CARLSTADT, NEW JERSEY

	Elapsed			Specific			Dissolved	Depth To	Volume	Approximate
Time	Time	Temperature	pН	Conductance	еН	Turbidity	Oxygen	Water	Purged	Purge Rate
(HH:MM)	(HH:MM)	(°C)	(std)	(mS)	(mv)	(NTU)	(mg/l)	(ft. btc)	(Liters)	(ml/min)
8:14	00:00			BEGIN PURC	SING			1.13		
8:15	00:01	16.6	9.94	2.62	-55.5	21.0	2.60	1.84	0.24	240
8:20	00:06	16.7	10.55	1.91	-72.1	55.0	2.36	1.91	1.00	160
8:25	00:11	17.3	10.82	1.74	-66.9	65.0	1.71	1.97	1.40	80
8:30	00:16	17.6	10.97	1.69	-65.1	60.0	1.34	2.22	1.80	80
8:35	00:21	17.9	11.07	1.65	-68.0	47.0	1.68	2.31	2.20	80
8:40	00:26	18.1	11.10	1.64	-66.4	30.0	1.56	2.33	2.60	80
8:45	00:31	18.2	11.12	1.63	-65.0	22.0	1.57	2.35	3.00	80
8:50	00:36	18.3	11.12	1.62	-65.3	21.0	1.47	2.36	3.40	80
8:55	00:41	18.7	11.13	1.61	-68.3	16.0	1.49	2.47	3.80	80
9:00	00:46	18.6	11.14	1.62	-62.9	16.0	1.38	2.51	4.20	80
9:05	00:51	18.7	11.19	1.61	-70.6	9.0	1.53	2.53	4.60	80
9:15	01:01	18.8	11.18	1.61	-79.2	9.0	1.41	2.65	5.00	80
9:20	01:06			BEGIN SAMP	LING					

## SUMMARY OF PURGING INFORMATION MONITORING WELL MW-14R SEPTEMBER 1996 GROUNDWATER SAMPLING EVENT 216 PATERSON PLANK ROAD SITE CARLSTADT, NEW JERSEY

	Elapsed			Specific			Dissolved	Depth To	Volume	Approximate
Time	Time	Temperature	pН	Conductance	eН	Turbidity	Oxygen	Water	Purged	Purge Rate
(HH:MM)	(HH:MM)	(°C)	(std)	(mS)	(mv)	(NTU)	(mg/l)	(ft. btc)	(Liters)	(ml/min)
8:22	00:00			BEGIN PURG	SING			1.68		
8:24	00:02	15.4	9.94	0.745	-92.8	61.0	-0.27	2.98	2.4	1200
8:27	00:05	15.5	10.22	0.898	-92.1	63.0	-0.66	3.19	4.3	630
8:30	00:08	16.1	10.30	0.962	-90.4	57.0	-0.75		5.9	530
8:33	00:11	16.4	10.31	0.990	-89.3	64.0	-0.75	3.22	6.9	330
8:36	00:14	16.6	10.31	1.050	-85.5	62.0	-0.72	3.25	7.9	330
8:39	00:17	16.7	10.29	1.060	-89.3	57.0	-0.74	3.26	8.9	330
8:42	00:20	16.8	10.27	1.080	-93.3	60.0	-0.71	3.27	10.0	370
8:45	00:23	16.9	10.24	1.070	-98.2	59.0	-0.71	3.27	11.0	330
8:48	00:26	17.0	10.20	1.080	-102.4	60.0	-0.69	3.28	12.0	330
8:51	00:29	17.1	10.13	1.080	-105.9	62.0	-0.69		12.9	300
8:54	00:32	17.1	10.02	1.080	-115.1	63.0	-0.72	3.28	13.8	300
8:58	00:36	17.1	10.03	1.080	-119.8	60.0	-0.71	3.28	14.7	225
9:01	00:39	17.1	10.03	1.070	-124.3	57.0	-0.69	3.29	15.6	300
9:05	00:43			BEGIN SAMP	LING					

## SUMMARY OF PURGING INFORMATION MONITORING WELL MW-15D SEPTEMBER 1996 GROUNDWATER SAMPLING EVENT 216 PATERSON PLANK ROAD SITE CARLSTADT, NEW JERSEY

	Elapsed			Specific			Dissolved	Depth To	Volume	Approximate
Time	Time	Temperature	pН	Conductance	eН	Turbidity	Oxygen	Water	Purged	Purge Rate
(HH:MM)	(HH:MM)	(°C)	(std)	(mS)	(mv)	(NTU)	(mg/l)	(ft. btc)	(Liters)	(ml/min)
8:00	00:00			BEGIN PURC	SING			9.15		
8:05	00:05	16.0	11.09	1.38		1.0	1.23	9.30	0.4	80
8:10	00:10	15.8	11.22	1.38		0.0	0.86	9.36	0.9	100
8:15	00:15	15.6	11.26	1.39	-115.2	0.0	0.66	9.42	1.4	100
8:20	00:20	15.4	11.31	1.40	-120.4	0.0	· 0.77	9.50	1.8	80
8:25	00:25	15.3	11.36	1.41	-125.1	1.0	0.72	9.51	2.8	200
8:30	00:30	15.2	11.41	1.41	-121.6	11.0	0.65	9.51	3.8	200
8:35	00:35	15.1	11.47	1.41	-119.4	20.0	0.70	9.53	4.8	200
8:40	00:40	15.9	11.61	1.63	-117.4	6.0	-0.05		5.8	200
8:45	00:45	15.9	11.63	1.60	-115.6	11.0	-0.06	9.54	6.5	140
8:50	00:50	.15.8	11.64	1.62	-116.0	8.0	-0.12	9.54	7.3	160
8:55	00:55	15.8	11.65	1.63	-117.5	8.0	-0.10	9.54	8.0	140
9:00	01:00	15.7	11.67	1.64	-118.1	8.0	-0.09	9.55	9.8	160
9:05	01:05			BEGIN SAMP	LING					

### SUMMARY OF PURGING INFORMATION MONITORING WELL MW-16D SEPTEMBER 1996 GROUNDWATER SAMPLING EVENT 216 PATERSON PLANK ROAD SITE CARLSTADT, NEW JERSEY

	Elapsed			Specific			Dissolved	Depth To	Volume	Approximate
Time	Time	Temperature	рН	Conductance	еН	Turbidity	Oxygen	Water	Purged	Purge Rate
(HH:MM)	(HH:MM)	(°C)	(std)	(mS)	(mv)	(NTU)	(mg/l)	(ft. btc)	(Liters)	(ml/min)
13:44	00:00			BEGIN PURC	SING			6.43		
13:45	00:01	16.0	11.76	2.97	31.9	27.0	2.20	6.54	0.2	220
13:50	00:06	16.0	11.79	3.18	18.0	26.0	1.86	6.56	1.3	220
13:55	00:11	16.1	11.79	3.21	3.2	22.0	1.79	6.56	2.5	230
14:00	00:16	16.2	11.78	3.19	-29.4	21.0	1.61	6.57	3.7	240
14:05	00:21	16.4	11.76	3.11	-46.8	12.0	1.49	6.59	4.9	240
14:10	00:26	16.5	11.73	3.02	-57.5	8.0	1.44	6.59	6.1	240
14:15	00:31	16.5	11.70	2.88	-61.8	5.0	1.58	6.57	7.3	240
14:20	00:36	16.5	11.69	2.83	-65.2	3.0	1.48	6.57	8.5	240
14:25	00:41	16.5	11.67	2.68	-69.7	3.0	1.47	6.57	9.7	240
14:30	00:46	16.4	11.65	2.59	-72.9	1.0	1.42	6.60	10.9	240
14:35	00:51	16.3	11.63	2.50	-68.6	1.0	1.32	6.61	12.1	240
14:45	01:01			BEGIN SAMP	LING					

# SUMMARY OF PURGING INFORMATION MONITORING WELL MW-17D SEPTEMBER 1996 GROUNDWATER SAMPLING EVENT 216 PATERSON PLANK ROAD SITE CARLSTADT, NEW JERSEY

	Elapsed			Specific			Dissolved	Depth To	Volume	Approximate
Time	Time	Temperature	pН	Conductance	еН	Turbidity	Oxygen	Water	Purged	Purge Rate
(HH:MM)	(HH:MM)	(°C)	(std)	(mS)	(mv)	(NTU)	(mg/l)	(ft. btc)	(Liters)	(ml/min)
9:11	00:00			BEGIN PURC	SING			4.16		
9:12	00:01	17.6	8.97	2.44	88.3	-8.0	0.59		0.3	300
9:17	00:06	17.7	7.76	2.60		169.0	0.27	4.40	1.8	300
9:24	00:13	16.8	7.27	2.79	-140.6	686.0	-0.29	4.62	3.0	170
9:30	00:19	16.8	7.29	2.79	-156.9		-0.63	4.69	4.0	170
9:43	00:32	17.1	7.13	2.85	-158.8	386.0	-0.32	4.70	6.2	170
9:52	00:41	17.1	7.15	2.85	-165.6	206.0	-0.44		11.5	590
9:57	00:46	17.0	7.14	2.85	-165.5	165.0	-0.56		13.0	300
10:04	00:53	17.1	7.12	2.85	-164.6	131.0	-0.71	4.71	15.2	315
10:15	01:04	17.1	7.11	2.86	-162.2	134.0	-0.74	4.72	18.5	300
10:19	01:08	17.1	7.11	2.86	-161.8	131.0	-0.79	4.72	19.7	300
10:21	01:10			BEGIN SAMP	LING					

### SUMMARY OF PURGING INFORMATION MONITORING WELL MW-18D SEPTEMBER 1996 GROUNDWATER SAMPLING EVENT 216 PATERSON PLANK ROAD SITE CARLSTADT, NEW JERSEY

	Elapsed			Specific			Dissolved	Depth To	Volume	Approximate
Time	Time	Temperature	pН	Conductance	еН	Turbidity	Oxygen	Water	Purged	Purge Rate
(HH:MM)	(HH:MM)	(°C)	(std)	(mS)	(mv)	(NTU)	(mg/l)	(ft. btc)	(Liters)	(ml/min)
11:44	00:00			BEGIN PURC	ING			4.13		
11:45	00:01	16.8	7.35	2.79	52.7	237.0	2.04	4.69	0.3	300
11:50	00:06	16.2	7.54	2.85	20.4	>999	1.24	4.77	2.1	350
12:00	00:16	16.6	7.40	2.89	-8.2	>999	1.10	4.65	4.1	400
12:08	00:24	17.1	7.36	2.89	-13.3	550.0	1.08	4.54	6.8	340
12:25	00:41	17.7	7.32	2.47	53.5	480.0	2.43	4.61	11.2	260
12:35	00:51	17.0	7.27	2.84	17.7	78.0	1.26	4.61	13.6	260
12:45	01:01	16.9	7.27	2.88	14.0	38.0	1.12	4.61	16.0	240
12:55	01:11	16.9	7.26	2.89	15.4	21.0	1.07	4.61	18.4	240
13:00	01:16	16.9	7.26	2.89	14.3	17.0	1.07	4.60	20.8	240
13:05	01:21	16.9	7.26	2.89	14.1	17.0	1.06	4.63	23.2	240
13:15	01:31			BEGIN SAMP	LING					

APPENDIX G

Chain of Custody Forms

R2-0000546

COMPUCHEM
_NVIRONMENTAL
CORPORATION

#### CHAIN-OF-CUL JDY RECORD

Nº 10031

	RATION	Ship to:				Project N	eme:	00	10	40	44	-	F	eld F	oint	of-Contact;	٥١	:
3306 Chapel Hil/Neison i Research Triangle Park, N		Cor	npu C	rhem		Sampler	Neme:		د.				T	elept	юла	No.: 609	- 27:	3-1110
		<u> </u>				Mike	Zar	<u> 275</u>	لكف	<u>12</u>	4	nde	<u> </u>	empl	ing t	or project com	plete? Y	or (See Note 1)
1-800-833-5097		Carrier:	Alrbi	11 No.: 755	346	Sampler	Bignatu a0	if <del>e</del> ;					P	rojec	t-spe	elfic (PS) or B	atch (B) C	· .
				35 E 6 0 0	<b>交</b> 得让								Ta.			A flammer		
				O Die S Kin Pres											D in			
		Box #1 Box	20 Ban #1	30x #4 Box #1			Organic	- An		RESERVED IN COLUMN TO SERVED genics	Oth	200	- 100	16 JA				
Sample ID	1	DOX # 1 DOX	3	202 #3   DOX #3	'		TT	TT	ŤŦ	11	T	ΙÏ	ÎΤ	П				
(Organics: 9 characters marc Inorganics: 6 characters;	F. 19	. 3	3	56	불	45 45	7 MS 45 C		11	H	l la	8	×	_[	-	Re	marka /	Comments
Sen Note 2 )	Date: Year: 19	Martix	History/Unfilter	Method Expect Conc.	No, of Bottles	Use for Lab GC (NS or DUP)	VOA-GC/MS SV.GC/MS Pest/PCB-GC	99		200	Oys. Fe	000	TOC/TOX	뒿			,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	
	Date	Preser Preser	# :	₹ 8 2	ટ્ર	35	\$ 8 8	<b>1</b>	11	3 5	80	2	ğ		5			
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RBGWOI	05'21 TI'P	wo	Flu	CK	9	<b>©</b> m²	XXX			x	VE		11	$\prod$		Filter		
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MW-20	21311615	WO	Flu (	7	4				$\dagger \dagger$	X	×			11	1	να's -		
	1111815	<b>10</b>	1:15		13	1-1	*	$\dagger \dagger$	H	7	++^	$\dag \uparrow$	1	††	+		1	
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Cilent's Special Instructions:			<u></u>		<del></del>	J		<del></del>	1		لاللل			ــــــــــــــــــــــــــــــــــــــ				
Lab: Received in Good Condition?	Y or N	Describe Probi	ome, If Anyz															
#1 Fielinquished By: (Sig.) M	ozameli.	Cate Q [7						Daller			nedatuge		<b>(a)</b>				Date:	Sample storage time requested?
Company Name: Gald	er UASS.		Company Nam		' <del>A</del> -			lme:	•	_	y Name:						Time:	(In days, see Note 3)
#1 Flacelyed By: (S/g.)		Date:		37: (Blo )							olved By:	(561)		<u> </u>	<u>.</u>	<del></del>	Date:	DESTROY or RETURN data siter the years of archivist?
Соглрану Name:		Time:	Company Nam	Comen	ch	<u> </u>	]7	Inet?	Ø	Сопред	y Name:				•		Time:	(Circle chalce; see Note 4)

Company Name:

| Time: | Company Name: | Time: | Company Name: | Time: | Company Name: | Time: | Company Name: | Time: | Company Name: | Time: | Company Name: | Time: | Company Name: | Time: | Company Name: | Time: | Company Name: | Time: | Company Name: | Time: | Company Name: | Time: | Company Name: | Time: | Company Name: | Time: | Company Name: | Time: | Company Name: | Time: | Company Name: | Time: | Company Name: | Time: | Company Name: | Time: | Company Name: | Time: | Company Name: | Time: | Company Name: | Time: | Company Name: | Time: | Company Name: | Time: | Company Name: | Time: | Company Name: | Time: | Company Name: | Time: | Company Name: | Time: | Company Name: | Time: | Company Name: | Time: | Company Name: | Time: | Company Name: | Time: | Company Name: | Time: | Company Name: | Time: | Company Name: | Time: | Company Name: | Time: | Company Name: | Time: | Company Name: | Time: | Company Name: | Time: | Company Name: | Time: | Company Name: | Time: | Company Name: | Time: | Company Name: | Time: | Company Name: | Time: | Company Name: | Time: | Company Name: | Time: | Company Name: | Time: | Company Name: | Time: | Company Name: | Time: | Company Name: | Time: | Company Name: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time: | Time:

1-800-833-5097

09-19-96 08:55AM

POQ3

#1 Received By: (Sig.) Company Name:

Bolt #1 | Surface Wester 2. Ground Wester ; 3. Lanchele

#### CHAIN-OF-CUSTODY RECORD

3306 Chapel Hill/Nelson Highway Research Triangle Park, NC 27709

Strip to:	Project Name: Can 15 tand+	Field Point of Contact Lon, Heidel
(WAY PO COST)	Serripler Harms:  JBH/SN	Telephone No: 609-273-1/10 Sampling for project complete? Ed. (See Note 1.)
Corrier Albanyo: Fedex 15503457	Sampler Storage Samuel	Project-specific (PS) or Betch (B) QC:

			6	Rk	1/S	dio	, in		<b>6</b>																				i,					<b>** 0</b>		
	(O	or, i	nici not	6; 8 124	ohe ples	: 6				Date: Year: 19	Time		Metrix gon al	Preservative g	1	Filtered/Unflered &	Method Bex #4	Espect, Conc.	No. of Bottles	Use for Lab QC (MS or DUP)	VOA-GCMS 9	Т	Pert/PCB-GC	T	T		Mercury	1	Radiologicais.	$\prod$	Маложо	Prenote		Remari	ks/Comm	nents
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	_					s (		X		Y ON H	1	7 	Date	1	'nŀ		Anne Relinquis		ş.)(ş				<u>:</u>	_	Deter			<b>131</b>	_	_		y: (81	<b>N</b>		Ontex	Germple storage time requested?

High (1): If "N" Lab will hold samples to await remainder of project-maniphing plants also she and minimizing OC ratio; if "I" lab will begin processing batches now. Hole (I): If CLP inoppanies disturbs required, (2) Analysis and pays for return of explore general storage has blind in Jeanway at year six.

DESTROY or HETURN
date wher his peers of
erchive? (Circle ofleror,
see Hote 4)

#### CHAIN-OF-CUS.JDY RECORD

73

CORPORATION	Ship to:	Project Name: Carlstadt	Field Point-of-Conlact: Loni Herdel
3306 Chapel Hill/Nelson Highway Research Triangle Park, NC 27709	Compuchen	Sampler Name: Sm/m=/JZH/SN	Telephone No.: 605 273   110
		· SM/ME/JUN/SM	Sampling for project complete? Y or (N) (See Note 1)
1-800-833-5097	Cerrier: Airbill No.: Fedex 7550361512	Klennill	Project-specific (PS) or Batch (B) QC:
BOX #1: L Chrisce Water 8 Trip Blank #2:	Box #2: AHC	Bot #3 refinere	COLP (900 PL Feetingles) Bott #5 H. High PWA-88 COVA BOD series - COMM   1
2 Ground Water 7, Oil (2)	C.NatSO/ N. Ned Preserved		COVA 600 series COVIG
6. Soil / Sedment (Bledge) / (1997)	"DN»(6-C)		Longer CIP
<b>加州</b> 沙埃。 《河景·雅斯曾被"新"。	x #1 Box #2 Box #3 Box #4 Box #5	Organice Analysis Inorganice Other	CONTRACTOR OF STATE O
			· · · · · · · · · · · · · · · · · · ·
Sample ID (Organica: 9 characters max, progenica: 6 characters; L	p 2 3	S 8 8 8	
See Note 2)		10 00 00 00 00 00 00 00 00 00 00 00 00 0	Hemarks / Comments
ineganics: 6 characters; See Note 2) :- in a	Preservative Filtered/Unflered Mothod Expect. Conc.	Use for Lab OC (MS or DUP) VOA-GC/MS SV-GC/MS Pest/PCB-GC WARTAIS Mercury Cyanides Radiologicals TOC / TOX	Other Other
	GBFCLI		
	GBUCLI		TRON ONLY, DISSOLVED
<del>▎▗╎╸╿╺╎╺╽</del> ┰ <del>╏╶┦╸┪╸</del> ┧╼╁╾╂ <del>┍╶┨┍╺╏</del> ╤╾╂┈	2 5 0 0 4 2	2	
	3BFCL1	MS	Inos only- Dissolved
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Cliant's Special Instructions: See Diave	Elmone		
	sacribe Problems II Any:	······································	
#1 Relinguished By: Sig.) Oxlondil	Date 17 16 #2 Relinquished By: [Sig.)	Date: #3 Relinquished By: [Sig.]	Date: Sample sionage time
Company Name: Golder ASSOC	Time 71 Company Name:	Time: / / Company Name:	Time: {In days, see Note 3}
#1 Received By: (Sig.)	Date: #2 Received By Sign	053/14/2(W3 Received By: (Sig.)	Oate: DESTROY or RETURN
0	Time: Company North	Time /9 Company Name:	Time: (Circle choice: see Nove 4)

Rote (1): If "N" leb will haid samples to save it remainder of project-maximizing batch sizes and minimizing CC ratio; if "I leb will begin processing betches row. Note (2): If CLP trougantics disketts required, ID limited to maximum of els characters, Note (3): Samples stored 60 days after date report mailed at no extra charge. Note (4): All lab copies of data destroy of his per live years unless client requests and pays for return of copies; annual storage fee billed in James y of year six.

#### CHAIN OF CUSTODY RECORD

PROJ. 1 943-622		PROJECT	inamb an 15ted	<del></del>		NO.			F	CONT	AINER	TYPE	7-/	
SAMPLI	ers: Ta		salm		· · · · · · · · · · · · · · · · · · ·	CON-		*/		Z'NO.	13/ N	\ \&/		REMARKS
SAMPLE	DATE	TIME	MATRIX	SAIN	FLE LOCATION	TAINERS	3		4	) (	3 / 3	\\cdot\\cdot\}	se/	
	9/18/12	1705	GW	mw.	8 <i>D</i>	8	2		1		2	2		
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	विक्षि	0800	<b>1</b> 3	18-0	2	1	I						Aralyze only	one Trip blank
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RH INQUEST	ED BY: (Sig	лирите)	Date I	Time 156 18/5	RECEIVED BY: (Signature)	<u></u>	RELLY	QUISH	ED BY	: (Signa	(ture)	Ĺ	Date / Time	RECEIVED BY: (Signature)
RECINQUISH)	EID BY: (Sig		Date I	Time .	RECEIVED BY: (Signature)		Ι.	-		: (Slgna	wrc)		Date / Time-	- RECRIVED BY: (Signature)
RELINQUISH	BD BY: (Sig	nature)	Date /	Time	RECEIVED FOR LABORATO	ORY BY:	9/19	nlo I Tir 176	7/7		REMA	RKS:	See LoA fo	n instructions (A ove Elimone)
COC2.XL	.s				-0 -	4.	0							( Limbre)

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#### CHAIN-OF-CU ODY RECORD

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CORPORATION	Ship to:	Project Name: Canl	Stadt   Fleid Point-of-Contact:	Lori Hardel
3306 Chapel Hill/Nelson Highway Research Triangle Park, NC 27709	Compuchen	Sampler Name. Sm/m	Teleprone No (-)	95 273 - 1 (1 (2) Implete? Y or (10) (See Note 1)
1-800-833-5097	Carrier: Airbill No.: Falex 7550861512	Sampler Signature:	Project-spectric ((PS)) of	r Batch (B) QC:
BOX #1: 1-Burl sce Water 9, Trip Blank 119 2. Ground Weler 7007 3. Leanata 1200 (Waster 4, Franch) 700 (Christian) 4. Franch 700 (Christian) 8. Sept 18-diment (Sundge	Falex 755 (B) 5 (2) Box #2: A HCl	Box WS. 1 Figures.	Book #4: CELPORO: R. Reno S. SEN-ANI I TO R W. CWA 500-yeller S. Oble L. Levi Cyric Care	ogical Box ws:   Light
Sample ID (Organics: 9 cheracters max, tanopanics: 6 characters; Seb Note 2)	Matrix Preservative Preservative Filterce/Unfiltered Wethod Expect. Cono.  Propect. Cono.	Organica Analysis (M3 or Duf) (M3 or Duf) (M3 or Duf) (M3 or Duf) (M3 or Duf) (M4 or Duf) (M5 or Duf) (M5 or Duf) (M5 or Duf) (M5 or Duf) (M5 or Duf) (M5 or Duf) (M5 or Duf) (M5 or Duf) (M5 or Duf) (M5 or Duf) (M5 or Duf)	Metale Metcury Gyanides Gyanides Tob / Tox O&a / TPH Phenois Other	Remarks / Comments
mW-2R 918:	2BFCL6	2 ms	2   Ino.	only Dissolved
mw-212 :	2BVCL3	3 ms	3   1   7A	L Metals
mw-2R 1:	200063	3 MS	3 1 1 1 1 1	<u>-</u>
mw-2R 1:	2AUCL6	o MS 6		
1 An w :				
TB-02 918 0800	6 A V C L			
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Client's Special instructions: Sae Diase	Ellonose	<del> </del>	<del></del>	
	Describe Problems, If Any:			
#1 Reliaquished By: [Sig.)	Odfill of #2 Pelinquished By: [Sig.)	Dete:	#3 Relinquiated By: (Sig.)	Date: Sample storage time
Company Name: Golden Assoc	Time: 130 Company Name:	<del></del>	Company Name:	Time: (In days, see Note 3)
#1 Received By: [Sig.)		1/1/2	a Received By: (Sig.)	Date: DESTROY or RETURN data etter (ive years of eichlys)?
Сопралу Мале:	Time: Company Name: 0	TIMECTO	Company Name:	Time: [Circle choice; see Note 4)

Note (1): 14 "N" lab will hold samples to exvalt remainder of project-maximizing batch size and minimizing OC ratio; if "N" lab will begin processing batches now. Note (2): if CLP inorganics distants required, ID limited to maximum of six characters.

Note (3): Samples sixed 60 days after date report mailed at no extra charge. Hote (4): All lab copies of data distroyed after large any animals elected required and pays for return of cepies; annual storage fee bited in January of year six.

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#### CHAIN-OF-CL CODY RECORD

Nº 999/

CORPORATION Ship to:		Project Name: Conts-	Field Point-of-Co	ontacl: Lovi Aerdel							
3306 Chapel Hil/Nelson Highway Research Triangle Park, NC 27709	and	Sampler Name:	Telephone No.:	609 2731110							
	mile chem	SM/M2	Sampling for pro	Sampling for project complete? Y or-(N) (See Note 1)							
1-800-833-5097 Carrier:	Airbili No.: X 755 0361512	Sampler Signature:	Project-specific	Edi DI Bekt iai Ju							
BOX #1: 1. Busines Victor 6. July Blank	CHCI E, lice Only	Box #3: P.Filiped		R. Radiological Box #5: 11 - High T. TOUP M. Medium 1:							
& Lenchale 4. Wante	Nebbook N. Not Preserved	1	W: CWA 500 series								
5. Disc) Captioned / Sludge	A 100 S		L Low Conc. CLP								
Box #1 Box	#2 Box #3 Box #4 Box #5	Organics Analysis	s inorganics Other								
Sample ID (Organics: 9 characters; See Note 2)  See Note 2)  See Note 2)	Filered/Unfilered Method Expect Conc. No. of Bottles	Use for Lab QC (MS or DUP) VOA-GC / MS SV-GC / MS Pest / POB-GC Horb-GC VOA-GC	Metals Marcury Cyanides Rediologicals TOC/TOX OMG/TPH Plenods Othor	Remarks / Comments							
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mw-2R 91/8: 2 E	VCL3	ms 3		ms/msh							
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Client's Special Instructions: Sur Duance Ellernon Late: Beceived in Good Condition? Year N Describe Prob											
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Company Name: Golden ASSOC Time: M	Сопраку Напа:	Time:	Company Narae:	Time: {In days, see Note 3}							
#1 Received By: [Sig.] Defe:	#2 Received By: San Ba	2 0419/19/1	(\$13 Received By: (Sig.)	Dale: DESTROY or RETURN deta after live years of archivel?							

Hote (1): If "Y" lab will note samples to avail semainser of project-maximizing betch size and minimizing OC sello; if "Y" lab will begin processing betches now. Note (2): If CLP inorganics diskette required, ID, limited to maximum of six characters.

Hote (3): Samples stored 60 days after date report castled at no extra charge. Hote (4): All tab copies of data descroyed pater five years unless client requests and pays for return of copies; around storage fee billed in January of years six.



#### **CHAIN OF CUSTODY RECORD**

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ET TROUTSH	HD BY; (Sig	nature)	Date /	·	RECEIVED BY: (Signatur	र)	RELL	NQUISE	(IED BY	': (Signa	mitc)		Date / Time	RECEIVED BY: (Signature)
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#### CHAIN OF CUSTODY RECORD

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#### CHAIN-OF-CUS ... DY RECORD

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	COMPUCHEM ENVIRONMENTAL CORPORATION
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#### **CHAIN-OF-CUSTODY RECORD**

Nº --418

	CORPORATION								S	ip to:			Project Name: Carlstadt										Fie	Field Point-of-Contact: Loni Hendel							
3306 Chi									ļ		OM	ouch	m		Sampler	Nam	e:		·	- 7					Telephone No.: 609 273 · 1/10 Sampling for project complete? Y or (N) (See Note 1)						
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2 3 4	SOX #1: 1. Sudage Weler 8. Tup Blank 2. Geomina Weler 7. Oll 3. Listachble 8. Waste 4. Finnath 9. Other 8. Boll / Sediment / Bludga									c	. HC+ :.HNO3 :. Ka) 1504 .Ne <sub>2</sub> S <sub>2</sub> O	, N	. Toe Only . Other A . Not Prese	eoff.	Box #3:								Box	,	9. 5V V. CY	Y-048 YA 60			'cal	8	iox #5: HHigh M Medium LLow
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Hote (1): If 'N' lab will how samples to await remainder of project-maximizing batch size and minimizing CC railo; if 'Y' lab with boyin processing betches now. Hote (2): If C.P increance diskette required, ID limited to maximum of six characters.

Note (3): Samples stored 50 days after oxid-report mailed at no extre charge. Hote (4): All lab copies of date destroyed after the same unless claim requests and pays for return of copies; annual storage fee billed in January of year six.

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			_		_	_		Ţ,	<u></u>	T		Box #1	Box #2	Box #3	Box #4	Box #5		7	Orga	nice .	Analys	la	Inorgan	ics C	Mher							
ino	elqi Banka Bank Note	:9 e ≈:8	har.	acte: ursci	613; 613;	ex,			Dalo; Your: 19 16	Time		Metrix	Pieservative	Filtered/Unfiltered	Method	Ехресь Сопо.	No. of Bottles	Use for Lab QC (MS or DUP)	VOA-GC / MS	Pest / PCB-GC	VOA-GO		Metals Mercury Cyanides	Rediolonicals		T00/T0X 086/TPH	Phenols	Outer	Re	marks /	Comments	
n	<i>y</i>  -	7	E	1	T	T	T	9	1/18	14	30	2	A	U	C	L	2		a		$\prod$								Only	d1550	lved	Fe.
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Сопу	any ł	Zam	et;		ŝ	<b>/</b>	L	<u>.                                    </u>	A	556	C.	Time	1780	отралу Н	ANDE:		<u> </u>			Time		• •	ompany N							Time;	(in days, see Nois	1)
#1 B	celvi	ed B	y: (9	lig.}								Date		2 Received		pope	بيك				$\omega \omega$	~	3 Received		g)					Date:	DESTROY or RETURN data after two years of suchivel?	
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Note (1): 18 1/4 lab will hald samples to await remainder of project-maximizing betch size and minimizing OC to illo; if "Y lab will bugin processing batches now. Note (2): 18 CLF longanize diskaste required, ID limited to maximum of six characters. Hote (3): Samples sloved 60 days after date report mailed at no extra charge. Hote (4): All lab copies of data destroyed after try, years writen executes and pays for return of copies; armuel storage (se billed in January of year six.

SEP-20-1996 9:51

#### CHAIN OF CUSTODY RECORD

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BAMPLERS:  JOH SO SON MZ						CON-		/	/ & /	/ /	THE SOLVE	/ع <sup>ال</sup> /لحدة	/ /		remarks		
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COC2.XI	LS						<u>i</u>		<del></del>	<del></del>		4	F1 8N7	TIX CAP	4-19-2 P	·····	

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	COMPUCHEM ENVIRONMENTAL CORPORATION
3306 Chap Research 1	ei Hili/Neison Highway riangle Park, NC 27709

#### **CHAIN-OF-CUSTODY RECORD**

Nº 16363

CORD	ORAT	IO N	Ob.	<del></del>					Destant	None	.—					Te	-I-I E	م المحادد	1.00=1-01-			
3306 Chapel Hill/Nels	Joulo	Ship to:							Project Name: Canlstadt Sampler Name:  This many AP							Field Point-of-Contact: Con, Herles						
Research Triangle Par	rk. NC 2770	y )9		(	لهموص	oua			Sample	r Nam	e: ,	,	,			T	elept	on-e t	Vo.: 60	9273	1110	
, iooo a can a can gio a ca					- ,					7	72H/.	sm/.	וןבח	40		s	ampl	ing fo	r project com	plete? Y	O(N) (See Note 1)	
1-800-833-5097	_		Carr	dex	Air	ыіі No. 153 <sup>г</sup>	: 0345	33 33	Sample	r Sign	ature	flo.	ull	W	1	P	rajec	l-apec	ifl (PS) or B	atch (B) Q	o:	
BOX #1: 9. Burtope Water 9. Trip Blank 21 Green Water 7. Cli 5. Line lasts 8. Waste 4. Clinate 9. Other 9. Soil / Sodiesen/ Stodge									Box #3: F.FRerad U.Linfiltered Box #4:							5.S W.C	Y7-846 Y/A 6			cal .	Box #6; st. Hgh IV. Medlus L. Low	
			Box #1	Box #2	Box #3	Box #4	Box #5		1	1010	nics A	nalyeli	Inorg	garde	s Othe	ar			<del></del>			
Sample ID (Organics: 8 characters max, inorganics: 8 characters; Sea Nota 2.)	Date: Vetr. 19	1tme	Мація	Preservative	Filtered/Unfluered	Method	Expect. Conc.	No. of Bottles	Uso for 1 ab OC (MS or DUP)	VOA-GC / MS SV-GC / MS	Past / PCB-GC Herb-GC	V0A-GC	Motals Mercury	Oyunides	Radiologicals	TOC / TOX	Phenols	Olhar	Re	marka /	Comments	
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Client's Special Instructions: Lab: Repolved in Good Candit					a, ii Any:																	
#1 Perinquished By: [Big.]					72 Reingul	ished By:	(Slg.)				Date		#3 Pelin	iz:ulshe	ed By:  S	ig.				Date:	Samp e slonge time	
Company Name.	derAss	٥٥			Sompany N						Time		Сотранц	y Kam	4:					Time	requested?(In days, see Note 3)	
#1 Received By: (Sig.)	V = 4		Date:		P2 Flaceive		L Constant	J			Date	9/20	B) ficce	ived B	y·(Sig.)					Date:	DESTROY of RETURN	
Company Name:		·	"im e:		Company N	lama:	100				T:69						date after five years of sichlysi? (Circle choice; see Note 4)					

Hitte (1): If 'N' hab will hold samples to await remaindar of project-maximizing batch size and minimizing QC radio; if 'N' hab will begin processing balches now. More (2): If 'C.-P inorgan' os diskeller required, IQ limited to most-num of skich ereculted. Hote (3): Samples stored 60 days after date report smalled at no extra change Hote (4): At lab copies of data destroyed after the years unless client requests and pays for roturn of copies annual storage fee billed in January of years x

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27.	COMPUCHEM ENVIRONMENTAL CORPORATION

#### **CHAIN-OF-CUSTODY RECORD**

**№** 16364

CORRENTAL			·							
CORPORATION 3306 Chapei Hill/Nelson Highway	Ship to:	Project Name: Court	Field Point-of-Contact	Field Point-of-Contact: Land Howel						
Research Triangle Park, NC 27709	Consider	Project Name: Colstander Name:  Sampler Name:	Telephone No.: 6 Sampling for project of	Telephone No.: (05-9-273-/// Sampling for project complete? Y or (6) (See Note 1)						
1-800-833-5097	Garrier: Airbiil No.: Fel Ex 7850361523	Sample/Signature	Project-specific (PS)	or Batch (B) QC:						
BOX #1: 1-Bistone Water B. Trip Blank 2. Grownd Water 7. Oil 4. Lenchalz 6. Viscle 4. Pagests 6. Ochor 5. Boll / Seddment / Studgs	Box #2; A HCI E. Ice Only 8. NNO <sub>3</sub> Q. Cther Q. NaHSO <sub>4</sub> N. Not Preserv D. Ne <sub>2</sub> S <sub>2</sub> O <sub>3</sub>	Box #3: F.F.terod  U.Unffdered	Box #4: C.CLP 3/90 R. Redi S.6W-949 T.TCLF W.CWA 900-series O. Other L. Low Conc. CLP	M. · Wadism						
B	ox #1 Box #2 Box #3 Box #4 Box #5	Organica Analysi	s Inorganics Other							
Semple ID (Organics: 9 characters max, inorganics: 6 characters. See Note 2	Provensaive Filtered/Untillored Method Expect. Conc.	No. or Bortles Use for Lata QC (MS or DUP) VOA-GC / MS SV.GC / MS Post / PCB-C Horb-GC VOA-GC	Munks Mercury Cyanides Fediologicals 10c/TOX 0.co./TPH Phrenols Onner	Remarks / Comments						
MW-180 91513:15	2月1111	2 2								
MW-180 719 13:15		z 2								
Mu - 18 DD 7 17 13 15	100	1								
MW. 1800 2191515	V B U V	1	TAL	Metils						
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Citent's Special instructions:	<del></del>	<del></del>	<del> </del>							
Late Received in Good-Condition Y or	Describe Problems, If Any:									
#1 Relinquished By: (Sig.)	Oate: 77 #2 Relinquished By: (Sig.)	Data	#3 Relinquished By: [Sig.]	Date: Samp's alwage time requested?						
Company Name. (G: Ust A))	Time (640 Company Name.	Time)	Сопраду Мага:	Time: (th days, see Note 3)						
#1 Received By: (Sig.)	Date: #2 Received By:  Sig.)		#3 Received By: [Sig.]	Date: DESTROY or RETURN data giver live years of prohius??						
Олорапу Нате:	Time: Company Name:	Time II	Company Name	Time: (Circle choice: see Noto 4)						

Hote (1): If "A" lab will hold samples to swall remainder of project-maximizing batch size and minimizing QC ratio; " "" hab will begin processing betches now. Hote (2): If CuP inorganics diskette required, Q I miled to maximum of six characters.

Hote (2): Samples stored 60 days after date report matted at no extra charge.

Rote (4): At two copies of data destroyed after two years unless silient requests and pays for return of copies; annual storage fire bised in January of years in.

COMPUCHEM ENVIRONMENTAL CORPORATION
CORPORATION

3306 Chapel Hill/Nelson Highway

Ship to:

# CHAIN-OF-CUSTODY RECORD

Project Name:

Sampler Name:

Field Point-of-Contact:

<b>№</b> 163 <b>6</b> 2	#28
Heride /	7004
(N) (See Note 1)	01 · 30PM
Box #5; HHigh : N Mod-um L-Law	09-00-66
Comments	
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Hesearch Ina	ngie Par	K, NG 27	709		C	ין במט		<i>411</i>				J	H/S	'n	AP/	m	2		piln	g for	project com	pleto? Y	of(N) (See Note 1)
1-800-833-509	)7			Car	راور: في م	C 7	rbīli No.:	3615	23	Gample	r Sja		Sm	1	W			P,ro]	ect-s	pecif	fic(PS) or E	Batch (B) C	QC:
BOX #1: 1. Bürjiot 2. Gröne 3. Liderts 4. Firests 8. Soll / S	d Waler ele	6. Trip Blac 7. Oli 6, Waslo 9. Other luiggs	nk	Box	C. )	HCI INO <sub>3</sub> . (AHSO <sub>4</sub> In <sub>2</sub> 9 <sub>2</sub> 0 <sub>3</sub>		lice Oray Other V Not Prese		Box #3:		ered Fitered			(	Вох	1	C.C.P S.SW- W. CW/ C.Low	848 A 600-		R Pactolog T.TCLP O.Othes	icai	Box#5: HHigh M Mod∙um L- Law
Sample ID (Organics: 9 chairs feorganics: 6 chars See Note 2)	dējs m ax, actem;	Dute; Year; 1916	Time	Box #1	Preservativo og	illered/Unfilered of x	Method Method	Cypect Conc.	No. of Bottles	Use for Lab QC (MS or DUP)	П	Past / PCB-GC	ΤĹ	Ls	Metrils Mercury Oyanides	Padiologicals Q		O&G / TPH	Oh-r		Re	ema <del>r</del> ks /	Comments
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		1		2	E	U	_	4	12		i	2	! /				ii	l l					
			V	2	B	U	2	4	1		П		$\Gamma$	T	1			1	$\prod$	T	TAL	Met	ak
mw-18	DD		1315	2	B	F	2	4	1		11	1	11	T	1	;		<b> </b>	Π	Τ.	Inow	وادم	als Dissolved
MW-95			249	2	0	U	C	4	1		$\prod$	7	Ħ	Ī	1		П	T	П	-		//-	
mw- 18			1315	2	E	U	1	1	1		$\prod$		Ħ	T				ī					
MW-95			1249	2	A	U	_	1	2		2	$\Pi$	$\Pi$	T				11	П	1			
mw-8R		1	0945	2	A	U	1	L	2		b	$\prod$	$\prod$	Ť	Hi		Ţ	11	T				
mw-18		17	1315	2	A	V	2	1	1		1	11	$\prod$	T	!			††	$\prod$	1			· · · · · · · · · · · · · · · · · · ·
18-03		11	0870	6	A	V	C	1	ī		1	1	11	$\dagger$	+++			+				·	
Client's Special Ins	dructions:	See	Dias	: [1]	mon	۰		1						<u>-</u> -		لمثما							
Late: Received in Oc	ood Conditi	onn?Y or N				ns, if Any:																	
#1 Relinquished By:	(Sig.)	Mond	W	04	19190	/2 Helinge	ished By:	(Elg.)				Cat	»:	'نــ	×3 Relinguls	hed By:	(Sip.	1				Date:	Sample alorage time requested?
Company Nume.	Gold	ler Ass	W_	Tim	545	Company I	Name:		·			Tima	-/	_	Сомрану На							Tima:	(In days, see Note 2)
#1 Received By: (Si				Date	2:	#2 Pisceivi	d By: JBig		3h/			59	2011	4	13 Received	By:  Sig	5)					Dete:	CESTROY or RETURN
				i im	6:	Commeny	Name:	7				1-6	WŌ	Te	Zaračeny Na							Time:	Cala ate: Tvo ye are at archiva@

Hote (1): A "N" lab will hald samples to exect remainder of orcject-maximizing batch size and minimizing OC radio; if "Y" lab will begin processing batches now. Hote (2): If CLP inorganics diskette required. IQ limited to meximum of six characters. Note (9); Samples stered 60 days after date report mixiled at no extra charge. Hote (4): All lab copies of data destroyed after five years unless tilent requests and pays for return of copies; entired storage fee billed in January of years in.

	COMPUCHEM Environmental
	CORPORATION
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Nº 15021

ENV1RONMENTAL										
CORPORATION	Ship to:			Project Name:	Carl	stadt	Field Poin	rt-of-Contact:	Lori	Hendal
3306 Chapel Hill/Nelson Highway Research: Triangle Park, NC 27709		ompuche	771	Project Name: Sampler Name	sm/n	nZ,		No.: 609	273	
1-800-833-5097	Corrior:	Airbill No.: 7550361		Sampler Signs				eclii (PS) or B		
BOX #1: 1. Suitable Walps: 6. Top Blank 2. Spising Water 7. Off 2. Lifechals 0. Woods 4. Primate D. Ocher 5. Sail / Sediment / Pudge	Box #2: A B. C.	HCI E.	Ice Only Other Place Kot Pressaved	Box #3: F.F.er	e1 uzed		Box #4: C.OLP 2/50 S. SW-848 W.: CY/A 600-60 1. Low Conc. 1		cel	Box #5: H - High M:- Medium L - Low
Sample ID (Organica: 6 characters max. Inorganica: 6 characters; Bea Note 2	Proservative	Box #3 Box #4 Box #4	Expost. Cono. No. of Bottles	Use for tab GC (MS or DUP) VOA-GC / MS	Herb-GC VOV-GO	Mutais Mercury Cyanides	Radiologiculs TOC/TOX O&G/TPH Phenois Other	Re	rnacks / (	Comments
mw-170 9191021	2 6	VC	4 2	2	ليلأ					
1	2 6	UC	E 2	}-}-	[ <u>[</u> ]	$\prod_{i} \prod_{j}$				
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	2 B	FC	41					Tros	ع مالع	Dissoluch
	20	UC	41							
11411114111	2 A	UC	1 2	2						
TB-03 9/19 0860	6 A	VC	L 1	1				Analyze	م ماده	HE Trip black
<del>╱┩╼╏╼╏╼╏╌┝┈┝═╏</del> ╌ <del>╏┈</del> ┞┈╾┈┼┈	AA	UC	L 2	2					<del></del>	
	2 B	FC	41					Inon	ر پادره	Distolved
MW-18DD 91913F5	2 A	VC	L 1	1					<del></del>	
	مالك	٠								
Lab: Received in Good Condition? Y or N	escribe Proble	ms, if Any:								
#   Relinquished By:  Sig Cylum Will	· Qukl	#2 Relinquished By: (	\$q.)		Cate:	#3 Relinquiste:	d By:  Slg.		Date:	Sample storage time
Company Name. Coldu ASSOC.	Time: \S\S	Cost pany Name:	44		Time:	Company Name	): 		Time:	In days, see Note 3 }
#1 Received By: (Sig.)	Daba:	#2 Received By: (Sig	W-27		7/20/21	#3 Pecetved By				DESTROY or RETLAN  deite after five years of archival?
Company Name:	Time:	Соправу Ката:	19/		1. J. C. O	Сэтралу Ната	×:			Circle choice; see Note 4 }

Note (1): If "I' lab will hald samples to await remainder of project-maximizing batch size and minimizing QC ratio; H " lab will begin processing batches now. Note (2): If CuP inorganics diskette required, ID, timbed to maximum of six characters Note (3): Samples stored 60 days after date report mailed at no extra charge. Note (5): All lab copies of data destroyed after five years un'ess client requests and pays for return of copies; annual storage fee billed in January of year six.

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Note (1): If "N" lab will hard samples to sweet remainder of project-materializing beach size and minimizing OC ratio; if "" lab will begin processing balches now. Note (2): "CLI" increpants diskette required, "Q limited to maximum of six characters.

Note (5): Samples stores 60 days after date report mailed at no extra charge. Note (4): All lab copies of data distributed after five years unless client requests and pays for return of copies; annual storage (see billed in January of year six.

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	COMPUCHEM ENVIRONMENTAL CORPORATION
3306 Chap	el Hill/Nelson Highway

Nº 16366

CORPORATION	Ship to:	Project Name: Constadt	Field Point-of-Contact: Love Acidel
3306 Chapel Hill/Nelson Highway Research Triangle Park, NC 27709	Compochem	Sampler Name:  THE SM M / MZ	Telephone No.: 6092731110
		JAH SM/M/mz	Sampling for project complete? Y on (See Note 1)
1-800-833-5097	Carrier: Airbill No.: Feder 7550361523	Sampler Signatures/	Project-specific(PS) or Batch (B) QC:
BOX #3: 1. Strategi Weiger 6. Trip Stank 2. Strains Wester 7. On 3: Likerheite 6. Vizzigs 4. Filments 6. Ottor 3. Bolf / Sediment / Studge	Box #2; A HCI E. Ice Only O. Other ALL C. NeHSO <sub>4</sub> N. Nox Preserved D. Ne <sub>2</sub> S <sub>2</sub> O <sub>3</sub>	Box #3: FAltared Box #4: 0	C.CLP 3;EQ R. Raciological Box #5: H High S. SW-848 T. TCLP M Mexilium J. CNA 500-señas O. Olther L Low L. Low Cons. CLP
	ox #1 Box #2 Box #3 Box #4 Box #5	Organics Analysis Inorganics Other	
Sample ID (Organics: 9-characters max, Inorganics: 6-characters; See Note 21	Proservative Filtered/Unfiltered Method Expect Conc.	Use for Lab GC (MS or DUP) VOA-GC / MS SV-GC / MS SV-GC / MS SV-GC / MS SV-GC / WOA-GC VOA-GC / VOA-GC VOA-GC VOA-GC / VOA-GC VOA-GC / VOA-GC VOA-GC / VOA-GC VOA-GC / VOA-GC / VOA-GC VOA-GC / VOA-GC Remarks / Comments	
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NW-18100 919 13:15	28/12		PAL Broken in box P/P
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	ie Ellmone		
	escribe Problems, II Any:	Jale: #3 Relinquished By: (Sig.)	Date: Sample storage time
#1 Relirquished By: (Sig.)	Time Company Name:	Thra: , Company Name:	Time: [In days, see Note 3]
Company Name. Color ASSOC.	Date #2 Received By May 75	Day 30 /9 A #1 Peceived By: (Sig.)	Coto: DESTROY OF RETURN
Company Name:	Time: Company Name Company Oct	Tin 130 Company Yame:	data after five years of archivel? Time: [Gircle choice; see Note 4]

Company Name: Time: Time: Company Name: Time: Time: Company Name: Time:

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# CHAIN OF CUSTODY RECORD

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Sampl	ers:	Sm	Cantel 15rul/m	2/AP		CON-			\ \\.	(N)	/ /	33	wis of	REMARKS
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# CHAIN OF CUSTODY RECORD

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SAMPL	ers:	TCH A	/SM/MZ			COM-	4	./	v/.	, .V.		* / * * / * * / * * / * * / * * * /	Parties of	remarks .
SAMPLE	DATE	TIME	MATRIX	SAN	PLE LOCATION	TAINERS	Vox	\ \text{i}	07	· /	1/1/4	1/42	<u> </u>	
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		0927	GW	MW-	15 <u>b</u>	1. 5	2							
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### CHAIN OF CUSTODY RECORD

PROJ. 943-6	NO. 222	PROJECT	NAMB	, An) 5	tadt		NO. OF			F	7	7	TYPE	7./	•
SAMPL	ers:	P.H/Sm	n/mz/	AP			CON-	4			/ & /-				RMARKS
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	9/20/96	1020	لهان		MW	-105	. 2	2							
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ELINOVISH.	ED BY: (Sig	nature)		∟e/Time		RECEIVED BY: (Signature)		RELIN	ILSIUO	ED AY	: (Signa	ture)		Date / Time	RECEIVED BY: (Signature)
ELINQUISH	ED BY: (Sig	pature)	Da	te / Time		RECEIVED FOR LABORATO	DRY BY:	9/2	aley Tic	n <sup>6</sup> 430	7	REMA 40		<u> </u>	<u></u>

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# CHAIN OF CUSTODY RECORD

943-1	NO. 0222	PROJECT	rname Ca~\s+	adt		NO. OF			/-	7	AINER	7	7	<u>.                                      </u>
Sampl		nlmz	-			CON-			20/2	eb/	RA TO	/ /	/ /	remarks
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LINQUISE	ED BY: (Si	gnature)	Date /	Time	RECEIVED FOR LABORA	TORY BY:	9/2	ar/To	91	39	RELLA	RKS:	·	-

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### CHAIN OF CUSTODY RECORD

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# CHAIN OF CUSTODY RECORD

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# **CHAIN OF CUSTODY RECORD**

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### CHAIN OF CUSTODY RECORD

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# APPENDIX H

Validation Narrative

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#### 1.0 INTRODUCTION

Analytical data collected between September 16 through September 24, 1996 at the 216 Paterson Plank Road NPL Site in Carlstadt, New Jersey has been validated as part of the Off-Property Investigation (Investigation). The samples were collected as specified by the Final Work Plan Amendment, December, 1995. The sample points chosen for analysis and the parameters which were analyzed are described in the Sampling, Analysis and Monitoring Plan (SAMP) and the Quality Assurance Project Plan (QAPjP). Samples from the Quarterly Operation and Maintenance (O&M) Monitoring Program and the Investigation were collected concurrently. For the purpose of this report, only the samples collected in support of the Investigation are discussed. The analytical results and results of the data review and validation for the Quarterly O&M monitoring wells was presented in the Quarterly O&M Report submitted to the USEPA in December 1996.

The samples were analyzed for the Inorganic Target Analyte List (TAL) plus cyanide in accordance with the U.S. Environmental Protection Agency (USEPA) Contract Laboratory Program Statement of Work for Inorganics Analysis, Multi-Media, Multi-Concentration (CLP SOW ILM03.0); and the Organic Target Compound List (TCL) in accordance with the Contract Laboratory Program Statement of Work for Organics Analysis, Multi-Media, Multi-Concentration (CLP SOW OLM03.1) for Volatiles Organic Compounds (VOCs), Semi-Volatile Organic Compounds (SVOCs) and Pesticides/PCBs. All of the groundwater monitoring well samples for metals analysis were collected as unfiltered (total). In addition to the TCL and TAL analyses plus cyanide, the samples collected as part of the Investigation were analyzed for Sulfide, Total Organic Carbon (TOC), Total Kjeldahl Nitrogen (TKN), Nitrate/Nitrite, total-Phosphorous, Alkalinity, Sulfate, Chloride and Methane, Ethane and Ethene, hereafter referenced as Inorganic List Parameters. Also, there were a select group of wells that were sampled for filtered (dissolved) Iron. The TCL/TAL analyses were performed by CompuChem Environmental (CompuChem) of Research Triangle Park, North Carolina. The Inorganic List Parameters analyses were performed by Accutest of Dayton, New Jersey.

Samples were collected from 10 primary locations. In addition, a sample of the on-Site potable water supply (PW-01) was taken and analyzed for TCL/TAL plus cyanide. Two sampling locations were sampled in duplicate for Field Duplicate analysis. The Sample Identification Points, sampling dates and the corresponding Sample Delivery Groups (SDGs) are summarized in Table H1.

Data validation of inorganic data collected using the CLP SOW ILM03.0 was performed in accordance with the <u>USEPA Region II Standard Operating Procedure (SOP) No. HW-2, Revision 11, Evaluation of Metals Data for the Contract Laboratory Program (dated January, 1992). Data validation for the organics was performed in accordance with the <u>USEPA Region II SOP No. HW-6, Revision 9, CLP Organics Data Review and Preliminary Review, dated January 1994. These documents are referred to as "functional guidelines" hereafter. Non-TCL/TAL analytical data were validated using the method-specific criteria as well as the criteria specified in the QAPjP dated September 1995.</u></u>

Data qualifiers are defined in Table H2. Where quality control criteria were met, positive results were not qualified and non-detected results were qualified with a "U" flag signifying that the result is below the quantitation limit (organics) or detection limit (inorganics). Where more than one qualifier for a sample result was warranted, the most predominant or general qualifier was applied to the results. For example, a positive result for a volatile organic compound may need to be qualified as undetected (U) due to its presence in the associated blanks; however, the initial or continuing calibration criteria for that compound may not have been met and would warrant qualification as an estimated result (J) or quantitation limit (UJ). In this particular case, the compound would be qualified as having an estimated quantitation limit (UJ). The (R) qualifier, which signifies that the result has been rejected, takes priority over all other qualifiers.

In some cases, there are multiple degrees to which the quality control criteria may not be met. For example, a matrix spike recovery for an inorganic analyte may be slightly greater than the upper limit of the Contract Required Recovery range; the corresponding positive results may be qualified as estimated (J). However, if the matrix spike recovery is greater than 150%, the positive results would be qualified as unusable (R). It should be noted that the discussions contained within Sections 2.0 through 5.0 explain where quality control was deficient. As specified in the functional guidelines, if the non-adherence to quality control criteria are slight, qualification of data may not be warranted. However, if the non-adherence is significant, qualification and possible rejection of the data may be necessary. The narrative discussion specifies where rejection of the data is necessary.

In general, the discussions which follow in Sections 2.0 through 5.0 describe only instances where the quality control criteria specified in the documents named above were not met. Tables H3 through H7 of this document summarize specific samples for which qualification occurred. This

report is intended to address the samples collected in support of the Investigation, except where an overlap has occurred (i.e., QC samples and dissolved Iron).

Following data validation and qualification, the analytical data and qualifiers for each sample point were summarized. Qualified results for the Investigation monitoring wells are provided in Appendix J of this report in a tabular format.

#### 2.0 TARGET COMPOUND LIST VOLATILE ORGANIC PARAMETERS

Samples were collected from 10 groundwater monitoring wells. Additionally, two wells were sampled in duplicate and three trip blanks and rinsate blanks were collected for VOCs. The samples were separated into two SDGs which contain samples and field duplicates and one SDG which contained one rinsate blank, all of which were analyzed for VOCs using the CLP SOW dated 3/90. The two SDGs which contain the samples (i.e., 1 and 48) were validated in accordance with the functional guidelines.

### **Data Quality Objectives**

Precision: Goals for laboratory and field precision were generally met, except where noted below.

Accuracy: Goals for accuracy were generally met, except where noted below.

Sample Result Verification: All sample results were supported in the raw data.

<u>Detection Limits</u>: The detection limit goals were achieved for all analyses, except where dilutions were required due to matrix problems.

<u>Completeness</u>: The data packages were complete for all requested analyses. Twelve (12) samples were validated in this data set. A total of 429 results for these samples were reported in which 429 were deemed valid. This results in a completeness of 100% for these samples which meets the Work Plan objective of 85%.

#### **Major Deficiencies**

There were no major deficiencies identified with VOCs.

#### **Minor Deficiencies**

Identified below are the minor deficiencies which required qualification of the data. Refer to Table H3 for the specific samples affected by each deficiency.

#### Volatile SDGs (1 and 48)

Laboratory preparation blanks, rinsate blanks and trip blanks are evaluated for target compound contamination. Methylene chloride, Acetone and Tetrachloroethene were found as contaminants in

various blanks for these SDGs. Samples associated with these blanks required qualification. For Methylene chloride and Acetone, an action limit of 10 times the concentration found in the blank was calculated. For Tetrachloroethene an action limit of 5 times the concentration found in the blank was calculated. For samples where any of these compounds were detected as a positive result between the Contract Required Quantitation Limit (CRQL) and the action limit, the result was flagged as undetected (U). For samples where any of these compounds were detected below the CRQL, the result was changed to the CRQL and qualified as undetected (U). Samples with positive results above the action limit did not require qualification.

The functional guidelines require the percent differences for the response factors (RRF) between the initial and continuing daily calibration be less than  $\pm$  25%. This criteria was not achieved for the compounds in the following continuing daily calibrations:

Sept 29, 1996	Chloromethane, Bromomethane, and Chloroethane;										
Sept 30, 1996	Vinyl chloride; an	d									
Sept. 24, 1996	Chloromethane, Chloroethane.	Bromomethane,	Vinyl	chloride,	and						

The samples associated with these calibrations required qualification as estimated values (J) for positive results and estimated quantitation limits (UJ) for non-detected results.

The functional guidelines require the response factors remain stable over the concentration range of the initial calibration (i.e. less than  $\pm$  30% RSD). This criterion was not achieved for the initial calibration analyzed on September 20, 1996 for Acetone. The samples associated with this initial calibration required qualification as estimated values (J) for positive results and estimated quantitation limits (UJ) for non-detected results.

#### 3.0 TARGET COMPOUND LIST SEMI-VOLATILE ORGANIC PARAMETERS

Samples were collected from 10 groundwater monitoring wells. Additionally, two wells were sampled in duplicate and three rinsate blanks were collected for SVOCs. The samples were grouped into two SDGs (SDG 1 and 48) by the laboratory and analyzed for SVOCs using the SOW dated 3/90. The SDG was validated in accordance with the functional guidelines.

### **Data Quality Objectives**

<u>Precision:</u> Goals for laboratory and field precision were generally met, except where noted below.

Accuracy: Goals for accuracy were generally met, except where noted below.

Sample Result Verification: All sample results were supported in the raw data.

<u>Detection Limits:</u> The detection limit goals were achieved for all analyses.

<u>Completeness:</u> The data packages were complete for all requested analyses. Twelve (12) samples were validated in this data set. A total of 832 results for these samples were reported in which 832 were deemed valid. This results in a completeness of 100% for these samples which meets the Work Plan objective of 85%.

#### **Major Deficiencies**

There were no major deficiencies identified for the SVOC analyses.

#### **Minor Deficiencies**

Identified below are the minor deficiencies which required qualification of the data. Refer to Table H4 for the specific samples affected by each deficiency.

#### **SDG 48**

The functional guidelines require the percent differences for the response factors between the initial and continuing daily calibration be less than  $\pm$  25%. This criteria was not achieved for the below listed compounds in the following continuing daily calibrations:

Oct 11, 1996 2,4-Dinitrophenol, 4-Nitrophenol, 4-Nitroaniline, Di-n-butylphthalate, Fluoranthene and Pyrene;

Oct. 11, 1996 4-Nitrophenol, Fluoranthene, 3,3'-Dichlorobenzidine, Di-n-octylphthalate.

The samples associated with these calibrations required qualification as estimated values (J) for positive results and estimated quantitation limits (UJ) for non-detected results.

During the data validation process, the qualitative identification of compounds are evaluated. The evaluations are based on mass spectra, retention time, peak shape and intensity. The laboratory is instructed by the SOW to report a compound as present even if all spectral criteria are not met. For the compound Pyrene in sample MW-14R, the mass spectra indicates that there is presumptive evidence of the presence of the compound, however, all criteria are not met. Since the compound is only presumed to be present in the sample, the result for this compound in the specified sample was qualified with the "N" flag.

#### 4.0 TARGET COMPOUND LIST PESTICIDE/PCBS

Samples were collected from 10 groundwater monitoring wells. Additionally, two wells were sampled in duplicate and three rinsate blanks for Pesticides and Polychlorinated Biphenyls (PCBs). The samples were grouped into two SDGs by the laboratory and analyzed for Pesticides and PCBs using the SOW dated 3/90. Each SDG was validated in accordance with the functional guidelines and guidance from the USEPA Region II Quality Assurance Chemist.

### **Data Quality Objectives**

<u>Precision:</u> Goals for laboratory and field precision were generally met, except where noted below.

Accuracy: Goals for accuracy were generally met, except where noted below.

<u>Sample Result Verification:</u> All sample results were supported in the raw data. Positive presence of a TCL pesticide/PCB must be confirmed by analysis on a dissimilar chromatographic column. Quantitation is performed for each column and the lower value is reported by the laboratory. The percent difference between the two results is calculated and reported by the laboratory.

<u>Detection Limits:</u> The detection limit goals were achieved for all analyses.

<u>Completeness</u>: The data packages were complete for all requested analyses. Twelve (12) samples were validated in this data set. A total of 364 results for these samples were reported in which 364 were deemed valid. This results in a completeness of 100% for these samples which meets the Work Plan objective of 85%.

#### **Major Deficiencies**

There were no major deficiencies which required rejection of the data.

### **Minor Deficiencies**

Identified below are the minor deficiencies which required qualification of the data. Refer Table H5 for the specific samples affected by each deficiency.

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### **SDG 48**

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The percent difference between the results reported from each GC column were greater than 25% but less than 70% for the compounds 4,4'-DDE and Endosulfan II in sample MW-15D. In accordance with the functional guidelines, compounds with percent differences greater than 25% but less than 70% were qualified as estimated values (J). Compounds with percent differences less than 25% did not require qualification.

Laboratory preparation blanks and rinsate blanks are evaluated for target compound contamination. Various pesticide compounds were found as contaminants in blanks in this SDG. Samples associated with these blanks required qualification. For all of these compounds, an action limit of 5 times the concentration found in the blank was calculated. Sample MW-15D required qualification as undetected result (U) for the compound beta-BHC.

#### 5.0 METALS PARAMETERS

Unfiltered samples were collected from 10 monitoring wells and filtered samples (iron) were collected from 10 monitoring wells. Additionally, two wells were sampled in duplicate and three field rinsate blanks were collected. The unfiltered samples were analyzed for TAL metals and the filtered samples were analyzed for Iron. The sample results were separated into four SDGs (two for TAL and two for Iron) by the laboratory and analyzed using the SOW ILM03.0. Each SDG was validated in accordance with the functional guidelines. The laboratory used an axial "trace" ICP instrument for the analysis of all metals with the exception of mercury. Mercury was analyzed by a cold vapor analyzer. The use of axial "trace" ICP instrument yields lower instrument detection limits for most of the analytes previously analyzed using the conventional ICP instrumentation. Additionally, it allows for the analysis of Arsenic, Selenium, Thallium and Lead by ICP rather that Graphite Furnace Atomic Absorption (GFAA).

#### **Data Quality Objectives**

Precision: Goals for laboratory and field precision were generally met, except where noted below.

Accuracy: Goals for accuracy were generally met, except where noted below.

Sample Result Verification: All sample results were supported in the raw data.

Detection Limits: The detection limit goals were achieved for all analyses.

<u>Completeness</u>: The data packages were complete for all requested analyses. Twelve (12) unfiltered samples and 26 filtered samples were validated in this data set. A total of 312 results for unfiltered samples were reported in which 305 were deemed valid. A total of 26 results for filtered samples were reported in which 26 were deemed valid. This results in a completeness of 98% for unfiltered samples and 100% for filtered samples which meet the Work Plan objective of 85% for each.

#### **Major Deficiencies**

Identified below are the major deficiencies which required rejection of the data. Refer to the tables in Attachment H6 for the specific samples affected by each deficiency.

### SDG 76M Unfiltered Metals

Laboratory preparation blanks and rinsate blanks are evaluated for target analyte contamination. Zinc was found as a contaminant in two of the rinsate blanks. Samples associated with these blanks required qualification. For Zinc, an action limit of 5 times the concentration found in the blank was calculated. For samples where Zinc was detected as a positive result between the IDL and the action limit, the result was flagged as rejected (R). Samples with a positive result above the action limit did not require qualification.

#### **Minor Deficiencies**

Identified below are the minor deficiencies which required qualification of the data. Refer to the tables in Attachment H6 for the specific samples affected by each deficiency.

#### SDG 3 - Unfiltered metals

The matrix spike recovery for Silver was lower than the criteria (75% - 125%) specified by the functional guidelines but greater than 30%. For the unfiltered portions of the affected samples, positive results were qualified as estimated values (J), and non-detects were qualified as estimated detection limit (UJ).

The functional guidelines require the absolute difference between the primary and field duplicate samples to be less than CRDL where the results are less than 5 times the CRDL. This criteria was not met for zinc in the associated field duplicate analysis. The positive results for this analyte for all samples in this SDG were qualified as estimated values (J).

#### **SDG 76M**

The recoveries of the CRDL standards for selenium were less than the lower control limit of less than 80% but greater than 50%. The positive results for this analyte for all samples in this SDG were qualified as estimated values (J), and non-detects were qualified as estimated detection limit (UJ).

#### SDG 3 and 76M

The functional guidelines require that a serial dilution be performed on any ICP elements which have concentrations equal to or greater than 10 times the IDL. Serial dilution analysis of the QC sample for these SDGs yielded a percent difference between the undiluted and diluted result for Potassium was greater than 10% but less than 100%. In accordance with the guidelines, positive

results greater than 10 times the IDL in the associated unfiltered samples were qualified as estimated values (J), and non-detects were qualified as estimated detection limit (UJ).

#### 6.0 INORGANIC LIST PARAMETERS

Samples were collected from 10 groundwater monitoring wells at and adjacent to the Site. Additionally, two wells were sampled in duplicate and three rinsate blanks for the analysis of the inorganic list parameters. The sample results were presented in multiple reports by the laboratory. Each report was validated in accordance with method-specific criteria and the criteria specified in the QAPjP.

#### **Data Quality Objectives**

Precision: Goals for laboratory and field precision were generally met, except where noted below.

Accuracy: Goals for accuracy were generally met, except where noted below.

Sample Result Verification: All sample results were supported in the raw data.

<u>Detection Limits:</u> The detection limit goals were achieved for all analyses

<u>Completeness</u>: The data packages were complete for all requested analyses. Eleven (11) samples were validated in this data set. A total of 88 results for these samples were could have been reported in which 88 were deemed valid. The completeness for all analytes is 100% which meets the Work Plan objective of 85% for each parameter.

#### **Major Deficiencies**

There were no major deficiencies reported for the Inorganic List Parameters.

#### **Minor Deficiencies**

The matrix spike recovery for Nitrate-Nitrite was lower than the criteria (75% - 125%) specified by the QAPjP but greater than 30%. For the affected samples, positive results were qualified as estimated values (J) and non-detects were qualified as estimated detection limit (UJ).

Laboratory preparation blanks and rinsate blanks are evaluated for target analyte contamination. TOC was found as a contaminant in one of the rinsate blanks. Samples associated with this blank required qualification. For TOC, an action limit of 5 times the concentration found in the blank was calculated. For samples where TOC was detected as a positive result between the MDL and the

action limit, the result was flagged as Estimated value (J). Samples with a positive result above the action limit did not require qualification.

#### 7.0 **SUMMARY**

Validation of the data collected for the Off-Property Investigation from the 216 Paterson Plank Road NPL Site was performed in accordance with USEPA Region II data validation guidelines, as applicable, and the criteria specified by the specific methods and the QAPjP.

Overall, the data required qualification due to some quality control criteria which were not achieved, but the majority of the data may be deemed usable in terms of objectives of the investigation. Although a positive result was qualified as estimated, the analyte should be considered present. Similarly, a non-detected result which was qualified as an estimated quantitation/detection limit should be considered not present for the purposes of this study, although the limit itself may not be precise. Rejected (unusable) data that are assigned the "R" qualifier should not be used. Rejected data have been included in the summary tables only for the purpose of completeness.

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TABLE H1 SAMPLE POINT IDENTIFICATIONS

				SDG NUMBERS	\$	)
SAMPLE POINT I. D.	DATE SAMPLED	ORGANICS	METALS, UNFILTERED	DISSOLVED IRON	INORGANICS LIST	CYANIDE
GROUNDWATER SAM	IPLES					
MW-8R	9/19/96	1	3	5	E14746	3
MW-10D	9/20/96	1	3	5	E14746	3
MW10R	9/20/96	1	3	5	E14746	3
MW-11R	9/24/96	48	76M	81	E14821	76
MW-15D	9/24/96	48	76M	81	E14821	76
MW-16D	9/23/96	48	76M	81	E14820	76
MW-17D	9/19/96	1	3	5	E14746	3
MW-18D	9/19/96	1	3	5	E14746	3
MW-14D	9/23/96	48	76M	5	E14820	76
MW-14R	9/23/96	48	76M	5	E14820	76
PW-01	9/23/96	48	76M	NA	NA	76

QUALITY CONTROL S	AMPLES					
TRIP BLANKS						
TB-03	9/19/96	1	NA	NA	NA	NA
TB-05	9/23/96	48	NA	NA	NA	NA
TB-06	9/24/96	48	NA	NA	NA	NA
RINSATE BLANKS						
RBGW-03	9/19/96	1	3	5	E14746	3
RBGW-05	9/23/96	48	76M	81	E14820	76
RBGW-06	9/24/96	48	76M	81	E14821	76
FIELD DUPLICATES						
MW-18DD	9/19/96	1	3	5	E14746	3
MW-14RD	9/23/96	48	76M	5	E14820	76
MATRIX SPIKE/MATRI	X SPIKE DUPLICATE	S				
MW-11R	9/24/96	48	NA	81	E14821	NA
MW-14R	9/23/96	NA	76M	NA	E14820	76

NOTES:

NA = Not Sampled

## TABLE H2 Data Qualifiers

Value - The data is acceptable; identification is confirmed.

- U The analyte was tested for but was not detected. The associated numerical value is either the sample quantitation limit (organics) or the sample detection limit (inorganics).
- B The analyte was detected at a concentration which is between the Instrument Detection Limit (IDL) and the Contract Required Detection Limit (CRDL). The data is acceptable.
- R Reject data due to quality control criteria. The data are unusable (analyte may or may not be present in the sample).
- N Tentative identification; consider analyte present.
- J The analyte is present. The associated numerical value is an estimated quantity and may not be accurate or precise.
- UJ The analyte was tested for but not detected. The sample quantitation limit or the sample detection limit is estimated and may be inaccurate or imprecise.

TABH-2.doc Golder Associates

Page 1 of 1

DATE: November 18, 1996

PROJECT NAME: 216 Paterson Plank Road NPL Site

**ANALYSIS: TCL Volatiles** 

**SAMPLE DELIVERY GROUP NUMBER: 1** 

REVIEWER: Jeffrey R. Hendel

DEFICIENCY	COMPOUND(S)	QUALIFIER	SAMPLES	SAMPLES AFFECTED				
Blank contamination	Acetone	U	MW-	10D				
RRF for initial calibration exceeds 30%.	Acetone	J for positive results UJ for non-	All					
D/ difference between the inited	Chloromathana Dramamathana	detected results	MW/ OD	- LIM 40D				
% difference between the inital and continuing RRFs exceeds 25%	Chloromethane, Bromomethane, Vinyl Chloride, Chloroethane	J for positive results	MW-8R, MW-18DD,	MW-18D, MW-17D,				
2.1.2 35.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1	y. Sinsings, officious and	UJ for non- detected results	MW-10D,	MW-10R				

**SAMPLE DELIVERY GROUP NUMBER: 48** 

REVIEWER: Jeffrey R. Hendel

DEFICIENCY	COMPOUND(S)	QUALIFIER	SAMPLES AFFECTED				
Blank contamination	Acetone	U (after changing result to CRQL)	MW-11R,	MW-15D			
		U	PW-01, MW-14RD,	MW-14D, MW-16D,			
	Methylene Chroride	U (after changing result to CRQL)	MW-14RD, MW-16D, MW-15D,	MW-11R, PW-01, MW-14R,			
	Tetrachloroethene	U (after changing result to CRQL)	MW-15D				
RRF for initial calibration exceeds 30%.	Acetone	J for positive results UJ for non- detected results	A	I			

Voa1 Golder Associates 1 of 2

PROJECT NO.: 943-6222

## **TABLE H3 (continued)**

## SAMPLE DELIVERY GROUP NUMBER: 48

REVIEWER: Jeffrey R. Hendel

DEFICIENCY	COMPOUND(S)	QUALIFIER	SAMPLES AFFECTED				
% difference between the inital and continuing RRFs exceeds 25%	Chloromethane, Vinyl Chloride	J for positive results UJ for non- detected results	MW-	11R			
	Chloromethane, Bromomethane, Chloroethane	J for positive results UJ for non-detected results	MW-14RD, MW-14D,	MW-16D, MW-14R			
	Vinyl Chloride	J for positive results UJ for non- detected results	MW-	15D			

Voa1 Golder Associates 2 of 2

DATE: November 18, 1996

PROJECT NAME: 216 Paterson Plank Road NPL Site

ANALYSIS: TCL Semi-Volatiles

**SAMPLE DELIVERY GROUP NUMBER: 48** 

REVIEWER: Jeffrey R. Hendel

DEFICIENCY	COMPOUND(S)	QUALIFIER	SAMPLES AFFECTED
Presumptive evidence to the presence of the compound	Pyrene	N	MW-14R
% difference between the initial and continuing RRFs exceeds 25%	4-Nitrophenol, Fluoranthene, 3,3'-Dichlorobenzidine, Di-n-Octylphthalate	J for positive results UJ for non- detected results	PW-01
	2,4-Dinitrophenol, 4-Nitrophenol, 4-Nitroaniline, Pyrene, Di-n-Butylphthalate, Fluoranthene	J for positive results UJ for non-detected results	MW-11R

Svoa1. Golder Associates 1 of 1

PROJECT NO.: 943-6222

DATE: November 18, 1996

PROJECT NO.: 943-6222 PROJECT NAME: 216 Paterson Plank Road NPL Site

ANALYSIS: TCL Pesticide/PCBs

**SAMPLE DELIVERY GROUP NUMBER: 48** 

REVIEWER: Jeffrey R. Hendel

DEFICIENCY	COMPOUND(S)	QUALIFIER	SAMPLES AFFECTED
Blank contamination	beta-BHC	U (after changing result to CRQL)	MW-15D
%D between concentrations reported on each GC column greater than 25% but less than 70%	4,4'-DDE, Endosulfan II	J	MW-15D

DATE: November 18, 1996

PROJECT NAME: 216 Paterson Plank Road NPL Site

ANALYSIS: TAL (unfiltered) Metals

**SAMPLE DELIVERY GROUP NUMBER: 3** 

**REVIEWER: Jeffrey R. Hendel** 

DEFICIENCY	ANALYTE(S)	QUALIFIER	SAMPLES AFFECTED
Matrix spike recovery less than 75%	Silver	J for positive results	ALL
but greater than 30%		UJ for non-detected	
		results	
Absolute difference between primary and	Zinc	J for positive results	ALL
field duplicates greater than CRDL when			
results of either is less than 5 times the CRDL			
Percent difference greater than 10% for	Potassium	J for positive results	ALL
Serial Dilution		>10 times the IDL	
		UJ for non-detected	
		results	

**SAMPLE DELIVERY GROUP NUMBER: 76M** 

REVIEWER: Jeffrey R. Hendel

DEFICIENCY	ANALYTE(S)	QUALIFIER	SAMPLES AFFECTED
Recovery of CRDL standard less than	Selenium	J for positive results	ALL
80% but greater than 50 %		UJ for non-detected	
		results	
Percent difference greater than 10% for	Potassium	J for positive results	ALL
erial Dilution		>10 times the IDL	
		UJ for non-detected	
		results	
Blank Contamination	Zinc	R when result	ALL
		less than action	
	ŀ	level	

PROJECT NO.: 943-6222

DATE: November 18, 1996

PROJECT NAME: 216 Paterson Plank Road NPL Site

**ANALYSIS: Inorganic List Parameters** 

SAMPLE DELIVERY GROUP NUMBER: N/A

REVIEWER: Jeffrey R. Hendel

DEFICIENCY	ANALYTE(S)	QUALIFIER	SAMPLES	AFFECTED
Matrix spike recovery less than 75%	Nitrate-Nitrite	J for positive results	MW-11R,	MW-15D,
but greater than 30%		UJ for non-detected	MW-14R,	MW-14D,
		results	MW-16D,	MW-14RD,
			MW-11R,	MW-15D
Blank Contamination	TOC	J for positive results	MW-16D,	MW-15D,
	•		MW-11R,	MW-14D,
			MW-14R,	MW-14RD

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PROJECT NO.: 943-6222

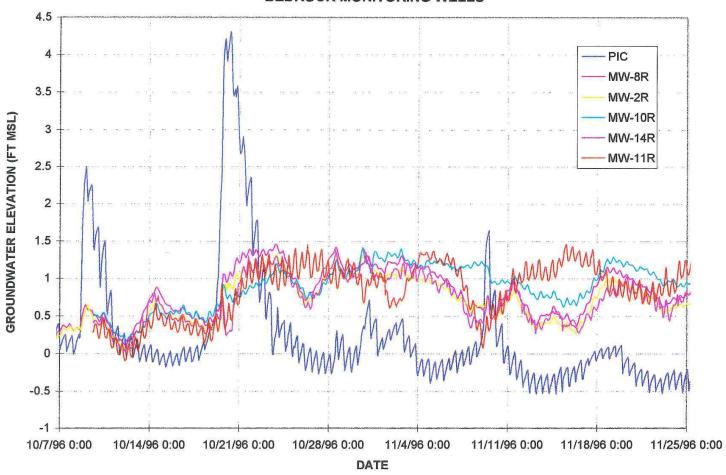
## APPENDIX I

Water Level Monitoring

R2-0000612

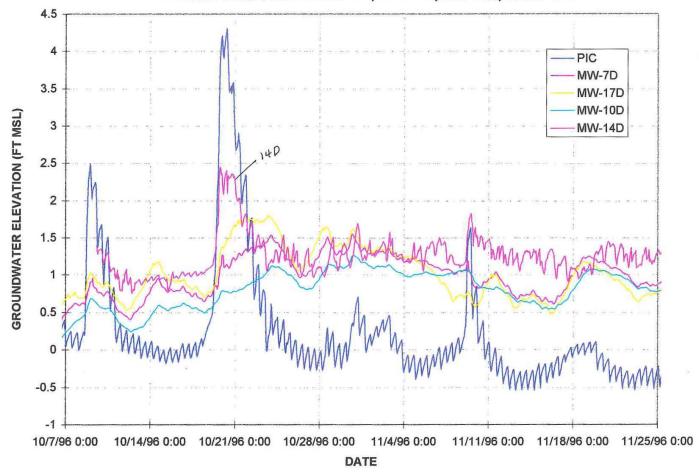
Till and Bedrock Monitoring Well Charts

## 216 PATERSON PLANK ROAD SITE GROUNDWATER ELEVATION vs TIME BEDROCK MONITORING WELLS



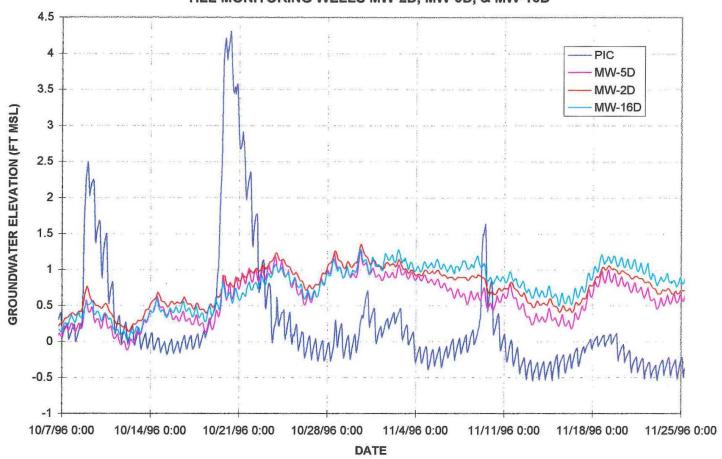
z:/6222/rireport/trolldat/Gwchart2/bedrock

## 216 PATERSON PLANK ROAD SITE GROUNDWATER ELEVATION vs TIME TILL MONITORING WELLS MW-7D, MW-10D, MW-14D, & MW-17D



z:/6222/rireport/trolldat/Gwchart2/till2

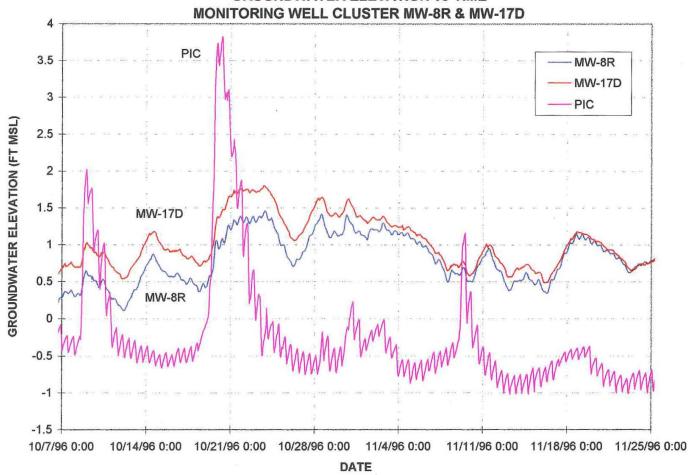
## 216 PATERSON PLANK ROAD SITE GROUNDWATER ELEVATION vs TIME TILL MONITORING WELLS MW-2D, MW-5D, & MW-16D



z:/6222/rireport/trolldat/Gwchart2/till1

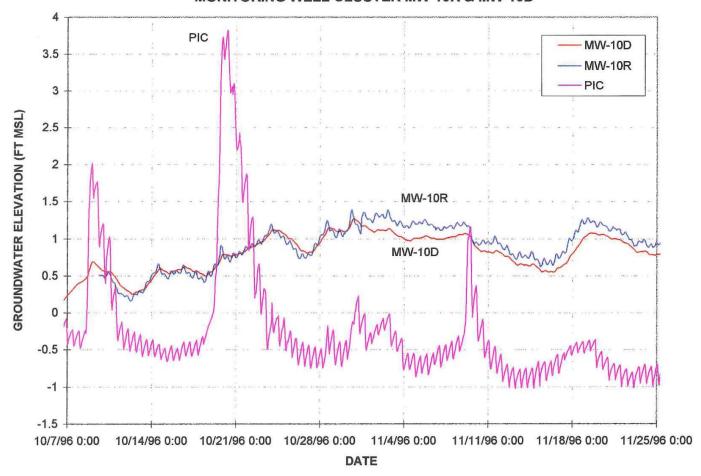


# 216 PATERSON PLANK ROAD SITE GROUNDWATER ELEVATION VS TIME



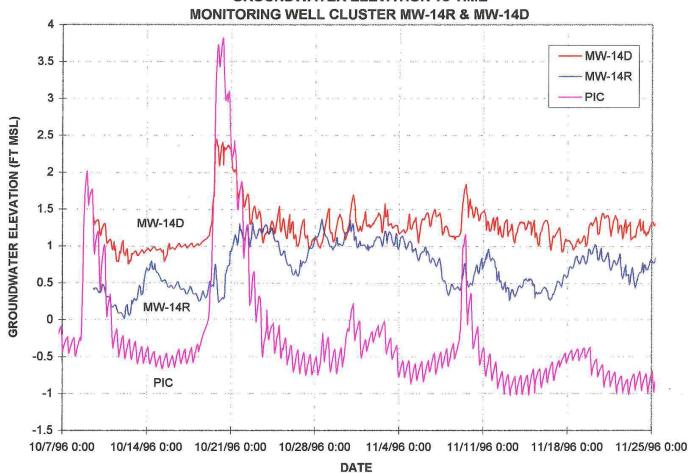
z:/6222/rireport/trolldat/Gwchart2

## 216 PATERSON PLANK ROAD SITE GROUNDWATER ELEVATION vs TIME MONITORING WELL CLUSTER MW-10R & MW-10D



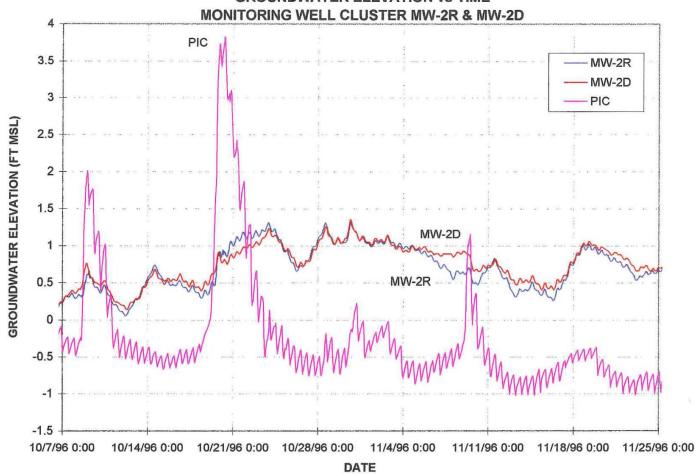
z:/6222/rireport/trolldat/Gwchart2

## 216 PATERSON PLANK ROAD SITE GROUNDWATER ELEVATION vs TIME



z:/6222/rireport/trolldat/Gwchart2

## 216 PATERSON PLANK ROAD SITE GROUNDWATER ELEVATION vs TIME



z:/6222/rireport/trolldat/Gwchart2

## APPENDIX J

Groundwater Chemistry Data

#### SUMMARY OF CLP OR \_\_\_\_,CS ANALYSES

216 Paterson Plank Road Site Sample Results Volatile Organics

Matrix: Groundwater

		S	ample Poin	<u> </u>	s	ample Poin	t	s	ample Poi	nt	s	ample Poi	nt	s	ample Poir	nt .
			MW-08R		1	MW-10D			MW-10R			MW-11R			MW-14D	
		Date S	ampled:9/1	9/96	Date S	ampled: 9/2	20/96	Date S	ampled: 9/	20/96	Date S	ampled: 9	24/96	Date S	ampled: 9/2	23/96
		Dilution	Factor: 1	.0	Dilution	Factor: 1	1.0	Dilution	Factor:	1.0			1.0		Factor:	1.0
		Percen	t Solid: N	IA %	Percen	t Solid: 1	۷A %	Percen		NA %	Percen		NA %	Percen		NA %
CRQL	Parameter	SQL	Result	Qual	SQL	Result	Qual	SQL	Result	Qual	SQL	Result	Qual	SQL	Result	Qual
10	Chloromethane	10	10	UJ	10	10	UJ	10	10	UJ	10	10	UJ	10	10	UJ
10	Bromomethane	10	10	UJ	10	10	UJ	10	10	UJ	10	10	Ū	10	10	UJ
10	Vinyl Chloride	10	10	UJ	10	10	UJ	10	10	UJ	10	10	UJ	10	10	Ü
10	Chloroethane	10	10	UJ	10	10	UJ	10	10	ÜJ	10	10	U	10	10	ŭ
10	Methylene Chloride	10	10	U	10	10	U	10	1	J	10	10	Ü	10	10	Ιŭ
10	Acetone	10	10	UJ	10	22	UJ	10	10	UJ	10	10	UJ	10	18	UJ
10	Carbon Disulfide	10	10	U	10	10	U	10	10	Ū	10	10	Ü	10	10	U
10	1,1-Dichloroethene	10	10	U	10	10	U	10	10	Ū	10	3	Ĵ	10	10	υ
10	1,1-Dichloroethane	10	10	U	10	10	U	10	10	Ū	10	2	J	10	10	Ū
10	Total 1,2-Dichloroethene	10	10	U	10	10	U	10	10	Ū	10	24		10	10	Ü
10	Chloroform	10	5	J	10	3	J	10	7	Ĵ	10	10	J	10	5	J
10	1,2-Dichloroethane	10	10	U	10	10	Ū	10	10	Ū	10	9	Ĵ	10	10	Ιŭ
10	2-Butanone	10	10	lυ	10	10	lυ	10	10	Ū	10	10	Ū	10	10	Ιŭ
10	1,1,1-Trichloroethane	10	10	U	10	10	Ū	10	10	Ū	10	1	Ĵ	10	1	Ĵ
10	Carbon Tetrachloride	10	10	U	10	10	U	10	10	Ū	10	10	Ü	10	10	Ü
10	Bromodichloromethane	10	10	Ū	10	10	Ū	10	10	Ü	10	10	ΙŪ	10	10	υ
10	1,2-Dichloropropane	10	10	U	10	10	U	10	10	Ū	10	10	Ü	10	10	Ü
10	cis-1,3-Dichloropropene	10	10	U	10	10	U	10	10	Ū	10	10	Ū	10	10	Ü
10	Trichloroethene	10	10	U	10	10	U	10	10	U	10	56		10	45	
10	Dibromochloromethane	10	10	U	10	10	lυ	10	10	Ū	10	10	U	10	10	U
10	1,1,2-Trichloroethane	10	10	U	10	10	Ū	10	10	Ū	10	10	Ü	10	10	Ü
10	Benzene	10	10	U	10	10	Ū	10	10	Ū	10	10	Ü	10	10	Ü
10	trans-1,3-Dichloropropene	10	10	U	10	10	U	10	10	Ū	10	10	Ū	10	10	Ü
10	Bromoform	10	10	lυ	10	10	U	10	10	Ū	10	10	Ū	10	10	Ū
10	4-Methyl-2-Pentanone	10	10	ĺυ	10	10	Ū	10	10	Ü	10	10	Ü	10	10	υ
10	2-Hexanone	10	10	U	10	10	Ū	10	10	Ū	10	10	Ü	10	10	Ü
10	Tetrachloroethene	10	10	Ū	10	10	Ū	10	10	Ü	10	50	"	10	2	J
10	Toluene	10	3	Ĵ	10	10	Ü	10	10	Ü	10	10	lυ	10	2	Ĵ
10	1,1,2,2-Tetrachloroethane	10	10	Ū	10	10	Ū	10	10	Ü	10	10	ΙŬ	10	10	Ü
10	Chlorobenzene	10	10	Ū	10	10	Ü	10	10	Ιŭ	10	10	ΙÜ	10	10	υ
10	Ethylbenzene	10	10	Ū	10	10	Ü	10	10	υ	10	10	U	10	2	J
10	Styrene	10	10	Ū	10	10	Ü	10	10	Ü	10	10	Ü	10	10	Ιŭ
10	Total Xylenes	10	10	UJ	10	10	Ū	10	10	Ü	10	10	U	10	8	l ŭ

Notes:

All units are µg/l.

Sample Quantitation Limit (SQL) is the CRQL multiplied by the dilution factor.

The Qual column indicates the qualifier applied to the result following data validation.

NA indicates Not Applicable.

MW-14RD is a field duplicate of MW-14R.

MW-18DD is a field duplicate of MW-18D.

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**Golder Associates** 

1 of 3

#### SUMMARY OF CLP ORGANICS ANALYSES

943-6222

216 Paterson Plank Road Site Sample Results Volatile Organics

Matrix: Groundwater

		S	ample Poi	nt	s	ample Poi	nt	s	ample Poir	nt	s	ample Poi	nt	s	ample Poi	nt
			MW-14R			MW-14RD	)		MW-15D		1	MW-16D			MW-17D	
		Date S	ampled:9/	23/96	Date Sampled: 9/23/96 Date Sampled: 9/24/96 D					Date Sampled: 9/23/96			Date Sampled: 9/19/96			
		Dilution	Factor:	1.0	l .	Factor:		1		1.0	1	Factor:		1	n Factor:	1.0
		Percen	t Solid:	NA %	Percen	t Solid:	NA %	1		NA %	1		NA %	1		NA %
CRQL	Parameter	SQL	Result	Qual	SQL	Result	Qual	SQL	Result	Qual	SQL	Result	Qual	SQL	Result	Qual
10	Chloromethane	10	10	UJ	10	10	UJ	10	10	U	10	10	UJ	10	10	UJ
10	Bromomethane	10	10	UJ	10	10	UJ	10	10	Ū	10	10	UJ	10	10	UJ
10	Vinyl Chloride	10	10	Ū	10	10	U	10	10	UJ	10	10	U	10	10	UJ
10	Chloroethane	·   10	10	Ū	10	10	Ü	10	10	U	10	10	Ü	10	10	UJ
10	Methylene Chloride	10	10	Ū	10	10	Ü	10	10	Ιŭ	10	10	υ	10	10	U
10	Acetone	10	10	UJ	10	13	UJ	10	10	UJ	10	190	UJ	10	10	Ü
10	Carbon Disulfide	10	10	υ	10	10	U	10	10	U	10	10	U	10	10	U
10	1,1-Dichloroethene	10	10	U	10	10	ΙŪ	10	10	υ	10	6	Ĵ	10	10	ŭ
10	1,1-Dichloroethane	10	10	Ū	10	10	Ū	10	10	ΙŬ	10	3	j	10	10	υ
10	Total 1,2-Dichloroethene	10	10	lυ	10	10	Ū	10	10	ΙŪ	10	30		10	10	Ιŭ
10	Chloroform	10	10	υ	10	10	Ū	10	10	ΙŪ	10	1	J	10	10	Ιŭ
10	1,2-Dichloroethane	10	10	υ	10	10	Ū	10	10	ΙŪ	10	11	"	10	10	Ιŭ
10	2-Butanone	10	10	ĺυ	10	10	Ū	10	10	Ū	10	10	υ	10	10	Ιŭ
10	1,1,1-Trichloroethane	10	10	U	10	10	Ū	10	10	Ü	10	3	Ĵ	10	10	Ιŭ
10	Carbon Tetrachloride	10	10	U	10	10	lυ	10	10	Ū	10	10	U	10	10	Ū
10	Bromodichloromethane	10	10	U	10	10	υ	10	10	Ū	10	10	Ū	10	10	Ū
10	1,2-Dichloropropane	10	10	U	10	10	Ū	10	10	Ιŭ	10	10	Ü	10	10	Ü
10	cis-1,3-Dichloropropene	10	10	U	10	10	Ū	10	10	Ū	10	10	Ū	10	10	Ιŭ
10	Trichloroethene	10	1	J	10	10	lυ	10	10	Ū	10	76		10	10	Ū
10	Dibromochloromethane	10	. 10	υ	10	10	U	10	10	Ū	10	10	υ	10	10	ĺΰ
10	1,1,2-Trichloroethane	10	10	υ	10	10	U	10	10	υ	10	10	Ū	10	10	υ
10	Benzene	10	10	υ	10	10	U	10	10	U	10	10	Ū	10	10	Ιŭ
10	trans-1,3-Dichloropropene	10	10	U	10	10	U	10	10	υ	10	10	Ū	10	10	Ū
10	Bromoform	10	10	υ	10	10	U	10	10	U	10	10	Ū	10	10	Ū
10	4-Methyl-2-Pentanone	10	10	υ	10	10	ļυ	10	10	U	10	10	Ū	10	10	Ū
10	2-Hexanone	10	10	U	10	10	U	10	10	U	10	10	Ū	10	10	Ū
10	Tetrachloroethene	10	10	υ	10	10	U	10	10	U	10	21		10	10	Ū
10	Toluene	10	10	υ	10	10	U	10	10	Ü	10	10	υ	10	10	Ü
10	1,1,2,2-Tetrachloroethane	10	10	ļυ	10	10	Ū	10	10	Ü	10	10	Ū	10	10	ŭ
10	Chlorobenzene	10	10	υ	10	10	U	10	10	Ū	10	10	Ū	10	10	ŭ
10	Ethylbenzene	10	10	υ	10	10	Ū	10	10	Ū	10	10	υ	10	10	υ
10	Styrene	10	10	U	10	10	Ū	10	10	Ū	10	10	υ	10	10	Ü
10	`Total Xylenes	10	10	υ	10	10	Ū	10	10	U	10	10	Ü	10	10	Ü

Notes:

All units are µg/l.

Sample Quantitation Limit (SQL) is the CRQL multiplied by the dilution factor.

The Qual column indicates the qualifier applied to the result following data validation.

NA indicates Not Applicable.

MW-14RD is a field duplicate of MW-14R.

MW-18DD is a field duplicate of MW-18D.

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January--, ⊍97

#### SUMMARY OF CLP ORGANICS ANALYSES 216 Paterson Plank Road Site Sample Results

Volatile Organics

943-6222

Matrix: Groundwater

			ample Poir	 it	s	ample Poir	nt	s	ample Poi	nt	S	ample Point		s	ample Poin	t
		ľ	MW-18D			MW-18DD			PW-01							
		Date S	ampled:9/1	9/96	Date S	ampled: 9/	19/96	Date S	ampled: 9/	23/96	Date S	ampled:		Date S	ampled:	
		Dilution	Factor:	1.0	Dilution	Factor:	1.0	Dilution	Factor:	1.0	Dilution	Factor:		Dilution	n Factor:	
		Percen	t Solid: 1	NA %	Percen	t Solid: 1	NA %	Percen		NA %	Percen	t Solid:	%	Percer	t Solid:	%
CRQL	Parameter	SQL	Result	Qual	SQL	Result	Qual	SQL	Result	Qual	SQL	Result	Qual	SQL	Result	Qual
10	Chloromethane	10	10	UJ	10	10	ÜJ	10	10	U						+
10	Bromomethane	10	10	UJ	10	10	UJ	10	10	U						
10	Vinyl Chloride	10	10	UJ	10	10	UJ	10	10	U						
10	Chloroethane	10	10	UJ	10	10	UJ	10	10	υ	l I					
10	Methylene Chloride	10	1	J	10	1	J	10	10	U						
10	Acetone	10	10	UJ	10	10	UJ	10	12	UJ		ı				
10	Carbon Disulfide	10	10	U	10	10	υ	10	10	U						
10	1,1-Dichloroethene	10	10	U	10	10	U	10	10	U						
10	1,1-Dichloroethane	10	10	U	10	10	U	10	10	Ü		l	1	l		
10	Total 1,2-Dichloroethene	10	10	U	10	10	U	10	10	Ū						
10	Chloroform	10	10	υ	10	10	U	10	23	-						
10	1,2-Dichloroethane	10	10	U	10	10	U	10	10	U						
10	2-Butanone	10	10	U	10	10	U	10	10	Ū						
10	1,1,1-Trichloroethane	10	10	U	10	10	υ	10	10	Ū						
10	Carbon Tetrachloride	10	10	U	10	10	U	10	10	Ü						ŀ
10	Bromodichloromethane	10	10	U	10	10	Ū	10	11	-						
10	1,2-Dichloropropane	10	10	U	10	10	υ	10	10	U						
10	cis-1,3-Dichloropropene	10	10	U	10	10	U	10	10	Ū						
10	Trichloroethene	10	10	U	10	10	U	10	10	Ū						
10	Dibromochloromethane	10	10	U	10	10	U	10	4	Ĵ		i				Ĭ
10	1,1,2-Trichloroethane	10	10	U	10	10	U	10	10	Ü	ĺ		Ï	[		
10	Benzene	10	10	ļυ	10	10	U	10	10	ΙŪ						
10	trans-1,3-Dichloropropene	10	10	U	10	10	U	10	10	Ú						
10	Bromoform	10	10	U	10	10	U	10	10	Ü						
10	4-Methyl-2-Pentanone	10	10	U	10	10	U	10	10	Ū						
10	2-Hexanone	10	10	U	10	10	U	10	10	Ü						
10	Tetrachloroethene	10	10	U	10	10	Ū	10	10	Ū						
10	Toluene	10	10	U	10	10	Ū	10	10	Ü						
10	1,1,2,2-Tetrachloroethane	10	10	U	10	10	U	10	10	Ü						
10	Chlorobenzene	10	10	U	10	10	U	10	10	Ü						
10	Ethylbenzene	10	10	U	10	10	Ū	10	10	Ü						
10	Styrene	10	10	U	10	10	Ū	10	10	Ü				1		
10	Total Xylenes	10	10	U	10	10	U	10	10	Ū						

Notes:

All units are µg/l.

Sample Quantitation Limit (SQL) is the CRQL multiplied by the dilution factor.

The Qual column indicates the qualifier applied to the result following data validation.

NA indicates Not Applicable.

MW-14RD is a field duplicate of MW-14R.

MW-18DD is a field duplicate of MW-18D.

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#### **SUMMARY OF CLP ORGANICS ANALYSES**

943-6222

216 Paterson Plank Road Site Sample Results Semivolatile Organics

Matrix: Groundwater

		S	ample Poir	nt	S	ample Poi	nt	S	ample Poir	nt	S	ample Point	t	s	ample Poir	i
			MW-08R		}	MW-10D			MW-10R			MW-11R			MW-14D	
		Date Sa	ampled:9/1	9/96	Date S	ampled: 9/	20/96	Date Sa	ampled: 9/2	20/96	Date Sa	ampled: 9/2	4/96	Date S	ampled: 9/2	23/96
		Dilution	Factor:	1.0	Dilution	Factor:	1.0	Dilution	Factor:	1.0	Dilution	Factor: 1	.0		Factor:	1.0
		Percen	t Solid:	NA %	Percen	t Solid:	NA %	Percen		NA %	Percen		NA %	Percen		NA %
CRQL	Parameter	SQL	Result	Qual	SQL	Result	Qual	SQL	Result	Qual	SQL	Result	Qual	SQL	Result	Qual
10	Phenol	10	10	U	10	10	U	10	10	U	10	19	1	10	10	U
10	bis(2-Chloroethyl)ether	10	10	Ŭ	10	10	Ü	10	10	Ιŭ	10	10	U	10	10	Ιŭ
10	2-Chlorophenol	10	10	Ū	10	10	Ū	10	10	Ü	10	10	Ιŭ	10	10	Ιŭ
10	1,3-Dichlorobenzene	10	10	ŭ	10	10	Ŭ	10	10	Ŭ	10	10	Ιŭ	10	10	Ü
10	1,4-Dichlorobenzene	10	10	ŭ	10	10	Ŭ	10	10	Ιŭ	10	10	Ιŭ	10	10	Ιŭ
10	1,2-Dichlorobenzene	10	10	ŭ	10	10	ŭ	10	10	Ιŭ	10	10	υ	10	10	١ŭ
10	2-Methylphenol	10	10	ŭ	10	10	ŭ	10	10	Ιŭ	10	10	Ü	10	10	Ü
10	2,2'-Oxybis(1-Chloropropane)	10	10	ŭ	10	10	ŭ	10	10	Ιŭ	10	10	Ü	10	10	ŭ
10	4-Methylphenol	10	10	Ιŭ	10	10	Ü	10	10	Ιŭ	10	10	Ü	10	10	Ü
10	N-Nitroso-di-n-propylamine	10	10	Ιŭ	10	10	Ιŭ	10	10	Ιŭ	10	10	Ιŭ	10	10	ΙÜ
10	Hexachloroethane	10	10	Ιŭ	10	10	Ü	10	10	Ιŭ	10	10	Ιŭ	10	10	Ιŭ
10	Nitrobenzene	10	10	ŭ	10	10	Ü	10	10	Ιŭ	10	10	Ιŭ	10	10	Ιŭ
10	Isophorone	10	10	Ū	10	10	Ū	10	10	Ιŭ	10	10	Ιŭ	10	10	Ιŭ
10	2-Nitrophenol	10	10	ŭ	10	10	Ü	10	10	Ιŭ	10	10	Ιŭ	10	10	Ιŭ
10	2,4-Dimethylphenol	10	10	Ιŭ	10	10	Ü	10	10	Ιŭ	10	10	Ιŭ	10	10	Ιŭ
10	bis(2-Chloroethoxy)Methane	10	10	Ü	10	10	Ü	10	10	Ιŭ	10	10	Ιŭ	10	10	Ιŭ
10	2,4-Dichlorophenol	10	10	Ū	10	10	Ŭ	10	10	Ŭ	10	10	Ιŭ	10	10	Ιŭ
10	1,2,4-Trichlorobenzene	10	10	Ū	10	10	Ŭ	10	10	Ŭ	10	10	Ιŭ	1 10	10	Ιŭ
10	Naphthalene	10	10	Ū	10	10	ŭ	10	10	Ιŭ	10	10	Ιŭ	10	10	Ιŭ
10	4-Chloroaniline	10	10	Ū	10	10	Ŭ	10	10	Ιŭ	10	10	Ιŭ	10	10	ŭ
10	Hexachlorobutadiene	10	10	Ū	10	10	Ū	10	10	Ιŭ	10	10	Ü	10	10	Ιŭ
10	4-Chloro-3-Methylphenol	10	10	Ū	10	10	Ιŭ	10	10	ľű	10	10	Ü	10	10	Ιŭ
10	2-Methylnaphthalene	10	10	Ū	10	10	ŭ	1 10	10	Ιŭ	10	10	Ιŭ	10	10	Ιŭ
10	Hexachlorocyclopentadiene	10	10	U	10	10	Ü	10	10	Ιŭ	10	10	Ιŭ	10	10	Ιŭ
10	2,4,6-Trichlorophenoi	10	10	U	10	10	Ü	10	10	Ιŭ	10	10	Ŭ	10	10	υ
25	2,4,5-Trichlorophenol	25	25	U	25	25	Ιū	25	25	Ιŭ	25	25	Ιŭ	25	25	Ιŭ
10	2-Chloronaphthalene	10	10	Ū	10	10	Ü	10	10	Ιŭ	10	10	Ιŭ	10	10	Ιŭ
25	2-Nitroaniline	25	25	Ū	25	25	Ιŭ	25	25	Ιŭ	25	25	Ιŭ	25	25	Ιŭ
10	Dimethyl Phthalate	10	10	Ü	10	10	Ιŭ	10	10	Ιŭ	10	10	Ιŭ	10	10	Ιŭ
10	Acenaphthylene	10	10	Ü	10	10	Ιŭ	1 10	10	Ιŭ	10	10	Ιŭ	10	10	Ιŭ
10	2,6-Dinitrotoluene	10	10	Ü	10	10	Ιŭ	10	10	Ιŭ	10	10	Ιŭ	10	10	Ιŭ
25	3-Nitroaniline	25	25	Ü	25	25	Ιŭ	25	25	Ιŭ	25	25	Ιŭ	25	25	Ü
10	Acenaphthene	10	10	Ū	10	10	Ü	10	10	Ιŭ	10	10	Ŭ	10	10	Ιŭ
Notes		·								, 0			, 0	0	, 10	, 0

#### Notes:

All units are µg/l.

Sample Quantitation Limit (SQL) is the CRQL multiplied by the dilution factor.

The Qual column indicates the qualifier applied to the result following data validation.

NA indicates Not Applicable.

MW-14RD is a field duplicate of MW-14R.

MW-18DD is a field duplicate of MW-18D.

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**Golder Associates** 

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#### SUMMARY OF CLP ORGANICS ANALYSES

943-6222

216 Paterson Plank Road Site Sample Results Semivolatile Organics

Matrix: Groundwater

		S	ample Poir	 nt	s	ample Poir	 nt	s	ample Poi	nt	S	ample Poir	t	S	ample Poin	,
			MW-08R			MW-10D			MW-10R			MW-11R			MW-14D	
		Date S	ampled:9/1	9/96	Date S	ampled: 9/	20/96	Date S	ampled: 9/	20/96	Date Sa	ampled: 9/2	24/96	Date S	ampled: 9/2	23/96
		Dilution	Factor:	1.0	Dilution	Factor:	1.0	Dilution	Factor:	1.0	Dilution	Factor:	1.0	Dilution	Factor:	1.0
		Percen	t Solid:	NA %	Percen	t Solid:	NA %	Percen	t Solid:	NA %	Percen	t Solid:	NA %	Percen		NA %
CRQL	Parameter	SQL	Result	Qual	SQL	Result	Qual	SQL	Result	Qual	SQL	Result	Qual	SQL	Result	Qual
10	Dibenzofuran	10	10	U	10	10		10	10	U	10	10	U	10	10	Ü
10	2,4-Dinitrotoluene	10	10	U	10	· 10	U	10	10	Ū	10	10	Ιŭ	10	10	Ü
10	Diethylphthalate	10	10	U	10	10	Ů	10	10	ŭ	10	10	Ιŭ	10	10	Ιŭ
10	4-Chlorophenyl-phenylether	10	10	U	10	10	Ū	10	10	Ιŭ	10	10	Ιŭ	10	10	Ŭ
10	Fluorene	10	10	υ	10	10	U	10	10	ŭ	10	10	Ιŭ	10	10	Ιŭ
25	4-Nitroaniline	25	25	υ	25	25	U	25	25	ŭ	25	25	UJ	25	25	Ŭ
25	4,6-Dinitro-2-methylphenol	25	25	υ	25	25	Ū	25	25	ŭ	25	25	Ü	25	25	Ü
10	N-Nitrosodiphenylamine	10	10	U	10	10	Ū	10	10	Ü	10	10	Ιŭ	10	10	Ü
10	4-Bromophenyl-phenylether	10	10	Ú	10	10	Ιŭ	10	10	Ŭ	10	10	Ιŭ	10	10	Ιŭ
10	Hexachlorobenzene	10	10	Ú	10	10	Ū	10	10	Ū	10	10	Ιŭ	10	10	Ιŭ
25	Pentachlorophenol	25	25	Ú	25	25	Ü	25	25	Ü	25	25	Ü	25	25	Ιŭ
10	Phenanthrene	10	10	Ú	10	10	Ū	10	10	Ü	10	10	ŭ	10	10	Ιŭ
10	Anthracene	10	10	U	10	10	U	10	10	Ū	10	10	Ιŭ	10	10	Ιŭ
10	Carbazole	10	10	U	10	10	U	10	10	ŭ	10	10	Ιŭ	10	10	Ιŭ
10	Di-n-butylphthalate	10	10	U	10	10	Ū	10	10	ŭ	10	10	UJ	10	10	Ü
10	Fluoranthene	10	10	Ū	10	10	Ū	10	10	Ŭ	10	10	UJ	10	10	Ιŭ
10	Pyrene	10	10	U	10	10	Ū	10	10	ŭ	10	10	ÜĴ	10	10	Ŭ
10	Butylbenzylphthalate	10	10	U	10	10	Ū	10	10	Ū	10	10	u	10	10	Ŭ
10	3,3'-Dichlorobenzidine	10	10	U	10	10	U	10	10	Ū	10	10	Ü	10	10	ĺΰ
10	Benzo(a)Anthracene	10	10	U	10	10	Ū	10	10	Ū	10	10	l ŭ	10	10	Ιŭ
10	Chrysene	10	10	U	10	10	U	10	10	Ū	10	10	l ŭ	10	10	Ιŭ
10	bis(2-Ethylhexyl)Phthalate	10	10	U	10	10	Ú	10	10	Ū	10	10	l ŭ	10	10	Ιŭ
10	Di-n-Octyl Phthalate	10	10	U	10	10	ĺΰ	10	10	Ū	10	10	Ŭ	10	10	Ιŭ
10	Benzo(b)Fluoranthene	10	10	U	10	10	Ū	10	10	Ü	10	10	Ŭ	10	10	ŭ
10	Benzo(k)Fluoranthene	10	10	U	10	10	Ū	10	10	ΙŪ	10	10	Ιŭ	10	10	Ü
10	Benzo(a)Pyrene	10	10	U	10	10	Ū	10	10	Ū	10	10	Ιŭ	10	10	Ιŭ
10	Indeno(1,2,3-cd)Pyrene	10	10	U	10	10	Ū	10	10	ΙŪ	10	10	Ιŭ	10	10	Ιŭ
10	Dibenz(a,h)Anthracene	10	10	U	10	10	U	10	10	Ū	10	10	Ū	10	10	Ιŭ
10	Benzo(g,h,i)Perylene	10	10	U	10	10	U	10	10	Ū	10	10	Ū	10	10	Ιŭ

#### Notes:

All units are µg/l.

Sample Quantitation Limit (SQL) is the CRQL multiplied by the dilution factor.

The Qual column indicates the qualifier applied to the result following data validation.

NA indicates Not Applicable.

MW-14RD is a field duplicate of MW-14R.

MW-18DD is a field duplicate of MW-18D.

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#### SUMMARY OF CLP ORGANICS ANALYSES

943-6222

216 Paterson Plank Road Site Sample Results Semivolatile Organics

Matrix: Groundwater

		S	ample Point		s	ample Point		S	ample Poin	· t	S	ample Poin	 t	l s	ample Poin	ıt -[
			MW-14R			MW-14RD			MW-15D			MW-16D			MW-17D	- 1
		Date Sa	ampled:9/23	/96	Date S	ampled: 9/2	3/96	Date Sa	ampled: 9/2	4/96	Date Sa	ampled: 9/2	3/96	Date Sa	ampled: 9/	19/96
		Dilution	Factor: 1.	.0	Dilution	Factor: 1	.0	Dilution	Factor: 1	.0	Dilution	Factor: 1	.0	l	Factor:	1.0
		Percent	t Solid: N	NA %	Percen	t Solid: N	VA %	Percent		NA %	1		NA %	Percen		NA %
CRQL	Parameter	SQL	Result	Qual	SQL	Result	Qual	SQL	Result	Qual	SQL	Result	Qual	SQL	Result	Qual
10	Phenol	10	10	U	10	10	Ü	10	10	U	10	10	U	10	10	U
10	bis(2-Chloroethyl)ether	10	10	Ū	10	10	Ū	10	10	Ü	10	10	Ü	10	10	l ŭ l
10	2-Chlorophenol	10	10	Ū	10	10	Ū	10	10	Ū	10	10	Ŭ	10	10	ΙŭΙ
10	1,3-Dichlorobenzene	10	10	Ū	10	10	Ū	10	10	Ŭ	10	10	Ŭ	10	10	l ŭ l
10	1,4-Dichlorobenzene	10	10	Ū	10	10	Ū	10	10	Ŭ	10	10	ŭ	10	10	∣ŭ l
10	1,2-Dichlorobenzene	10	10	Ū	10	10	Ū	10	10	Ŭ	10	10	ŭ	10	10	ΙŭΙ
10	2-Methylphenol	10	10	U	10	10	Ū	10	10	Ū	10	10	Ιŭ	10	10	l ŭ l
10	2,2'-Oxybis(1-Chloropropane)	10	10	U	10	10	U	10	10	Ū	10	10	Ū	10	10	انا
10	4-Methylphenol	10	10	U	10	10	Ū	10	10	Ū	10	10	ŭ	10	10	l ŭ l
10	N-Nitroso-di-n-propylamine	10	10	U	10	10	U	10	10	Ū	10	10	Ŭ	10	10	l ŭ l
10	Hexachloroethane	10	10	U	10	10	U	10	10	U	10	10	Ιū	10	10	ΙŭΙ
10	Nitrobenzene	10	10	U	10	10	U	10	10	U	10	10	Ū	10	10	ΙŭΙ
10	Isophorone	10	10	U	10	10	U	10	10	U	10	10	U	10	10	ΙŭΙ
10	2-Nitrophenol	10	10	U	10	10	U	10	10	U	10	10	U	10	10	ΙŭΙ
10	2,4-Dimethylphenol	10	10	U	10	10	U	10	10	U	10	10	U	10	10	ΙŭΙ
10	bis(2-Chloroethoxy)Methane	10	10	U	10	10	U	10	10	U	10	10	U	10	10	ΙŭΙ
10	2,4-Dichlorophenol	10	10	U	10	10	U	10	10	U	10	10	U	10	10	ΙŭΙ
10	1,2,4-Trichlorobenzene	10	10	U	10	10	U	10	10	U	10	10	U	10	10	ΙυΙ
10	Naphthalene	10	10	U	10	10	U	10	10	U	10	10	U	10	10	U
10	4-Chloroaniline	10	10	U	10	10	U	10	10	U	10	10	U	10	10	lυl
10	Hexachlorobutadiene	10	10	U	10	10	U	10	10	U	10	10	U	10	10	U
10	4-Chloro-3-Methylphenol	10	10	U	10	10	U	10	10	U	10	10	U	10	10	U
10	2-Methylnaphthalene	10	10	U	10	10	U	10	10	U	10	10	U	10	10	U
10	Hexachlorocyclopentadiene	10	10	U	10	10	U	10	10	U	10	10	U	10	10	U
10	2,4,6-Trichlorophenol	10	10	U	10	10	U	10	10	U	10	10	U	10	10	U
25	2,4,5-Trichlorophenol	25	25	U	25	25	U	25	25	U	25	25	U	25	25	U
10	2-Chloronaphthalene	10	10	U	10	10	U	10	10	U	10	10	U,	10	10	U
25	2-Nitroaniline	25	25	U	25	25	U	25	25	U	25	25	U	25	25	U
10	Dimethyl Phthalate	10	10	U	10	10	U	10	10	U	10	10	U	10	10	U
10	Acenaphthylene	10	10	U	10	10	U	10	10	U	10	10	U	10	10	υ
10	2,6-Dinitrotoluene	10	10	U	10	10	U	10	10	U	10	10	U	10	10	U
25	3-Nitroaniline	25	25	U	25	25	U	25	25	U	25	25	U	25	25	U
10	Acenaphthene	10	10	U	10	10	U	10	10	U	10	10	U	10	10	U
25	2,4-Dinitrophenol	25	25	U	25	25	U	25	25	U	25	25	U	25	25	U
25	4-Nitrophenol	25	25	U	25	25	U	25	25	U	25	25	U	25	25	U

Notes:

All units are μg/l.

Sample Quantitation Limit (SQL) is the CRQL multiplied by the dilution factor.

The Qual column indicates the qualifier applied to the result following data validation.

NA indicates Not Applicable.

MW-14RD is a field duplicate of MW-14R.

MW-18DD is a field duplicate of MW-18D.

ACCESS\carlstad.mb1svoc report (11/6/96) new wells

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#### SUMMARY OF CLP ORGANICS ANALYSES

943-6222

216 Paterson Plank Road Site Sample Results Semivolatile Organics

Matrix: Groundwater

		S	ample Poin	t	S	ample Poin	 t	S	ample Poi	nt	S	ample Poir	nt	s	ample Poin	nt I
			MW-14R			MW-14RD			MW-15D			MW-16D			MW-17D	
		Date S	ampled:9/2	3/96	Date Sa	ampled: 9/2	3/96	Date Sa	ampled: 9/	24/96	Date Sa	ampled: 9/	23/96	Date S	ampled: 9/1	19/96
		Dilution	Factor:	1.0	Dilution	Factor: 1	.0	l .	•	1.0	l	•	1.0		Factor:	1.0
		Percen	t Solid:	NA %	Percen		NA %	Percen		NA %	Percen		NA %	Percen		NA %
CRQL	Parameter	SQL	Result	Qual	SQL	Result	Qual	SQL	Result	Qual	SQL	Result	Qual	SQL	Result	Qual
10	Dibenzofuran	10	10	U	10	10	- υ ·	10	10	U	10	10	U	10	10	U
10	2,4-Dinitrotoluene	10	10	Ū	10	10	Ū	10	10	ϋ	10	10	Ŭ	10	10	l ŭ l
10	Diethylphthalate	10	10	lυ	10	10	Ū	10	10	Ū	10	10	Ü	10	10	ΙŭΙ
10	4-Chlorophenyl-phenylether	10	10	Ū	10	10	Ū	10	10	Ü	10	10	Ŭ	10	10	ΙŭΙ
10	Fluorene	10	10	ΙŪ	10	10	Ü	10	10	Ŭ	10	10	Ιŭ	10	10	υ
25	4-Nitroaniline	25	25	Ū	25	25	Ū	25	25	Ü	25	25	Ŭ	25	25	Ü
25	4,6-Dinitro-2-methylphenol	25	25	U	25	25	Ū	25	25	Ιŭ	25	25	Ιŭ	25	25	Ü
10	N-Nitrosodiphenylamine	10	10	U	10	10	Ū	10	10	Ιŭ	10	10	Ιŭ	10	10	Ü
10	4-Bromophenyl-phenylether	10	10	Ū	10	10	Ū	10	10	Ιŭ	10	10	Ιŭ	10	10	Ü
10	Hexachlorobenzene	10	10	lυ	10	10	Ū	10	10	Ιŭ	10	10	Ü	10	10	ŭ
25	Pentachlorophenol	25	25	lυ	25	25	Ū	25	25	Ιŭ	25	25	Ιŭ	25	25	ŭ
10	Phenanthrene	10	10	U	10	10	U	10	10	Ιŭ	10	10	Ιŭ	10	10	ŭ
10	Anthracene	10	10	ĺυ	10	10	Ū	10	10	Ιŭ	10	10	Ιŭ	10	10	Ü
10	Carbazole	10	10	U	10	10	U	10	10	ΙŪ	10	10	Ŭ	10	10	Ü
10	Di-n-butylphthalate	10	10	lυ	10	10	U	10	10	Ιŭ	10	10	Ü	1 10	10	ϋ
10	Fluoranthene	10	10	lυ	10	10	Ū	10	10	Ιŭ	10	10	Ŭ	10	10	ϋ
10	Pyrene	10	1	JN	10	10	U	10	10	Ιŭ	10	10	Ŭ	10	10	Ŭ
10	Butylbenzylphthalate	10	10	ļυ	10	10	Ū	10	10	Ιŭ	10	10	Ŭ	10	10	ϋ
10	3,3'-Dichlorobenzidine	10	10	U	10	10	Ū	10	10	Ιŭ	10	10	Ü	1 10	10	Ιŭ
10	Benzo(a)Anthracene	10	10	·υ	10	10	U	10	10	Ιŭ	10	10	Ιŭ	1 10	10	ϋ
10	Chrysene	10	10	ļυ	10	10	U	10	10	Ιŭ	10	10	Ιŭ	10	10	Ιŭ
10	bis(2-Ethylhexyl)Phthalate	10	10	U	10	10	U	10	10	Ū	10	1	J	10	10	Ŭ
10	Di-n-Octyl Phthalate	10	10	U	10	10	Ū	10	10	Ιŭ	10	10	Ιŭ	10	10	Ŭ
10	Benzo(b)Fluoranthene	10	10	U	10	10	U	10	10	Ū	10	10	Ιŭ	10	10	ŭ
10	Benzo(k)Fluoranthene	10	10	U	10	10	Ū	10	10	ΙŬ	10	10	Ιŭ	10	10	Ιŭ
10	Benzo(a)Pyrene	10	10	U	10	10	U	10	10	ΙŪ	10	10	Ü	10	10	Ŭ
10	Indeno(1,2,3-cd)Pyrene	10	10	U	10	10	U	10	10	ΙŪ	10	10	Ü	10	10	ϋ
10	Dibenz(a,h)Anthracene	10	10	U	10	10	Ū	10	10	Ιŭ	10	10	Ιŭ	10	10	Ŭ
10	Benzo(g,h,i)Perylene	10	10	U	_10	10	U	10	10	Ū	10	10	Ū	10	10	Ū

#### Notes:

All units are µg/l.

Sample Quantitation Limit (SQL) is the CRQL multiplied by the dilution factor.

The Qual column indicates the qualifier applied to the result following data validation.

NA indicates Not Applicable.

MW-14RD is a field duplicate of MW-14R.

MW-18DD is a field duplicate of MW-18D.

ACCESS\cardstad.mb1svoc report (11/6/96) new wells

1/17/97 4:04:11 PM

#### SUMMARY OF CLP ORGANICS ANALYSES

943-6222

216 Paterson Plank Road Site Sample Results Semivolatile Organics

Matrix: Groundwater

		S	ample Poir	nt -		ample Poin	t	S	ample Poir	nt	s	ample Poin	t	S	ample Poin	i
			MW-18D		ı	MW-18DD			PW-01							
		Date Sa	ampled:9/1	9/96	Date S	ampled: 9/1	9/96	Date Sa	ampled: 9/	23/96	Date S	ampled:		Date S	ampled:	
		Dilution	Factor:	1.0	Dilution	Factor:	1.0	Dilution	Factor:	1.0	Dilution	Factor:		Dilution	Factor:	
		Percen	t Solid:	NA %	Percen	t Solid:	NA %	Percen	t Solid:	NA %	Percen	t Solid:	%	Percen	t Solid:	%
CRQL	Parameter	SQL	Result	Qual	SQL	Result	Qual	SQL	Result	Qual	SQL	Result	Qual	SQL	Result	Qual
10	Phenol	10	10	U	10	10		10	10	U			1			+
10	bis(2-Chloroethyl)ether	10	10	U	l 10	10	lυ	10	10	Ū	l				i	
10	2-Chlorophenol	10	10	lυ	10	10	Ū	10	10	Ιŭ			ł	1		
10	1,3-Dichlorobenzene	10	10	ΙŪ	10	10	Ü	10	10	Ιŭ	1					
10	1,4-Dichlorobenzene	10	10	Ū	10	10	Ιŭ	10	10	ΙŬ	ļ					
10	1,2-Dichlorobenzene	10	10	Ū	10	10	Ū	10	10	Ιŭ	1					
10	2-Methylphenol	10	10	Ū	10	10	Ū	10	10	Ιŭ						
10	2,2'-Oxybis(1-Chloropropane)	10	10	Ū	10	10	Ū	10	10	Ιŭ						
10	4-Methylphenol	10	10	Ū	10	10	Ŭ	10	10	Ιŭ	l	•				
10	N-Nitroso-di-n-propylamine	10	10	Ū	10	10	Ιŭ	10	10	Ü	l					
10	Hexachloroethane	10	10	Ū	10	10	Ŭ	10	10	Ιŭ	1					
10	Nitrobenzene	10	10	Ū	10	10	Ŭ	10	10	Ιŭ		ŀ				
10	Isophorone	10	10	Ū	10	10	Ŭ	10	10	Ιŭ		,				
10	2-Nitrophenol	10	10	Ū	10	10	Ŭ	10	10	Ιŭ						
10	2,4-Dimethylphenol	10	10	Ū	10	10	Ŭ	10	10	Ιŭ	l					
10	bis(2-Chloroethoxy)Methane	10	10	Ŭ	10	10	Ŭ	10	10	Ιŭ	l		1			
10	2,4-Dichlorophenol	10	10	Ū	10	10	Ŭ	10	10	Ιŭ	l					
10	1,2,4-Trichlorobenzene	10	10	Ū	10	10	Ü	10	10	Ü	l					
10	Naphthalene	10	10	Ū	10	10	Ŭ	10	10	Ιŭ	l		1			
10	4-Chloroaniline	10	10	Ū	10	10	Ŭ	10	10	Ιŭ	ł					
10	Hexachlorobutadiene	10	- 10	Ū	10	10	Ŭ	10	10	Ιŭ	l		1			
10	4-Chloro-3-Methylphenol	10	10	Ū	10	10	Ŭ	10	10	Ü	l					
10	2-Methylnaphthalene	10	10	Ū	10	10	Ŭ	10	10	Ιŭ	l					
10	Hexachlorocyclopentadiene	10	10	U	10	10	Ū	10	10	Ιŭ	l					
10	2,4,6-Trichlorophenol	10	10	Ū	10	10	Ŭ	10	10	Ιŭ	l					
25	2,4,5-Trichlorophenol	25	25	Ū	25	25	ŭ	25	25	Ιŭ			1			
10	2-Chloronaphthalene	10	10	υ	10	10	Ü	10	10	Ιŭ	l					
25	2-Nitroaniline	25	25	Ū	25	25	Ιŭ	25	25	Ιŭ	Ī					
10	Dimethyl Phthalate	10	10	Ιŭ	10	10	ľŭ	10	10	Ιŭ						
10	Acenaphthylene	10	10	Ιŭ	10	10	Ιŭ	10	10	Ü				]		
10	2,6-Dinitrotoluene	10	10	Ιŭ	10	10	Ιŭ	10	10	Ü						
25	3-Nitroaniline	25	25	Ιŭ	25	25	Ιŭ	25	25	U						
10	Acenaphthene	10	10	Ιŭ	10	10	l ŭ	10	10	Ü						
25	2,4-Dinitrophenol	25	25	U	25	25	U	25	25	U						
25	4-Nitrophenol	25	25	Ιŭ	25	25	Ü	25	25 25	UJ					!	
Motors				1_0_			0	20	25	00	l	<u> </u>	<u> </u>	I	l	1

#### Notes:

All units are µg/l.

Sample Quantitation Limit (SQL) is the CRQL multiplied by the dilution factor.

The Qual column indicates the qualifier applied to the result following data validation.

NA indicates Not Applicable.

MW-14RD is a field duplicate of MW-14R.

MW-18DD is a field duplicate of MW-18D.

ACCESS\carlstad.mb1svoc report (11/6/96) new wells 1/17/97 4:07:36 PM

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#### SUMMARY OF CLP ORGANICS ANALYSES

943-6222

216 Paterson Plank Road Site Sample Results Semivolatile Organics

Matrix: Groundwater

		S	ample Poin	t	s	ample Poi	nt	s	ample Poi	nt	s	ample Poin	t	s	ample Poin	
			MW-18D			MW-18DD	)		PW-01						•	1
		Date Sa	ampled:9/1	9/96	Date S	ampled: 9/	19/96	Date S	ampled: 9/	23/96	Date S	ampled:		Date S	ampled:	i
		Dilution	Factor: 1	.0	Dilution	Factor:	1.0	Dilution	Factor:	1.0	Dilution	Factor:		Dilution	Factor:	
		Percen	t Solid:	NA %	Percen	t Solid:	NA %	Percen	t Solid:	NA %	Percen	t Solid:	%	Percen		%
CRQL	Parameter	SQL	Result	Qual	SQL	Result	Qual	SQL	Result	Qual	SQL	Result	Qual	SQL	Result	Qual
10	Dibenzofuran	10	10	U	10	10	- U	10	10	U						+
10	2,4-Dinitrotoluene	10	10	lυ	10	10	U	10	10	Ū						
10	Diethylphthalate	10	10	U	10	10	lυ	10	10	Ū						
10	4-Chlorophenyl-phenylether	10	10	U	10	10	ΙŪ	10	10	Ιŭ		1				
10	Fluorene	10	10	U	10	10	ΙŪ	10	10	Ιŭ						
25	4-Nitroaniline	25	25	U	25	25	Ιŭ	25	25	Ιŭ						
25	4,6-Dinitro-2-methylphenol	25	25	U	25	25	Ιŭ	25	25	υ						
10	N-Nitrosodiphenylamine	10	10	U	10	10	Ū	10	10	Ü				ŀ		
10	4-Bromophenyl-phenylether	10	10	ĺυ	10	10	ΙŪ	10	10	Ü	ĺ	ĺ		į	•	1 1
10	Hexachlorobenzene	10	10	U	10	10	ΙŪ	10	10	Ŭ				ĺ		
25	Pentachlorophenol	25	25	U	25	25	ΙŪ	25	25	Ü		ļ				
10	Phenanthrene	10	10	U	10	10	ΙŪ	10	10	Ιŭ		i				
10	Anthracene	10	10	U	10	10	Ū	10	10	Ū		i				1 1
10	Carbazole	10	10	U	10	10	Ū	10	10	ΗŬ						
10	Di-n-butylphthalate	10	10	U	10	10	ΙŪ	10	10	Ū						
10	Fluoranthene	10	10	U	10	10	ΙŪ	10	10	ÜJ						
10	Pyrene	10	10	U	10	10	ΙŪ	10	10	Ü						
10	Butylbenzylphthalate	10	10	U	10	10	lυ	10	10	Ū						
10	3,3'-Dichlorobenzidine	10	10	U	10	10	Ū	10	10	ÜJ						
10	Benzo(a)Anthracene	10	10	U	10	10	Ū	10	10	Ü						
10	Chrysene	10	10	U	10	10	U	10	10	Ū				l		1 1
10	bis(2-Ethylhexyl)Phthalate	10	10	ĺυ	10	10	U	10	10	Ū	ĺ	1		ſ	ĺ	ìi
10	Di-n-Octyl Phthalate	10	10	U	10	10	ΙŪ	10	10	UJ						
10	Benzo(b)Fluoranthene	10	10	U	10	10	Ū	10	10	Ü						
10	Benzo(k)Fluoranthene	10	10	Ū	10	10	υŪ	10	10	Ιŭ						
10	Benzo(a)Pyrene	10	10	U	10	10	ΙŪ	10	10	Ιŭ						
10	Indeno(1,2,3-cd)Pyrene	10	10	U	10	10	Ū	10	10	υ						
10	Dibenz(a,h)Anthracene	10	10	Ū	10	10	υŪ	10	10	Ιŭ						
10	Benzo(g,h,i)Perylene	10	10	U	10	10	Ū	10	10	υ						

#### Notes:

All units are µg/l.

Sample Quantitation Limit (SQL) is the CRQL multiplied by the dilution factor.

The Qual column indicates the qualifier applied to the result following data validation.

NA indicates Not Applicable.

MW-14RD is a field duplicate of MW-14R.

MW-18DD is a field duplicate of MW-18D.

ACCESS\carlstad.mb1svoc report (11/6/96) new wells

1/17/97 4:04:19 PM

#### SUMMARY OF CLP ORGANICS ANALYSES

943-6222

216 Paterson Plank Road Site Sample Results Pesticides / PCBs

Matrix: Groundwater

		1	ample Poir	nt	s	ample Poir	nt	S	ample Poir	nt	S	ample Poi	nt	s	ample Poir	ıt
		1	MW-08R			MW-10D			MW-10R			MW-11R			MW-14D	
		Date Sa	ampled:9/1	9/96	Date S	ampled: 9/2	20/96	Date S	ampled: 9/	20/96	Date S	ampled: 9/	24/96	Date S	ampled: 9/2	23/96
		Dilution	Factor:	1.0	Dilution	Factor:	1.0	Dilution	Factor:	1.0	Dilution	Factor:	1.0	Dilution	Factor:	1.0
		Percent	Solid:	NA %	Percen	t Solid:	NA %	Percen	t Solid:	NA %	Percen	t Solid:	NA %	Percen	t Solid:	NA %
CRQL	Parameter	SQL	Result	Qual	SQL	Result	Qual	SQL	Result	Qual	SQL	Result	Qual	SQL	Result	Qual
0.05	alpha-BHC	0.05	0.05	U	0.05	0.05	U	0.05	0.05	U	0.05	0.05	U	0.05	0.05	U
0.05	beta-BHC	0.05	0.05	U	0.05	0.05	U	0.05	0.05	U	0.05	0.05	ĺυ	0.05	0.05	l ŭ l
0.05	delta-BHC	0.05	0.05	U	0.05	0.05	U	0.05	0.05	U	0.05	0.05	Ū	0.05	0.05	υ
0.05	gamma-BHC (Lindane)	0.05	0.05	U	0.05	0.05	U	0.05	0.05	U	0.05	0.05	U	0.05	0.05	l u l
0.05	Heptachlor	0.05	0.05	· U	0.05	0.05	U	0.05	0.05	U	0.05	0.05	Ü	0.05	0.05	l ŭ l
0.05	Aldrin	0.05	0.05	U	0.05	0.05	U	0.05	0.05	U	0.05	0.05	Ū	0.05	0.05	ا ن
0.05	Heptachlor Epoxide	0.05	0.05	U	0.05	0.05	U	0.05	0.05	U	0.05	0.05	Ū	0.05	0.05	ΙŭΙ
0.05	Endosulfan I	0.05	0.05	U	0.05	0.05	U	0.05	0.05	U	0.05	0.05	Ū	0.05	0.05	l ŭ l
0.1	Dieldrin	0.1	0.1	U	0.1	0.1	U	0.1	0.1	U	0.1	0.1	Ū	0.1	0.1	ΙŭΙ
0.1	4,4'-DDE	0.1	0.1	U	0.1	0.1	U	0.1	0.1	υ	0.1	0.1	Ū	0.1	0.1	Ū
0.1	Endrin	0.1	0.1	U	0.1	0.1	U	0.1	0.1	U	0.1	0.1	Ū	0.1	0.1	Ū
0.1	Endosulfan II	0.1	0.1	U	0.1	0.1	U	0.1	0.1	U	0.1	0.1	Ū	0.1	0.1	l ŭ l
0.1	4,4'-DDD	0.1	0.1	U	0.1	0.1	ļυ	0.1	0.1	U	0.1	0.1	U	0.1	0.1	Ū
0.1	Endosulfan Sulfate	0.1	0.1	ļυ	0.1	0.1	U	0.1	0.1	U	0.1	0.1	Ū	0.1	0.1	Ū
0.1	4,4'-DDT	0.1	0.1	U	0.1	0.1	U	0.1	0.1	U	0.1	0.1	U	0.1	0.1	Ū
0.5	Methoxychlor	0.5	0.5	U	0.5	0.5	ļυ	0.5	0.5	U	0.5	0.5	U	0.5	0.5	Ū
0.1	Endrin Ketone	0.1	0.1	U	0.1	0.1	U	0.1	0.1	U	0.1	0.1	Ü	0.1	0.1	l ŭ l
0.1	Endrin Aldehyde	0.1	0.1	U	0.1	0.1	U	0.1	0.1	U	0.1	0.1	U	0.1	0.1	ΙŪ
0.05	alpha-Chlordane	0.05	0.05	U	0.05	0.05	U	0.05	0.05	U	0.05	0.05	U	0.05	0.05	U
0.05	gamma-Chlordane	0.05	0.05	U	0.05	0.05	U	0.05	0.05	U	0.05	0.05	υ	0.05	0.05	Ū
5	Toxaphene	5	5	U	5	5	U	5	5	U	5	5	ļυ	5	5	Ū
1	Aroclor-1016	1 1	1	U	1	1	ļυ	1	1	υ	1	1	U	1	1	Ū
2	Aroclor-1221	2	2	U	2	2	U	2	2	U	2	2	U	2	2	Ü
1	Aroclor-1232	1	1	U	1	1	U	1	1	U	1	1	Ū	1	1	Ū
1	Aroclor-1242	1	1	U	1	1	U	1	1	υ	1	1	U	1	1	Ū
1	Aroclor-1248	1	1	U	1	1	U	1	1	U	1	1	Ū	1	1	υ
1	Aroclor-1254	1	1	U	1	1	U	1	1	Ū	] 1	1	Ü	1	1	ΙŭΙ
11	Aroclor-1260	1_1_	1	U	1	1	U	1	1	U	1	1	Ū	1	1	Ŭ

Notes:

All units are µg/l.

Sample Quantitation Limit (SQL) is the CRQL multiplied by the dilution factor.

The Qual column indicates the qualifier applied to the result following data validation.

NA indicates Not Applicable.

MW-14RD is a field duplicate of MW-14R.

MW-18DD is a field duplicate of MW-18D.

ACCESS\carlstad.mb1\pest report (11/6/96) new wells 1/21/97 3:12:29 PM

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#### SUMMARY OF CLP ORGANICS ANALYSES

#### 216 Paterson Plank Road Site Sample Results Pesticides / PCBs

Matrix: Groundwater

		S	ample Poi	nt	S	ample Poi	nt	S	ample Poi	nt	S	ample Poir	it	S	ample Poin	it
			MW-14R			MW-14RD	)		MW-15D			MW-16D			MW-17D	
		Date Sa	ampled:9/	23/96	Date S	ampled: 9	/23/96	Date S	ampled: 9/	24/96	Date S	ampled: 9/2	23/96	Date S	ampled: 9/1	19/96
		Dilution	Factor:	1.0	Dilution	Factor:	1.0	Dilution	Factor:	1.0	Dilution	Factor:	1.0	Dilution	Factor:	1.0
		Percen	t Solid:	NA %	Percen	t Solid:	NA %	Percen	t Solid:	NA %	Percen	t Solid:	NA %	Percen		NA %
CRQL	Parameter	SQL	Result	Qual	SQL	Result	Qual	SQL	Result	Qual	SQL	Result	Qual	SQL	Result	Qual
0.05	alpha-BHC	0.05	0.05	U	0.05	0.05	U	0.05	0.051	U	0.05	0.05	U	0.05	0.05	U
0.05	beta-BHC	0.05	0.05	U	0.05	0.05	U	0.05	0.022	U	0.05	0.05	U	0.05	0.05	U
0.05	delta-BHC	0.05	0.05	U	0.05	0.05	Ū	0.05	0.051	U	0.05	0.05	U	0.05	0.05	U
0.05	gamma-BHC (Lindane)	0.05	0.05	U	0.05	0.05	U	0.05	0.051	U	0.05	0.05	U	0.05	0.05	Ū
0.05	Heptachlor	0.05	0.05	U	0.05	0.05	U	0.05	0.051	U	0.05	0.05	U	0.05	0.05	U
0.05	Aldrin	0.05	0.05	U	0.05	0.05	U	0.05	0.051	U	0.05	0.05	U	0.05	0.05	U
0.05	Heptachlor Epoxide	0.05	0.05	U	0.05	0.05	U	0.05	0.051	U	0.05	0.05	U	0.05	0.05	U
0.05	Endosulfan I	0.05	0.05	U	0.05	0.05	U	0.05	0.051	U	0.05	0.05	U	0.05	0.05	Ū
0.1	Dieldrin	0.1	0.1	U	0.1	0.1	U	0.1	0.1	U	0.1	0.1	U	0.1	0.1	Ū
0.1	4,4'-DDE	0.1	0.1	U	0.1	0.1	U	0.1	0.1	J	0.1	0.1	ΙU	0.1	0.1	Ū
0.1	Endrin	0.1	0.1	U	0.1	0.1	U	0.1	0.1	U	0.1	0.1	U	0.1	0.1	U
0.1	Endosulfan II	0.1	0.1	U	0.1	0.1	U	0.1	0.1	J	0.1	0.1	U	0.1	0.1	Ū
0.1	4,4'-DDD	0.1	0.1	U	0.1	0.1	U	0.1	0.1	U	0.1	0.1	U	0.1	0.1	Ū
0.1	Endosulfan Sulfate	0.1	0.1	U	0.1	0.1	U	0.1	0.1	U	0.1	0.1	U	0.1	0.1	U
0.1	4,4'-DDT	0.1	0.1	U	0.1	0.1	U	0.1	0.1	U	0.1	0.1	υ	0.1	0.1	υ
0.5	Methoxychlor	0.5	0.5	U	0.5	0.5	U	0.5	0.51	υ	0.5	0.5	U	0.5	0.5	U
0.1	Endrin Ketone	0.1	0.1	U	0.1	0.1	U	0.1	0.1	U	0.1	0.1	υ	0.1	0.1	U
0.1	Eridrin Aldehyde	0.1	0.1	U	0.1	0.1	U	0.1	0.013	J	0.1	0.1	υ	0.1	0.1	U
0.05	alpha-Chlordane	0.05	0.05	U	0.05	0.05	U	0.05	0.051	U	0.05	0.05	υ	0.05	0.05	U
0.05	gamma-Chlordane	0.05	0.05	U	0.05	0.05	U	0.05	0.051	U	0.05	0.05	U	0.05	0.05	U
5	Toxaphene	5	5	U	5	5	U	5	5.1	U	5	5	U	5	5	U
1	Aroclor-1016	1	1	U	1	1	U	1	1	U	1	1	υ	1	1	Ū
2	Aroclor-1221	2	2	U	2	2	U	2	2	U	2	2	υ	2	2	U
1	Aroclor-1232	1	1	U	1	1	U	1	1	U	1	1	υ	1	1	U
1	Aroclor-1242	1	1	U	1	1	U	1	1	U	1	1	U	1	1	Ū
1	Aroclor-1248	1	1	U	1	1	ļυ	1	1	U	1	1	υ	1	1	Ū
1	Aroclor-1254	1	1	U	1	1	U	1	1	U	1	1	Ū	1	1	Ū
1	Aroclor-1260	1 1	1	U	1	1	U	1 1	1	lυ	1 1	1	U	1 1	1	Ū

Notes:

All units are µg/l.

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NA indicates Not Applicable.

MW-14RD is a field duplicate of MW-14R.

MW-18DD is a field duplicate of MW-18D.

ACCESS\carlstad.mb1\pest report (11/6/96) new wells 1/21/97 3:12:34 PM

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Page 2 of 3

#### SUMMARY OF CLP ORGANICS ANALYSES ...

943-6222

216 Paterson Plank Road Site Sample Results Pesticides / PCBs

Matrix: Groundwater

			ample Poin MW-18D	l	ample Poi		S	ample Poi	nt	S	ample Point		s	ample Poin	t	
		ł	ampled:9/1	9/96	1	ampled: 9		Date Sa	ampled: 9/	23/96	Date S	ampled:		Date S	ampled:	
		1	•	.0		Factor:		I	-	1.0		Factor:			Factor:	
		Percent		NA %	Percen			Percen		NA %			0/	Percen		%
CRQL	Parameter	SQL	Result	Qual	SQL	Result	Qual	SQL	Result	Qual	SQL	Result				
0.05	alpha-BHC	0.05	0.05	U	0.05		U	0.05			SUL	Result	Qual	SQL	Result	Qual
0.05	beta-BHC	0.05	0.05	U	0.05	0.05	1 -		0.05	U						
0.05	delta-BHC	1 1	0.05	1		0.05	U	0.05	0.05	U						
0.05		0.05		U	0.05	0.05	U	0.05	0.05	U				ŀ		
0.05	gamma-BHC (Lindane)	0.05	0.05	U	0.05	0.05	U	0.05	0.05	U						
0.05	Heptachlor Aldrin	0.05	0.05	U	0.05	0.05	U	0.05	0.05	U						
1 1		0.05	0.05	U	0.05	0.05	U	0.05	0.05	U	i					1 1
0.05	Heptachlor Epoxide	0.05	0.05	U	0.05	0.05	U	0.05	0.05	U	l					
0.05	Endosulfan I	0.05	0.05	U	0.05	0.05	U	0.05	0.05	U						
0.1	Dieldrin	0.1	0.1	U	0.1	0.1	U	0.1	0.1	U		!				
0.1	4,4'-DDE	0.1	0.1	U	0.1	0.1	U	0.1	0.1	U				İ		
0.1	Endrin	0.1	0.1	U	0.1	0.1	U	0.1	0.1	U						1
0.1	Endosulfan II	0.1	0.1	U	0.1	0.1	U	0.1	0.1	U						
0.1	4,4'-DDD	0.1	0.1	U	0.1	0.1	U	0.1	0.1	U	l					
0.1	Endosulfan Sulfate	0.1	0.1	U	0.1	0.1	U	0.1	0.1	U	ĺ					
0.1	4,4'-DDT	0.1	0.1	U	0.1	0.1	U	0.1	0.1	U				İ		1
0.5	Methoxychlor	0.5	0.5	U	0.5	0.5	U	0.5	0.5	U	1					
0.1	Endrin Ketone	0.1	0.1	ļυ	0.1	0.1	U	0.1	0.1	ĺυ						
0.1	Endrin Aldehyde	0.1	0.1	υ	0.1	0.1	U	0.1	0.1	U						1
0.05	alpha-Chlordane	0.05	0.05	Jυ	0.05	0.05	U	0.05	0.05	Ū	]		j	}		j
0.05	gamma-Chlordane	0.05	0.05	U	0.05	0.05	υ	0.05	0.05	Ū	ĺ					
5	Toxaphene	5	5	U	5	5	ĺυ	5	5	Ü						
1	Aroclor-1016	1 1	1	lυ	1	1	Ū	1	1	Ü						
2	Aroclor-1221	2	2	Ū	2	2	Ū	2	2	Ü						
1	Aroclor-1232	1 1	1	Ū	1 1	1	Ü	1 1	1	Ü						
1	Aroclor-1242	1 1	1	Ü	1	1	υ	1 1	1	Ü						
1	Aroclor-1248	1 1	1	U	1	1	Ιŭ	i	1	U						
1	Aroclor-1254	1 1	1	Ü	1	1	Ü	1 1		U				ł		
1	Aroclor-1260		1	l ü	1	1	Ü	1		U	1					
Notoce			<del></del>	J _ <u>~</u> _	J	L!		I	l!		I	L	L	l	L <u></u>	

Notes:

All units are µg/l.

Sample Quantitation Limit (SQL) is the CRQL multiplied by the dilution factor.

The Qual column indicates the qualifier applied to the result following data validation.

NA indicates Not Applicable.

MW-14RD is a field duplicate of MW-14R.

MW-18DD is a field duplicate of MW-18D.

ACCESS\carlstad.mb1\pest report (11/6/96) new wells 1/21/97 3:12:37 PM

Golder Associates

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### SUMMARY OF INORGANICS ANALYSES

216 Paterson Plank Road Site Sample Results TAL Metals

Matrix: Groundwater

		Samp	le Point			Samp	le Point			Samp	le Point			Samp	le Point	
	1	MW	/-08R			MV	/-10D			MW	/-10R			MV	/-11R	
	Date Sar	npled:	9/19/96		Date Sar	npled:	9/20/96		Date Sar	npled:	9/20/96		Date Sar	npled:	9/24/96	
	Dilution F	actor:	NA		Dilution F	actor:	NA		Dilution 6	actor:	NA		Dilution F	actor:	NA	
	Percent :	Solid:	NA %	<u>,</u>	Percent :	Solid:	NA %	<b>.</b>	Percent	Solid:	NA %	, ,	Percent :	Solid:	NA %	
Parameter	CRDL	IDL	Result	Qual	CRDL	IDL	Result	Qual	CRDL	IDL	Result	Qual	CRDL	IDL	Result	Qua
Aluminum	200	28.2	174	В	200	28.2	193	В	200	28.2	348.0		200	28.2	361.0	
Antimony	60 、	2.2	2.2	Ü	60	2.2	3.5	В	60	2.2	2.2	υ	60	2.2	2.2	U
Arsenic	10	2.3	2.3	Ü	10	2.3	2.6	В	10	2.3	2.3	Ŭ	10	2.3	2.3	Ū
Barium	200	0.2	73.4	В	200	0.2	40.9	В	200	0.2	25.7	В	200	0.2	34.3	В
Beryllium	5	0.1	0.1	Ū	5	0.1	0.1	Ū	5	0.1	0.1	Ιŭ	5	0.1	0.1	Ü
Cadmium	5	0.3	0.3	Ü	5	0.3	0.31	В	5	0.3	0.3	В	5	0.3	0.3	Ü
Calcium	5000	11.0	308000		5000	11.0	88300		5000	11.0	91900.0	"	5000	11.0	120000.0	"
Chromium	10	1.6	163		10	1.6	373		10	1.6	5.3	В	10	1.6	14.0	
Cobalt	50	0.5	0.57	В	50	0.5	0.54	В	50	0.5	0.5	Ιū	50	0.5	0.5	υ
Copper	25	1.8	10.7	В	25	1.8	8.6	В	25	1.8	4.5	В	25	1.8	10.4	В
Iron	100	25.5	114		100	25.5	162		100	25.5	354.0	_	100	25.5	362.0	
Lead	3	1.3	1.3	U	<b>3</b>	1.3	1.7	В	3	1.3	1.3	U	3	1.3	2.5	В
Magnesium	5000	4.3	14700	İ	5000	4.3	527	В	5000	4.3	4170.0	В	5000	4.3	119.0	В
Manganese	15	0.5	6.6	В	15	0.5	4.3	В	j 15	0.5	14.9	В	15	0.5	3.7	В
Mercury	0.2	0.2	0.2	U	0.2	0.2	0.2	U	0.2	0.2	0.2	Ū	0.2	0.2	0.2	Ū
Nickel	40	1.6	15.7	В	40	1.6	13	В	40	1.6	6.0	В	40	1.6	4.3	В
Potassium	5000	29.4	38800	J	5000	29.4	41100	J	5000	29.4	3840.0	J	5000	29.4	10100.0	J
Selenium	5	3.0	3	U	5	3.0	3	U	5	3.0	3.0	Ū	5	3.0	3.0	ŪJ
Silver	10	0.6	0.6	UJ	10	0.6	0.6	UJ	10	0.6	0.6	UJ	10	0.6	0.6	U
Sodium	5000	214.0	144000		5000	214.0	82100		5000	214.0	36700.0	ĺ	5000	214.0	46300.0	i -
Thallium	10	3.1	3.1	U	10	3.1	3.1	U	10	3.1	3.1	U	10	3.1	3.1	U
Vanadium	50	0.6	4.2	В	50	0.6	48.1	В	50	0.6	28.3	В	50	0.6	62.8	
Zinc	20	1.2	21.8	J	20	1.2	16.7	J	20	1.2	24.1	J	20	1.2	24.5	R
Cyanide	_10	10.0	10	U	10	10.0	10	U	10	10.0	10.0	ĺυ	10	10.0	10.0	U

#### Notes:

All units are µg/l.

CRDL indicates Contract Required Detection Limit.

IDL is the Instrument Detection Limit.

The Qual column indicates the qualifier applied to the result following data validation.

NA indicates Not Applicable.

MW-14RD is a field duplicate of MW-14R.

MW-18DD is a field duplicate of MW-18D.

## SUMMARY OF INORGANICS ANALYSES

216 Paterson Plank Road Site Sample Results TAL Metals

Matrix: Groundwater

		Samp	le Point			Samp	le Point	-		Samp	le Point			Samp	le Point	
		MV	/-14D			MV	/-14R			MW	-14RD			MV	/-15D	
	Date Sar	npled:	9/23/96		Date Sar	npled:	9/23/96		Date Sar	mpled:	9/23/96		Date Sar	npled:	9/24/96	
	Dilution F	actor:	NA		Dilution F	actor:	NA		Dilution I	Factor:	NA		Dilution F	actor:	NA	
	Percent :	Solid:	NA %	•	Percent :	Solid:	NA %		Percent :	Solid:	NA %	,	Percent S	Solid:	NA %	á
Parameter	CRDL	IDL	Result	Qual	CRDL	IDL	Result	Qual	CRDL	IDL	Result	Qual	CRDL	IDL	Result	Qual
Aluminum	200	28.2	544		200	28.2	167	В	200	28.2	173.0	В	200	28.2	389.0	
Antimony	60	2.2	2.2	υ	60	2.2	2.2	Ū	60	2.2	2.2	Ū	60	2.2	2.2	U
Arsenic	10	2.3	8	В	10	2.3	3	В	10	2.3	2.6	В	10	2.3	2.3	Ü
Barium	200	0.2	61.4	В	200	0.2	16	В	200	0.2	16.7	В	200	0.2	108.0	В
Beryllium	5	0.1	0.1	U	5	0.1	0.1	U	5	0.1	0.1	Ū	5	0.1	0.1	Ū
Cadmium	5	0.3	0.48	В	5	0.3	0.3	Ū	5	0.3	0.3	В	5	0.3	0.3	Ü
Calcium	5000	11.0	103000	ĺ	5000	11.0	170000		5000	11.0	168000.0		5000	11.0	123000.0	
Chromium	10	1.6	434	ĺ	10	1.6	4	В	10	1.6	3.9	В	10	1.6	42.0	
Cobalt	50	0.5	0.58	В	50	0.5	0.5	U	50	0.5	0.5	Ū	50	0.5	0.5	U
Copper	25	1.8	22.1	В	25	1.8	3.3	В	25	1.8	4.3	В	25	1.8	8.9	В
Iron	100	25.5	135		100	25.5	1320	1	100	25.5	1310.0		100	25.5	290.0	-
Lead	3	1.3	1.3	U	3	1.3	1.3	U	3	1.3	1.9	υ	3	1.3	3.2	
Magnesium	5000	4.3	150	В	5000	4.3	9760	1	5000	4.3	9300.0		5000	4.3	1270.0	В
Manganese	15	0.5	2.9	В	15	0.5	36.8		15	0.5	35.3	ĺ	15	0.5	6.5	В
Mercury	0.2	0.2	0.2	U	0.2	0.2	0.2	U	0.2	0.2	0.2	υ	0.2	0.2	0.2	Ū
Nickel	40	1.6	9	В	40	1.6	3.6	В	40	1.6	5.9	В	40	1.6	18.9	В
Potassium	5000	29.4	101000	J	5000	29.4	2520	J	5000	29.4	2500.0	J	5000	29.4	14800.0	J
Selenium	5	3.0	4.1	J	5	3.0	3	UJ	5	3.0	3.0	UJ	5	3.0	3.0	UJ
Silver	10	0.6	0.6	U	10	0.6	0.6	U	10	0.6	0.6	U	10	0.6	0.6	U
Sodium	5000	214.0	120000		5000	214.0	36000		5000	214.0	35400.0		5000	214.0	55900.0	İ
Thallium	10	3.1	3.1	U	10	3.1	3.1	U	10	3.1	3.1	U	10	3.1	3.1	U
Vanadium	50	0.6	87.3		50	0.6	9.8	В	50	0.6	9.6	В	50	0.6	21.7	В
Zinc	20	1.2	54.3	R	20	1.2	68.2	R	20	1.2	73.9	R	20	1.2	32.2	R
Cyanide	10	10.0	10.9	<u> </u>	10	10.0	10	U	_10	10.0	10.0	U	10	10.0	10.0	Ūυ

#### Notes:

All units are µg/l.

CRDL indicates Contract Required Detection Limit.

IDL is the Instrument Detection Limit.

The Qual column indicates the qualifier applied to the result following data validation.

NA indicates Not Applicable.

MW-14RD is a field duplicate of MW-14R.

MW-18DD is a field duplicate of MW-18D.

### SUMMARY OF INORGANICS ANALYSES

216 Paterson Plank Road Site Sample Results TAL Metals

Matrix: Groundwater

		Samp	le Point			Sample Point Sample Point						Sample Point				
		MW	/-16D			MV	/-17D			MV	V-18D			MW	-18DD	
	Date Sar	npled:	9/23/96		Date Sar	npled:	9/19/96		Date Sar	npled:	9/19/96		Date Sar	npled:	9/19/96	
	Dilution F	actor:	NA		Dilution F	actor:	NA		Dilution F	actor:	NA		Dilution F	actor:	NA	
	Percent :	Solid:	NA %	, •	Percent :	Percent Solid:		NA %		Percent Solid:		NA %		Percent Solid:		•
Parameter	CRDL	IDL	Result	Qual	CRDL	IDL	Result	Qual	CRDL	IDL	Result	Qual	CRDL	IDL	Result	Qua
Aluminum	200	28.2	246		200	28.2	531		200	28.2	203.0		200	28.2	219.0	
Antimony	60	2.2	2.2	U	60	2.2	2.2	l u	60	2.2	2.2	υ	60	2.2	2.2	U
Arsenic	10	2.3	2.3	Ū	10	2.3	2.3	Ü	10	2.3	2.3	Ü	10	2.3	2.3	U
Barium	200	0.2	184	В	200	0.2	64.6	В	200	0.2	35.4	В	200	0.2	35.1	В
Beryllium	5	0.1	0.1	U	5	0.1	0.1	Ū	5	0.1	0.1	Ū	5	0.1	0.1	Ιυ
Cadmium	5	0.3	0.3	υ	5	0.3	0.34	В	5	0.3	0.3	ŭ	5	0.3	0.3	Ιŭ
Calcium	5000	11.0	224000	ĺ	5000	11.0	254000		5000	11.0	297000.0	ĺ	5000	11.0	296000.0	ľ
Chromium	10	1.6	2.1	В	10	1.6	6.1	В	10	1.6	3.2	В	10	1.6	2.5	В
Cobalt	50	0.5	0.5	U	50	0.5	1.7	В	50	0.5	0.9	В	50	0.5	1.0	В
Copper	25	1.8	5.8	В	25	1.8	4.7	В	25	1.8	6.3	В	25	1.8	6.1	В
Iron	100	25.5	41.9	В	100	25.5	945	1	100	25.5	138.0		100	25.5	128.0	
Lead	3	1.3	1.9	В	3	1.3	1.3	U	3	1.3	1.3	υ	3	1.3	1.9	В
Magnesium	5000	4.3	4570	В	5000	4.3	57300		5000	4.3	48500.0		5000	4.3	48500.0	
Manganese	15	0.5	3.1	В	15	0.5	1360		15	0.5	318.0		15	0.5	319.0	ĺ
Mercury	0.2	0.2	0.2	U	0.2	0.2	0.2	U	0.2	0.2	0.2	υ	0.2	0.2	0.2	U
Nickel	40	1.6	4.4	В	40	1.6	41.5		40	1.6	29.4	В	40	1.6	30.6	В
Potassium	5000	29.4	12100	J	5000	29.4	7640	J	5000	29.4	5690.0	J	5000	29.4	5690.0	J
Selenium	5	3.0	3	UJ	5	3.0	3	U	5	3.0	3.0	υ	5	3.0	3.0	U
Silver	10	0.6	0.6	U	10	0.6	0.6	UJ	10	0.6	0.6	UJ	10	0.6	0.6	UJ
Sodium	5000	214.0	93100		5000	214.0	244000		5000	214.0	199000.0		5000	214.0	199000.0	
Thallium	10	3.1	3.1	U	10	3.1	3.1	υ	10	3.1	3.1	U	10	3.1	3.1	U
Vanadium	50	0.6	10	В	50	0.6	1.9	В	50	0.6	4.8	В	50	0.6	4.7	В
Zinc	20	1.2	50.6	R	20	1.2	13.7	J	20	1.2	18.4	J	20	1.2	31.8	J
Cyanide	10	10.0	10	U	10	10.0	10	U	10	10.0	10.0	U	10	10.0	10.0	lυ

#### Notes:

All units are µg/l.

CRDL indicates Contract Required Detection Limit.

IDL is the Instrument Detection Limit.

The Qual column indicates the qualifier applied to the result following data validation.

NA indicates Not Applicable.

MW-14RD is a field duplicate of MW-14R.

MW-18DD is a field duplicate of MW-18D.

#### **SUMMARY OF INORGANICS ANALYSES**

216 Paterson Plank Road Site Sample Results TAL Metals

Matrix: Groundwater

			le Point			Samp	le Point			Samp	le Point		Sample Point			
			V-01													
	Date Sar	npled:	9/23/96		Date Sar	npled:			Date Sar	npled:			Date Sar	npled:		
	Dilution F	actor:	1		Dilution F	actor:			Dilution F	actor:			Dilution F	actor:		
	Percent :	Solid:	NA %	5	Percent Solid: %		Percent Solid: %				Percent Solid:			6		
Parameter	CRDL	IDL	Result	Qual	CRDL	IDL	Result	Qual	CRDL	IDL	Result	Qual	CRDL	IDL	Result	Qual
Aluminum	200	28.2	238												· · · · · · · · · · · · · · · · · · ·	
Antimony	60	2.2	2.2	U					ł			}				ļ
Arsenic	10	2.2	2.2	U	'	Ì						ł				
Barium	200	0.2	68.2	В								}				}
Beryllium	5	0.2	0.1	Ü		l										
Cadmium	5	0.1	0.1	U		1										
Calcium	5000	11.0	35100	0												
Chromium	10	1.6	1.6	U												
Cobalt	50	0.5	0.5	Ü		[										
Copper	25	1.8	21.6	В		1							ł			
Iron	100	25.5	27.0	В												
Lead	3	1.3	1.9	В					1							
Magnesium	5000	4.3	6770	"	1		 		1	1			ł			
Manganese	15	0.5	7.7	В	ļ	1	 		1				<b>!</b>			}
Mercury	0.2	0.3	0.2	Ü					1				1			
Nickel	40	1.6	3	В					ļ	1			1			
Potassium	5000	29.4	1970	J									ļ			
Selenium	5	3.0	3	บ้า		ł			ł					ŀ		1
Silver	10	0.6	0.6	U												
Sodium	5000	214.0	37000											1		
Thallium	10	3.1	3.1	U	1				1							
Vanadium	50	0.6	0.93	В	1				1				1			
Zinc	20	1.2	38.6	R	1				1				ł			
Cyanide	10	10.0	10	Ü									1	}		

All units are µg/l.

CRDL indicates Contract Required Detection Limit.

IDL is the Instrument Detection Limit.

The Qual column indicates the qualifier applied to the result following data validation.

NA indicates Not Applicable.

MW-14RD is a field duplicate of MW-14R.

MW-18DD is a field duplicate of MW-18D.

#### SUMMARY OF INORGANICS ANALYSES

216 Paterson Plank Road Site Sample Results Indicator List Parameters

Matrix: Groundwater

	Sample P	Sample Point			Sample F	oint	Sample	Point	Sample Point	
	MW-08	R	MW-10	D	MW-10	R	MW-1	ļR	MW-14D	
	Date Sampled:			1		1 ' 1		: 9/24/96	Date Sampled: 9/23/96 Dilution Factor: NA	
	Dilution Factor:							r: NA		
	Percent Solid:	NA %	Percent Solid:	NA %	Percent Solid:	NA %	Percent Solid:	NA %	Percent Solid:	NA %
Parameter	Result	Qual	Result	Qual	Result	Qual	Result	Qual	Result	Qual
Alkalinity	35.2		73.5		36.8		121		150	
Chloride	635		28.8		78.4		60.5	•	80.2	
Ethane	100	U	100	U	100	U	100	U	100	U
Ethene	100	U	100	U	100	U	100	U	100	U
Methane	135		100	U	100	U	100	U	100	U
Nitrate-Nitrite	0.1	U	0.1	U	0.1	U	0.1	UJ	0.18	J
Phosphorus, Total	0.1	U	0,1	U	0.1	U	0.1	U	0.1	U
Sulfate	251		330		181		221		393	
Sulfide	2	U	2	U	2	U	3		3.1	
TKN	0.35		0.45		0.21		1.3		1.1	
Total Organic Carbon	3.6		1.4		1.2		5.3	J	3.6	J
Dissolved Iron	25.5	U	25.5	U	25.5	U	25.5	U	25.5	U

**Golder Associates** 

#### Notes:

All units are mg/l except for the following: Ethane, Ethene, Methane, and Dissolved Iron.

The Qual column indicates the qualifier applied by the laboratory to the result following data validation.

NA indicates Not Analyzed.

Sample ID MW-14RD is field duplicate of MW-14R.

Sample ID MW-18DD is field duplicate of MW-18D.

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#### **SUMMARY OF INORGANICS ANALYSES**

#### 216 Paterson Plank Road Site Sample Results Indicator List Parameters

Matrix: Groundwater

Sample Point Sample Point Sample Point Sample Point Sample Point MW-14R MW-14RD MW-15D MW-16D MW-17D Date Sampled:9/23/96 Date Sampled: 9/23/96 Date Sampled: 9/24/96 Date Sampled: 9/23/96 Date Sampled: 9/19/96 Dilution Factor: NA Dilution Factor: Dilution Factor: NA Dilution Factor: NA Dilution Factor: NA Percent Solid: Percent Solid: Percent Solid: Percent Solid: NA % Percent Solid: NA % NA % NA % NA % Parameter Result Qual Result Qual Result Qual Result Qual Result Qual Alkalinity 16.4 15.8 214 172 257 Chloride 90.3 91.3 22.3 372 653 U U Ethane 100 U 100 100 U 100 100 U U U Ethene U 100 100 U U 100 100 100 Methane U U 100 U 100 100 323 100 U UJ UJ Nitrate-Nitrite UJ 0.1 UJ U 0.1 0.1 0.1 0.1 Phosphorus, Total U 0.1 U 0.1 U U 0.1 U 0.1 0.1 Sulfate 492 379 181 112 228 Sulfide 2 U 2 U U 2 2 U 2

U

U

U

0.2

25.5

U

U

U

0.2

1.5

25.5

#### Dissolved Iron Notes:

TKN

0.2

1

25.5

U

U

U

0.2

25.5

Total Organic Carbon

943-6222

0.26

3.5

277

All units are mg/l except for the following: Ethane, Ethene, Methane, and Dissolved Iron.

The Qual column indicates the qualifier applied by the laboratory to the result following data validation.

NA indicates Not Analyzed.

Sample ID MW-14RD is field duplicate of MW-14R.

Sample ID MW-18DD is field duplicate of MW-18D.

#### SUMMARY OF INORGANICS ANALYSES

#### 216 Paterson Plank Road Site Sample Results Indicator List Parameters

Matrix: Groundwater

	Sample Po		Sample F	Point	Sample F	oint	Sample	Point	Sample	Point
	MW-18	MW-18D		DD						,
	Date Sampled:	9/19/96	Date Sampled:	9/19/96	Date Sampled:	:	Date Sampled	l:	Date Sample	d:
	Dilution Factor:	NA	Dilution Factor:	: NA	Dilution Factor	:	Dilution Facto	r:	Dilution Facto	or:
	Percent Solid:	NA %	Percent Solid:	NA %	Percent Solid:	%	Percent Solid:	%	Percent Solid	: %
Parameter	Result	Qual	Result	Qual	Result	Qual	Result	Qual	Result	Qual
Alkalinity	147		142	1						
Chloride	717		722							
Ethane	100	U	100	U						
Ethene	100	U	100	U						
Methane	100	U	100	U						
Nitrate-Nitrite	0.1	U	0.1	U	<b>1</b>				1	
Phosphorus, Total	0.1	U	0.1	U	1					
Sulfate	263		256							
Sulfide	2	U	2	U						
TKN	0.3		0.26		I					
Total Organic Carbon	2.8		2.9							
Dissolved Iron	25.5	U	NS		i l				<u>'</u>	1

#### Notes:

Sample ID MW-14RD is field duplicate of MW-14R.

Sample ID MW-18DD is field duplicate of MW-18D.

All units are mg/l except for the following: Ethane, Ethene, Methane, and Dissolved Iron.

The Qual column indicates the qualifier applied by the laboratory to the result following data validation.

NA indicates Not Analyzed.

#### SUMMARY OF INORGANICS ANALYSES

943-6222

216 Paterson Plank Road Site Sample Results Indicator List Parameters

Matrix: Groundwater

	Sample P	oint	Sample F	Point	Sample P	oint	Sample F	Point	Sample Point MW-08D	
	MW-02	D	MW-02	:R	MW-05	D	MW-07	D.		
	Date Sampled:	Date Sampled:9/17/96 D		Date Sampled: 9/18/96 D		Date Sampled: 9/18/96		9/18/96	Date Sampled: 9/18/96	
	Dilution Factor:	NA	Dilution Factor:	: NA	Dilution Factor:	NA	Dilution Factor:	: NA	Dilution Factor	: NA
	Percent Solid:	NA %	Percent Solid:	NA %	Percent Solid:	NA %	Percent Solid:	NA %	Percent Solid:	NA %
Parameter	Result	Qual	Result	Qual	Result	Qual	Result	Qual	Result	Qual
Alkalinity	22.6		37.3		26.2		32.6		38.3	
Chloride	754		615		385		43.9		454	
Ethane	100	U	100	U	100	U	100	U	100	U
Ethene	100	U	100	U	100	U	100	U	100	U
Methane	287		125		104		100	U	474	
Nitrate-Nitrite	0.1	U	0.1	U	0.1	U	0.1	U	0.1	U
Phosphorus, Total	0.1	U	0.1	U	0.1	U	0.1	U	0.14	
Sulfate	191		192		305		338		366	
Sulfide	2	U	2	U	2	U	2	U	2	U
TKN	0.24		0.2	U	0.37		0.4	U	0.26	
Total Organic Carbon	1 1	U	1	U	1 1	U	1 1	U	1.3	
Dissolved Iron	25.5	U	25.5	U	25.5	U	25.5	U	25.5	U

Golder Associates

#### Notes:

All units are mg/l except for the following: Ethane, Ethene, Methane, and Dissolved Iron.

The Qual column indicates the qualifier applied by the laboratory to the result following data validation.

NA indicates Not Analyzed.

#### SUMMARY OF INORGANICS ANALYSES

943-6222

#### 216 Paterson Plank Road Site Sample Results Indicator List Parameters

Matrix: Groundwater

	Sample P	oint	Sample F	Point	Sample P	oint	Sample Point		Sample Point		
	MW-11	D	MW-12D		RMW-13D						
	Date Sampled:	9/24/96	Date Sampled: 9/23/96 D		Date Sampled:	9/23/96	Date Sampled	<b>d</b> :	Date Sampled:		
	Dilution Factor: NA		Dilution Factor: NA		Dilution Factor: NA		Dilution Factor:		Dilution Factor:		
	Percent Solid: NA %		Percent Solid: NA %		Percent Solid: NA % I		Percent Solid: %		Percent Solid	: %	
Parameter	Result	Qual	Result	Qual	Result	Qual	Result	Qual	Result	Qual	
Alkalinity	36.9		267		39.6						
Chloride	189		494		308		<b>!</b>				
Ethane	100	U	100	U	100	U				i	
Ethene	100	U	100	U	100	U					
Methane	599		505		369						
Nitrate-Nitrite	0.1	UJ	0.1	UJ	0.1	UJ	<b>\</b>			1	
Phosphorus, Total	0.1	U	0.1	U	0.1	U	1				
Sulfate	204	•	63.8		227						
Sulfide	2	U	2	U	2	U					
TKN	0.2	U	0.2		0.2	U					
Total Organic Carbon	1.5		2.6	J	1	U	]				
Dissolved Iron	25.5	U	223		25.5	U	<u></u>				

#### Notes:

All units are mg/l except for the following: Ethane, Ethene, Methane, and Dissolved Iron.

The Qual column indicates the qualifier applied by the laboratory to the result following data validation.

NA indicates Not Analyzed.